



From state estimation to long horizon MPC for non-linear industrial applications

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- Development of techniques for data reconciliation exploiting a-priori knowledge of process behavior.
- Techniques for state reconstruction of approximate process models.
- Development of MPC techniques enabling broad bandwidth, high performance control along optimal trajectories.
- Integrated implementation of these techniques



Why use estimation/control?



Need control to implement optimal dynamic trajectories

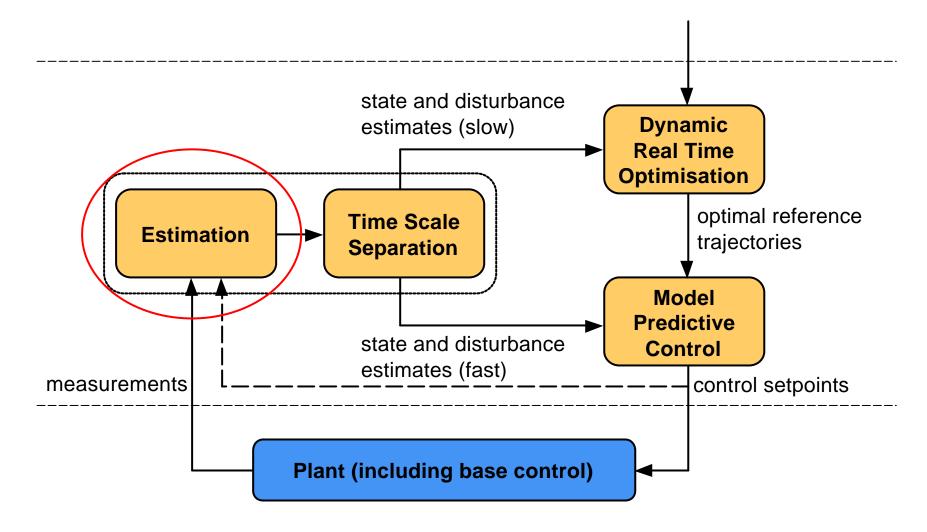
- Disturbances are continuously upsetting the plant
 - actuator/sensor failures
 - set-point changes, feed fluctuations
- There always exists plant-model mismatch
 - uncertain reaction kinetics and physical properties
 - uncertain heat and mass transfer
- The initial conditions are always unknown
 - models suited for production are usually not suited for start-up simulation



Estimation in the INCOOP project Delft TU/e









Purpose of state estimation



Contrary to linear MPC we need to initialize the model

- The input-output behavior depends on the state
 - along grade/load changes considerable change in dynamics
- The output prediction is based on simulation with the nonlinear model starting from an initial state
- Disturbances and uncertain parameters are estimated using the state estimator
 - the disturbance models are dynamic and have their own states



State estimation problem





Set of measurements of process variables:

$$\{y_{k}^{m}, y_{k-1}^{m}, y_{k-2}^{m}, ..., y_{k-N+1}^{m}, y_{k-N}^{m}\}$$

Set of manipulated variables

$$\{u_{k}^{m}, u_{k-1}^{m}, u_{k-2}^{m}, \dots, u_{k-N+1}^{m}, u_{k-N}^{m}, \}$$

Dynamic model (simplified for presentation):

$$\dot{x} = f(x, u, w), \quad x(t_0) = x_0$$
$$y = g(x, u, v)$$



Problem formulation (cont.)



Find the estimate $\hat{x}_{k|k}$ by finding function j, (Cox,64, Lee,95):

$$\hat{x}_{k|k} = \mathbf{j} (y_k^m, ..., y_{k-N}^m, u_{k-1}, ..., u_{k-N}, \hat{x}_{k-N|k-N})$$

minimizing variance on estimation error:

$$J = \Delta \hat{x}_{k-N}^T P_{k-N}^{-1} \Delta \hat{x}_{k-N} + \sum_{i=k-N}^{-1} w_i^T W^{-1} w_i + \sum_{i=k-N}^{-1} v_i^T V^{-1} v_i$$

process disturbance,

• v: measurement noise, covariance:

• $\Delta \hat{x}_{k-N}$ initial state update,

length of data sets

covariance:

covariance:



Extended Kalman Filter



Earlier studies showed ext. Kalman filter (Lewis,86) was:

