

A Batch Reactor Heat Recovery Challenge Problem

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Outline

- 1 Introduction
- 2 Problem description
- 3 Simulations
- 4 Discussion
- 5 Conclusions

Optimizing real processes consists of 2 parts:

- 1 Optimization problem
 - Formulating the problem
 - Solving it systematically, often using a model
- 2 Implement the solution in the real process



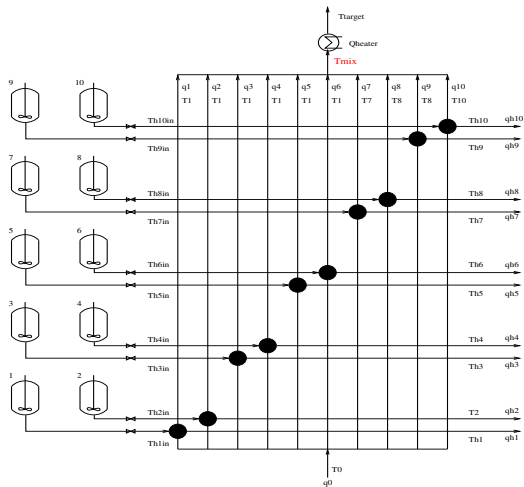
This presentation:

- Challenge problem to test
 - Optimization
 - Implementation
- Discussion

Some challenges when optimizing real systems

- Optimization part
 - Non-linearity
 - Non-convexity
 - Integer variables
 - Non-smoothness
 - Time-varying systems (Dynamic systems)
- Implementation part
 - Missing information
 - Uncertainty
 - Disturbances (parametric uncertainty)
 - Noise
 - Structural model mismatch
 - Temporal uncertainty

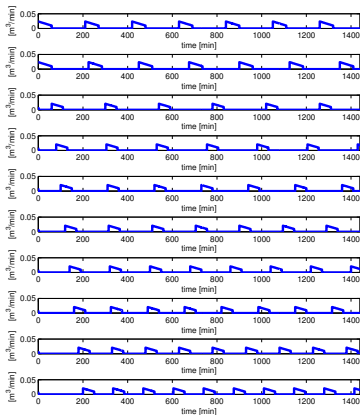
Heat recovery challenge problem



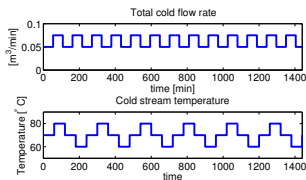
Objective: Adjust split to maximize T_{mix}

Heat recovery challenge problem

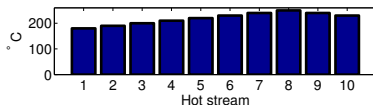
Hot flow rates



Cold flow rate and temperature



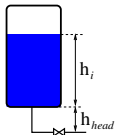
Hot stream temperatures



Heat recovery challenge problem

Batch discharge

- Flow rate:



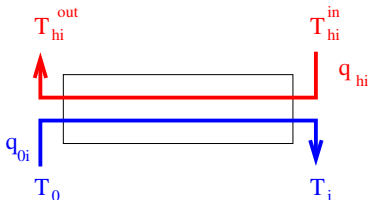
$$q_{hi}^j(t) = \begin{cases} 0 & \text{for } t < t_s \\ k_i \sqrt{\Delta p_i^j} & \text{for } t_{sj}^j \leq t \leq t_{si}^j + t_{ei}^j \\ 0 & \text{for } t > t_{si}^j + t_{ei}^j \end{cases}$$

- t_{si}^j : Start time of discharge j
- t_{ei}^j : End time of discharge j ($h_i^j = 0$)
- Pressure drop at valve

$$\Delta p_i^j = \rho g (h_i^j + h_{head})$$

- Level during discharge j

$$A \frac{dh_i^j}{dt} = -q_i^j$$



- SS-assumption:
- Energy balances

$$Q_i = q_{0i}(T_i - T_0)$$

$$Q_i = q_{hi}(T_{hi}^{in} - T_{hi}^{out})$$

- Heat transfer

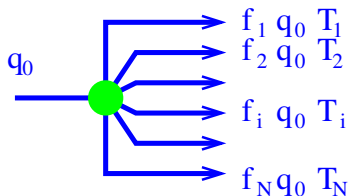
$$Q_i = UA(q_{hi})\Delta T_{log,i}$$

- Heat transfer

$$\Delta T_{log,i} = \frac{(T_{h,i} - T_0) - (T_{hi}^{in} - T_i)}{\log \frac{(T_{h,i} - T_0)}{(T_{hi}^{in} - T_i)}}$$

$$UA_i(q_{hi}) = UA_{0i} \left(\frac{q_{hi}(t)}{q_{h0i}} \right)^{0.8}$$

Splitter and mixer

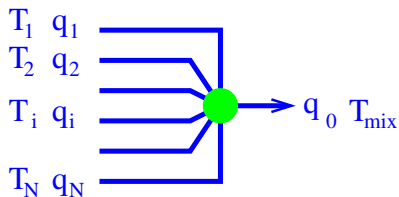


- Splitter

$$T_i = T_0$$

$$q_i = f_i q_0$$

$$\sum_{i=1}^N f_i = 1$$



- Mixer

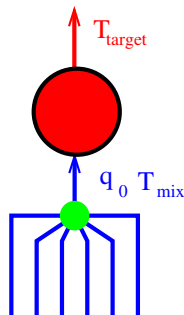
$$T_{mix} = \frac{1}{q_0} \sum_{i=1}^N q_i T_i$$

