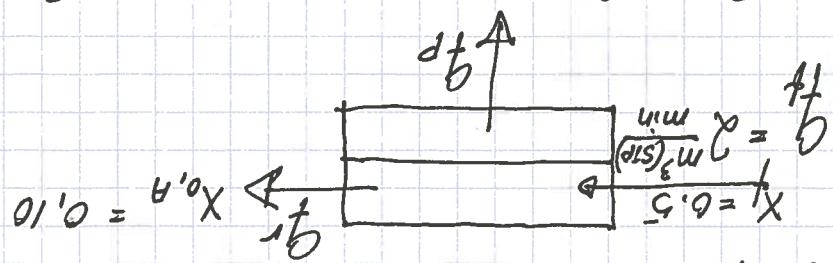


$$q_t = q_r + q_p$$



du Stream:

→ using this route to calculate

$$\text{b) Assuming } 25\% \text{ hign} \Rightarrow X_{0,A} = 0.10$$

$$\Rightarrow \text{gas B is thus } X_{0,B} = 0.92$$

$$X_{0H,A} = 0.079 \approx 0.08 \text{ for gas A}$$

$$= \frac{30(1-0.5) + 0.5}{0.5[1 + (30-1)\frac{1}{10}(1-0.5)]}$$

$$\frac{x^* (1-x^*)}{[1 + (\alpha^* - 1) \frac{p_A}{p_B} (1-x^*)]} = X_{0n}$$

Using given information and eq. 13.4-12

a) Designing our main effect.

25% vels

Apparatus I Membrane-separation

Total gasif. MB eff.

EKSamen 2013 - Sep-tel

$$\text{which is } \frac{0.154}{0.154 - 1.00\%} = 15.4\% \text{ loss$$

$$1.06 \cdot 0.145 = 0.154 \frac{\text{min}}{\text{m}^3(\text{STP})}$$

Gas B in permeate:

$$\text{Hence, } q_{\text{permeate B}} = \frac{1}{\text{min}} \frac{\text{m}^3(\text{STP})}{\text{m}^3(\text{STP})}$$

$q_{\text{permeate A}}$: $0.2 \cdot 0.5 = 0.1 \text{ m}^3(\text{STP})/\text{min}$

How much of A are we focusing?

$$= \frac{0.855}{0.53} (q_{\text{permeate A}})$$

$$= \frac{0.5 - 0.1(1 - 0.53)}{0.53}$$

$$\text{using 13.4-8: } q_r = \frac{\Theta}{(1-\Theta) - x_0(1-\Theta)}$$

Calculating composition q_r

$$\text{thus } q_r = 0.94$$

$$= 1.06 \frac{\text{min}}{\text{m}^3(\text{STP})}$$

$$\theta = \frac{q_r}{q_p} = 0.53 \Leftrightarrow q_p = 0.53 \cdot \theta$$

- Try to increase selectivity (hence metal)
- Change pressure ratio with regard to $\text{eff}(E)$
- Make a cascade solution or the two steps
- (d) Reduce the loss of E by:

$$\frac{\text{Membrane area}}{0.14 \cdot 76.24 \cdot 10^{-3} \cdot 357 \cdot 10^6 \text{ cm}^2} = 0.916 \cdot 10^6 \text{ cm}^2$$

$$\frac{60 \cdot 400 \cdot 10^{-6} \cdot 0.14 \cdot 76}{0.53 \cdot 2 \cdot 0.86 \cdot 10^6 \cdot \text{cm}^2} =$$

~~$$= 0.53 \cdot (2 \cdot 10^6 \text{ cm}^3/60s) \cdot 0.86 / 0.14 \cdot 76 \text{ cm}^2$$~~

new g-force cm: $1 - 0.86 = 0.14 \text{ bar}$

$$= \frac{400 \text{ bar} \cdot 10^{-6} \text{ m}}{0.53 \cdot 2 \text{ min} \cdot 0.86} (10 \text{ bar} \cdot 0.86 - 1 \text{ bar} \cdot 0.86)$$

$$= \frac{(P_A/e)(P_n x_0 - P_n y_p)}{\Theta q + X_p} \text{ l/m}$$

eq. 13.4-9:

1c) Calculating membrane area:

$$= \frac{7.5 \text{ cm}}{12.8} \text{ unused bed}$$

$$= \left(1 - \frac{9.58}{12.8} \right) 0.30 \text{ m}$$

$$H_{\text{unb}} = \left(1 - \frac{t_b}{t_u} \right) H$$

b) Break point: $t_b = 9.58 \text{ h}$

graph or table,

$$t_u = \int_{t_0}^0 (1 - \frac{C}{C_0}) dt \leftarrow \text{from}$$

t_b	0.4	0.85	1.0	9.6	1.0
	0.098				
	0.027				
	1.00				
	12.8				
t_u					
C/C_0					
t_u					
C/C_0					

← see table

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column

current

concentration

=

a) calculating $C/C_0 \rightarrow \text{table } \times \cancel{0.926}$

$$H = 30 \text{ cm } C_0 = 212.8 \text{ g/m}^3$$

Problem on Adsorption (4)

25% weight

Forslag til fysisk Mary-Beth

$$\frac{712 \cdot 8 \text{ kg}}{160 \text{ kg H}_2\text{O}} = 0.22 \text{ kg partial}$$

$$= \frac{35.95}{0.225} \text{ m}^3 \text{ kg H}_2\text{O} \approx 160 \text{ kg H}_2\text{O}$$

$$926 \cdot 10^{-6} \cdot 4052 \cdot 9.58 \text{ kg H}_2\text{O} \text{ m}^2 \cdot 0.025 \text{ m}$$

$$\frac{926 \cdot 10^{-6} \text{ kg H}_2\text{O}}{\text{kg N}_2}$$

Total water adsorbed:

$$\text{N}_2\text{-dew rate: } 4052 \text{ kg/m}^2\text{h}$$

after 12.8 h the column is saturated

for water up-toe with 11.41% breakthrough of the column

$$\text{up to } t_b \\ \text{dew point } \text{N}_2 \leftarrow 9.58 \text{ kg H}_2\text{O} / \text{m}^3 \text{ air}$$

$$\text{up to } t_b \\ \text{dew point } \text{N}_2 = 11.19 \text{ kg H}_2\text{O} / \text{m}^3 \text{ air}$$

$$\text{up to } t_b \\ \text{dew point } \text{N}_2 = 9.58 + 1.61 \text{ h} = 11.19 \text{ h}$$

\Rightarrow total capacity will be used

mass transfer zone is 1.61 h

\Rightarrow additional led in

is 3.22 h.

c) The graph between $t = 9.58$ and 12.8 h