- easier to tune than horizon estimator
- not less accurate than horizon estimator
- much faster than horizon estimator
- regularizes itself in case of singular covariances

But if used, must adapt for constraints

- do regularization yourself via I/O model reduction
- need QP to find estimate



Extended Kalman Filter



Choice to work recursively:

$$\hat{x}_{k|k} = \mathbf{j}(y_k^m, u_{k-1}, \hat{x}_{k-1|k-1})$$

inear choice for $\hat{\pmb{j}}$! $\hat{x}_{k|k} = \hat{x}_{k|k-1} + K(y_k^m - \hat{y}_{k|k-1})$

Using linear dynamics to propagate variance:

$$\begin{pmatrix} \Delta \dot{x} \\ \Delta y \end{pmatrix} = \begin{pmatrix} A & G \\ C & F \end{pmatrix} \begin{pmatrix} \Delta x \\ \Delta w \end{pmatrix}$$

- X
- W

states (all) disturbances measured outputs
$$\begin{pmatrix} A & B \\ C & D \end{pmatrix} \coloneqq \begin{pmatrix} \frac{\partial f}{\partial x} & \frac{\partial f}{\partial u} \\ \frac{\partial g}{\partial x} & \frac{\partial g}{\partial u} \\ \end{pmatrix}$$



Compute open-loop prediction





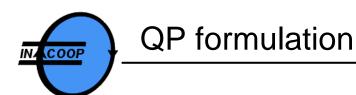
Compute state prediction using nonlinear model, can use any dynamic simulation tool such as GPROMS:

$$\hat{x}_{k+1|k} = \underbrace{F_{Ts}(\hat{x}_{k|k} \mid k, u_k, w_k)}_{\text{model-integration}}$$

$$= \hat{x}_{k|k} + \int_{0}^{Ts} f(x(t), u_k, 0) dt$$

And corresponding output prediction, (automatic)

$$\hat{y}_{k+1|k} = g(\hat{x}_{k+1|k}, u_k)$$





Define output error: $\boldsymbol{e}_k \coloneqq \boldsymbol{y}_k^m - \hat{\boldsymbol{y}}_{k|k-1}$

And arrive at QP:

$$\min_{\Delta \hat{x}_{k-1}, w_{k-1}} \frac{1}{2} \begin{pmatrix} \Delta \hat{x}_{k-1}^T \\ w_{k-1} \end{pmatrix} \begin{pmatrix} P_{k-1}^{-1} & 0 \\ 0 & W^{-1} \end{pmatrix} \begin{pmatrix} \Delta \hat{x}_{k-1} \\ w_{k-1} \end{pmatrix} + v_k^T V^{-1} v_k$$

$$v_k = \mathbf{e}_k - C \Delta \hat{x}_k = \mathbf{e}_k - (CA \quad CB) \begin{pmatrix} \Delta \hat{x}_{k-1} \\ w_{k-1} \end{pmatrix}$$

- can add arbitrary linear constraints on x,w
- must regularize P such that it has inverse
- 'input'-'output' Gramian based model-reduction provides one way (Moore, 76).



Unconstrained solution



Note that unconstrained case:

$$\Delta x_{k} = -H^{-1}g \qquad H = \begin{pmatrix} P_{k-1}^{-1} + A^{T}C^{T}V^{-1}CA & A^{T}C^{T}V^{-1}CB \\ B^{T}C^{T}V^{-1}CA & W^{-1} + B^{T}C^{T}V^{-1}CB \end{pmatrix}$$
$$g = -A^{T}C^{T}V^{-1}\mathbf{e}_{k}$$

compares to familiar Riccati solution:

