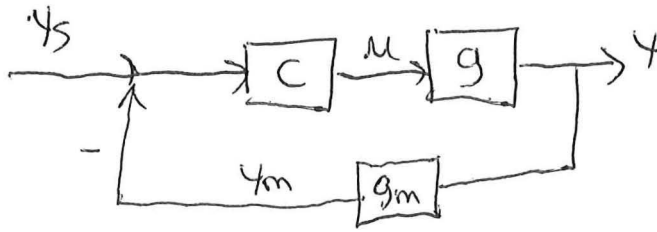


SIMC-rule with measurement delay ( $\theta_m$ )



$g \approx \frac{k e^{-\theta s}}{(\tau_1 s + 1)(\tau_2 s + 1)}$   
 (approximated using half rule)

Before we assumed  $g_m = 1$ .  
 Now assume that  $g_m = e^{-\theta_m s}$

Rule: Design C based on  $\theta_{tot} = \theta + \theta_m$

SIMC-rule (cascade PID) =  $K_c = \frac{1}{k} \frac{\tau_1}{(\tau_c + \theta_{tot})}$ ,  $\tau_c = \min(\tau_1, 4(\tau_c + \theta_{tot}))$ ,  $\tau_D = \tau_2$

Should also choose  $\tau_c = \theta_{tot}$  ("tight" control)

Proof: We design for desired setpoint response ("direct synthesis")

$y = T y_s$  where  $T = \frac{g_c}{1 + g g_m C}$ . Desired  $T = \frac{e^{-\theta s}}{\tau_c s + 1}$

Algebra:  $\frac{k \frac{e^{-\theta s}}{(\tau_1 s + 1)(\tau_2 s + 1)} \cdot C}{1 + \frac{k e^{-\theta s} e^{-\theta_m s} C}{(\tau_1 s + 1)(\tau_2 s + 1)}} = \frac{e^{-\theta s}}{\tau_c s + 1}$

Delay in g only! (setpoint from  $y_s$  to  $y$ )

Get  $\frac{1}{(\tau_1 s + 1)(\tau_2 s + 1) + e^{-(\theta + \theta_m)s}} = \frac{1}{\tau_c s + 1}$   
 $\approx 1 - \theta_{tot} s$  (usual approx.)

$\Rightarrow \frac{(\tau_1 s + 1)(\tau_2 s + 1)}{k C} = (\tau_c + \theta_{tot}) s$

$C = \frac{(\tau_1 s + 1)(\tau_2 s + 1)}{k(\tau_c + \theta_{tot}) s}$

QED