$$q_0 = \sum_{i=1}^N q_i$$

Objective function and heater

- Heater duty

$$Q_{heat}(t) = q_0 c_p (T_{target} - T_{mix}(t))$$

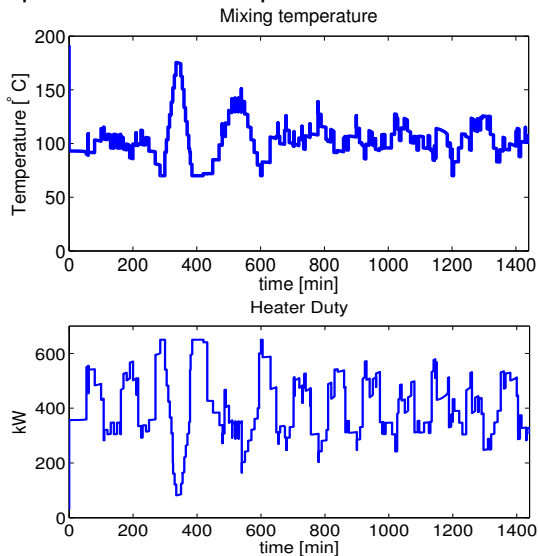


Objective:

$$\min_{f_i} \int_0^{24h} Q_{heater}(t) dt$$

Open-loop Simulation – equal f_i

- Equal fractions in all parallel branches



Introduction

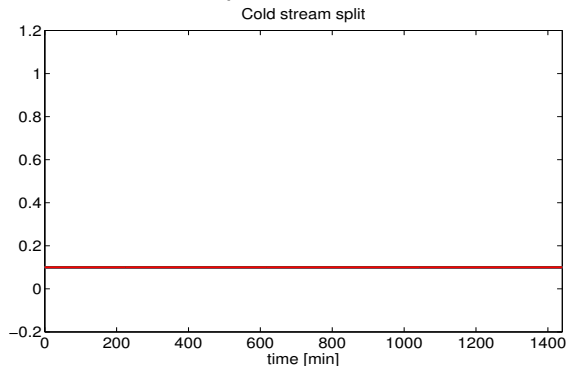
Problem
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- Equal fractions in all parallel branches



$$J = \int_0^{24h} Q_{heat} dt = 35005.17 MJ$$

“Optimization”

Definition

An **active branch** is a branch connected to a no-zero hot stream

Idea

$$q_i = f_i q_0$$

- assign flow only to active branches

$$f_{i,active} = 1/n_{active}$$

$$f_{i,inactive} = 0$$

- if no branch is active, then

$$f_i = 1/n_{total}$$

“Optimized”

J. Jäschke

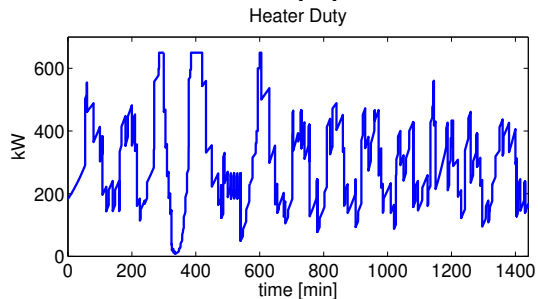
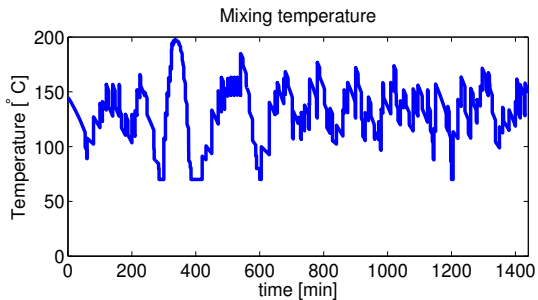
[Introduction](#)

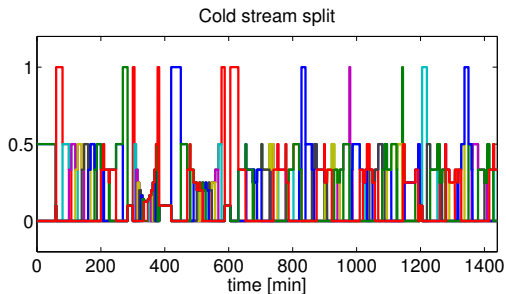
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$$J = \int_0^{24h} Q_{heat} dt = 25364.11 MJ$$

Discussion

Implementation of “optimal solution”

- Very simple
- Assumption: Only hot flows measured
- Clearly sub-optimal

Optimization

- Nonlinear problem
- Time-varying
- Static optimization at each time instant
- Suboptimal policy
 - Temperatures not used.
 - Piecewise constant f_i
- Large improvement

$$35,005.17 MJ \implies 25,364.11 MJ$$

Conclusions

- Nonlinear optimization problem:
 - Sub-optimal solution
 - Simple implementation
- For true optimal solution:
 - More information required
 - Temperatures
 - Flow rates
 - Estimate unmeasured parameters (UA_0)

Future work

- Improve “optimization” algorithm
 - Include temperature measurements
 - Time varying f_i
- Assume flows are not measured
- Modify problem
 - Add buffer tank before split

Thank you !

A simulink model will be made available on
[http://www.nt.ntnu.no/users/skoge/
publications/2012/BatchChallenge](http://www.nt.ntnu.no/users/skoge/publications/2012/BatchChallenge)