$$\Delta x_k = K \boldsymbol{e}_k$$

$$P = APA^T - APC^T (CPC'+V)^{-1} CPA + W$$

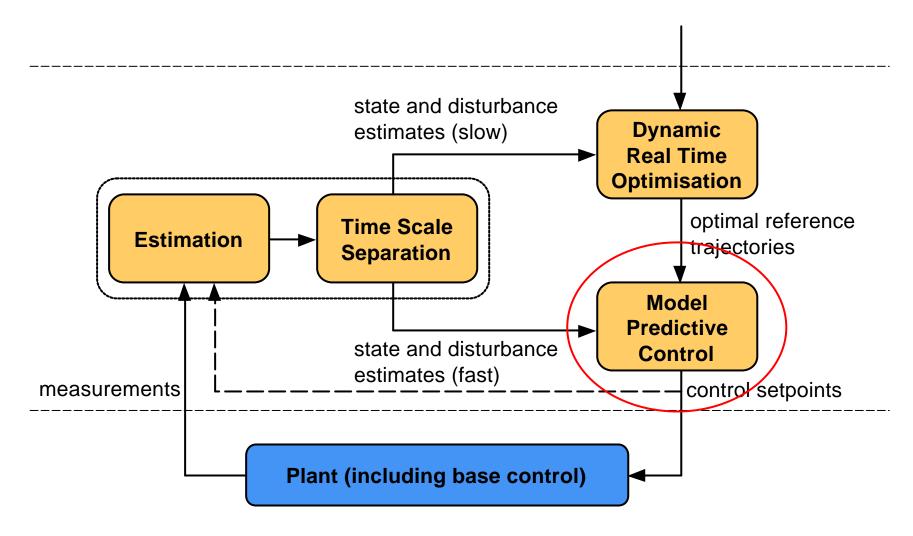
$$K = PC^T (CPC^T + V)^{-1}$$

Note: here only $CPC^T + V$ needs to be invertible!



MPC in the INCOOP project







NMPC problem formulation



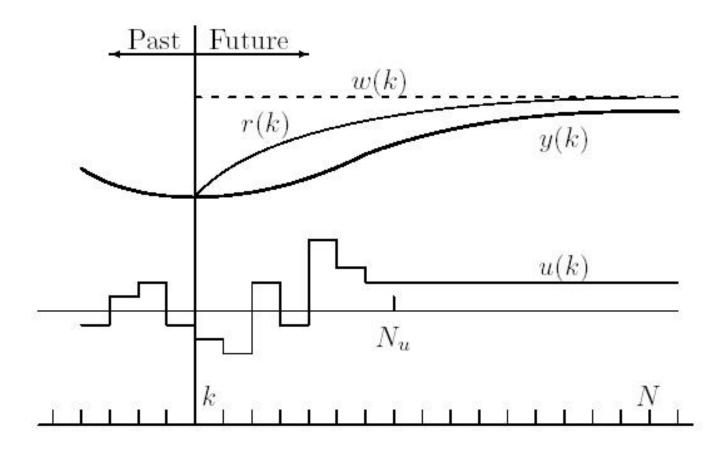
The problem of finding a control sequence for a continuous time plant

$$\dot{x} = f(x, u), x(t_0) = \hat{x}_0$$
$$y = g(x, u)$$

Minimizing some continuous time control objective:

$$J(u) = x(t_f)^T Px(t_f) + \int_{t_0}^{t_f} l(y(t), u(t)) dt$$

One can go many ways!







A full NMPC problem generally much too much time consuming to enable high performance.

Desire small sample time and long prediction horizon!

Approach:

- Discretize continuous time objective (trapezoidal rule)
- Use local dynamics to approx. sensitivity functions:
 Linear Time Varying (LTV) control
- Very reliable for proper choice of sample time
- Much faster for many of optimization variables
- After a few iterations you get `SQP' behaviour



Linear-Time-Varying MPC





Integrate nonlinear model along previous input sequence: gives output and state predictions:

$$\{y_k^{pred}, y_{k+1}^{pred}, ..., y_{k+N}^{pred}\}, \{x_k^{pred}, x_{k+1}^{pred}, ..., x_{k+N}^{pred}\}$$

 Derive linear time varying (LTV) model along this trajectory (time-discretize local dynamics)

$$\delta y = G_{U} \delta u, \ \delta u = (\delta u_{k}, ..., \delta u_{k+N-1})^{T}$$

$$G_{U} = \begin{pmatrix} D_{k} & 0 & ... & ... \\ C_{k+1} B_{k} & D_{k+1} & 0 & ... \\ C_{k+2} A_{k+1} B_{k} & C_{k+2} B_{k+1} & D_{k+2} & 0 \\ C_{...} A_{...} A_{...} B_{...} & C_{...} A_{...} B_{...} & C_{...} B_{...} & ... \end{pmatrix}$$



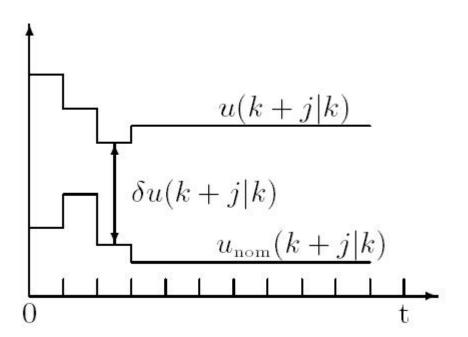
Optimizing control input





Optimizing control inputs:

$$\delta u_{k+j|k} = u_{k+j|k} - u_{k+j|k}^{nom}$$



An effective choice for the nominal control input:

$$u_{k+j|k}^{nom} = u_{k+j|k-1}^{opt}$$





•LTV-MPC problem amounts to find an optimal control sequence $\{u(k+j)\}_{j=1}^{N-1}$ minimizing the objective function:

$$J_{k} = x_{k+N}^{T} P x_{k+N} + \sum_{j=1}^{N} \begin{pmatrix} y_{k+j}^{pred} - y_{k+j}^{ref} \\ u_{k+j}^{pred} - u_{k+j-1}^{pred} \end{pmatrix}^{T} \begin{pmatrix} Q & 0 \\ 0 & R \end{pmatrix} \begin{pmatrix} y_{k+j}^{pred} - y_{k+j}^{ref} \\ u_{k+j}^{pred} - u_{k+j-1}^{pred} \end{pmatrix}^{T}$$

subject to constraints:

$$y_{\min} \le y(k+j) \le y_{\max}$$

$$u_{\min} \le u(k+j) \le u_{\max}$$

$$\Delta u_{\min} \le \Delta u(k+j) \le \Delta u_{\max}$$

$$j = 0, ..., N$$



Nominal control input concept





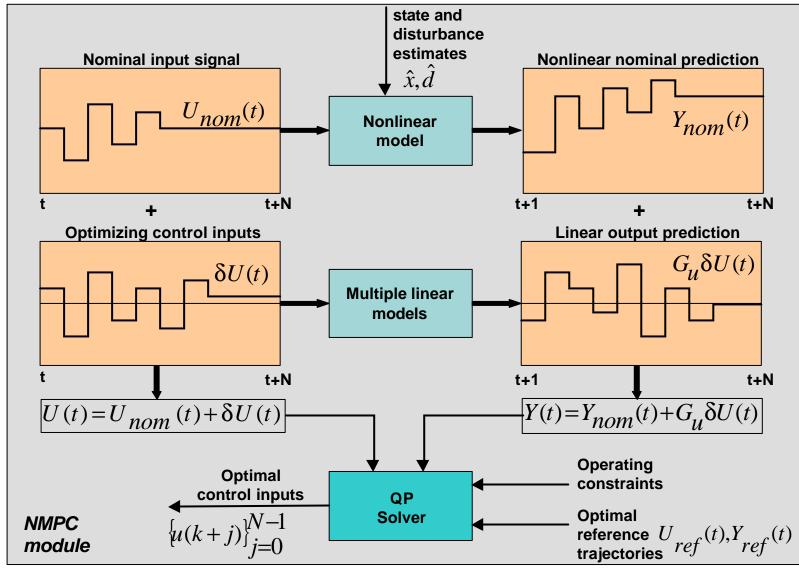
 Then solve resulting QP and add solution to previous control sequence:

$$u_{k+j}^{pred} = u_{k+j}^{nom} + \delta u_{k+j}$$



Nonlinear MPC





Outlook



Standard QP solvers: •Active Set Methods

(ASM)

State variables are

eliminated •Interior-Point Methods

(IPM): Mosek, etc.

Computational time increases with the 3^{rd} power of the number of variables Nn_u

Structured IPM:

State variables are *not* eliminated

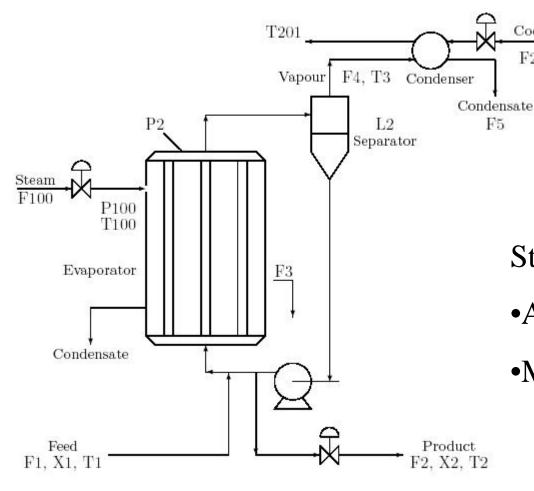
Computational time increases linearly with the number of variables

-> Allows long horizon prediction/ large bandwidth



Example: Evaporation process





3 MVs:

 F_2, P_{100}, F_{200}

Structured IPM is faster than

•ASM for N > 25

Cooling water

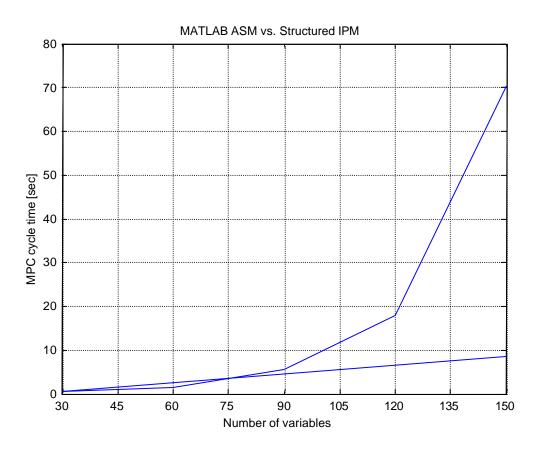
F200, T200

•Mosek for N > 160



Evaporation process results







Example 2: Distillation process





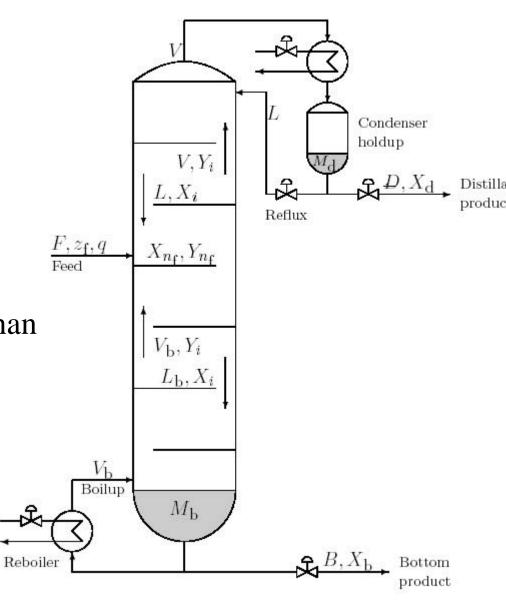
2 MVs:

Reflux L

Boilup

Structured IPM is faster than

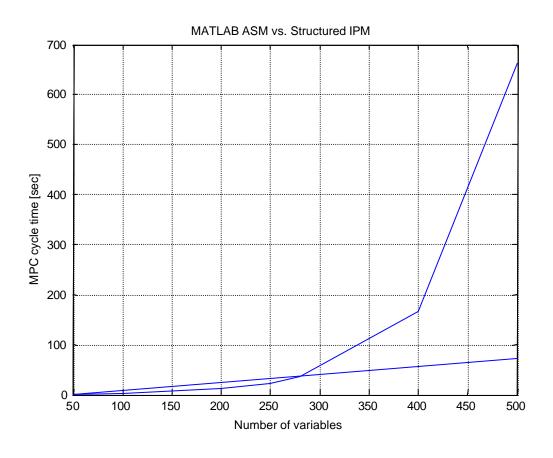
ASM for N > 140

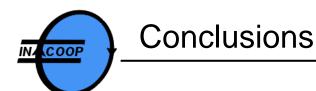




Distillation process results









- Estimator+MPC have been implemented within INCOOP software architecture.
- Tested and operative for both Bayer and Shell process.
- For large scale problems QP computation time is no longer a bottleneck. Model simulation (MPC prediction) is the main computational burden in the environment.