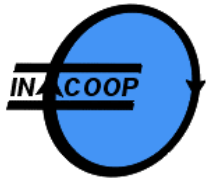


Dynamic Real-time Optimization

Jitendra Kadam, Wolfgang Marquardt, Martin Schlegel
Lehrstuhl für Prozesstechnik
RWTH Aachen

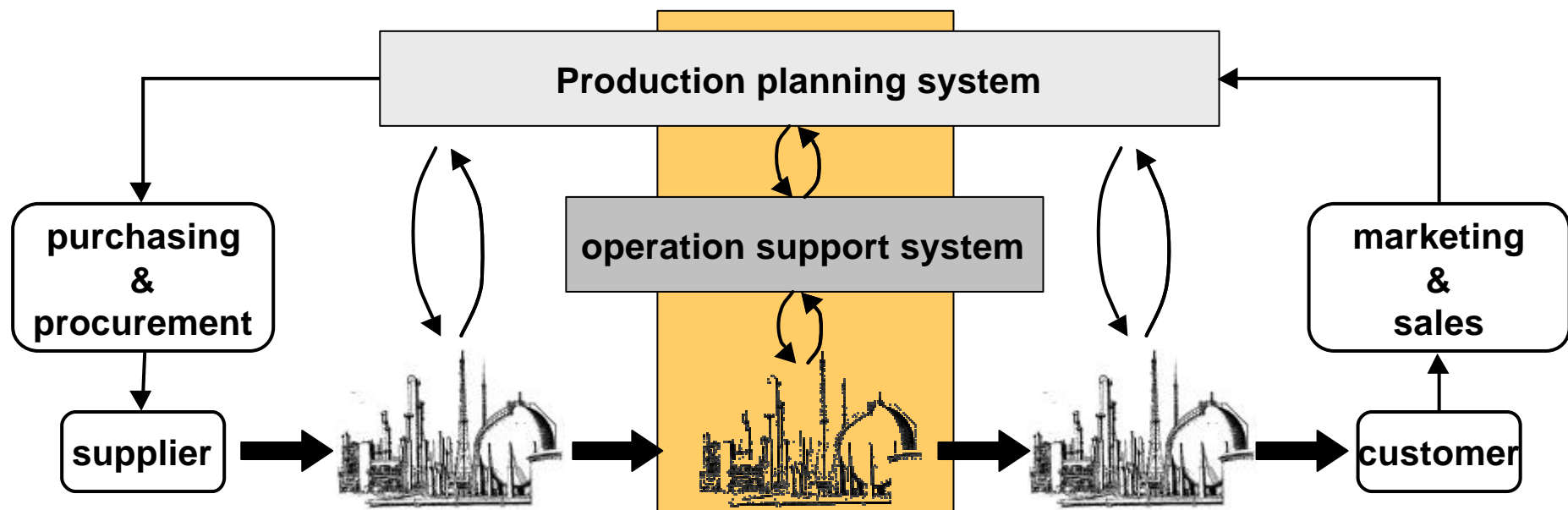
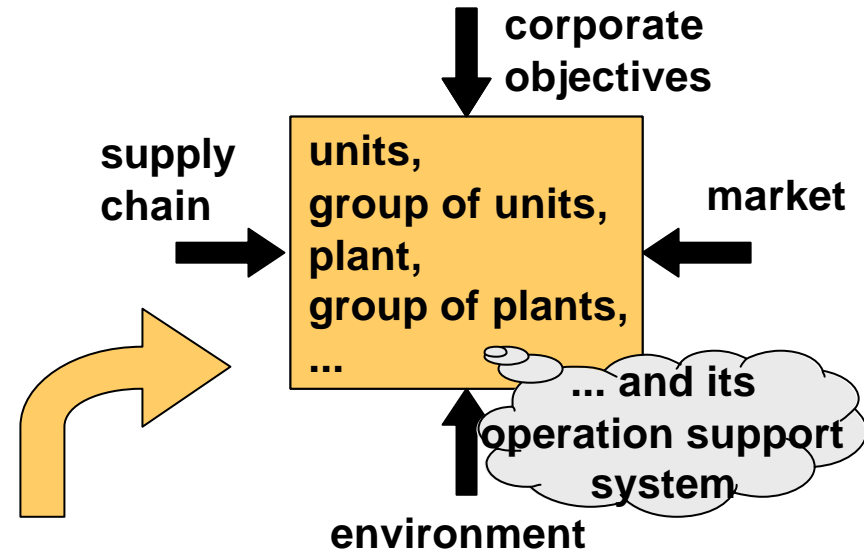
INCOOP Workshop
Düsseldorf, January 23 – 24, 2003

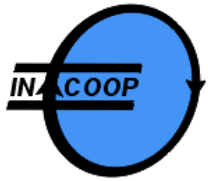


Operational strategies – the status

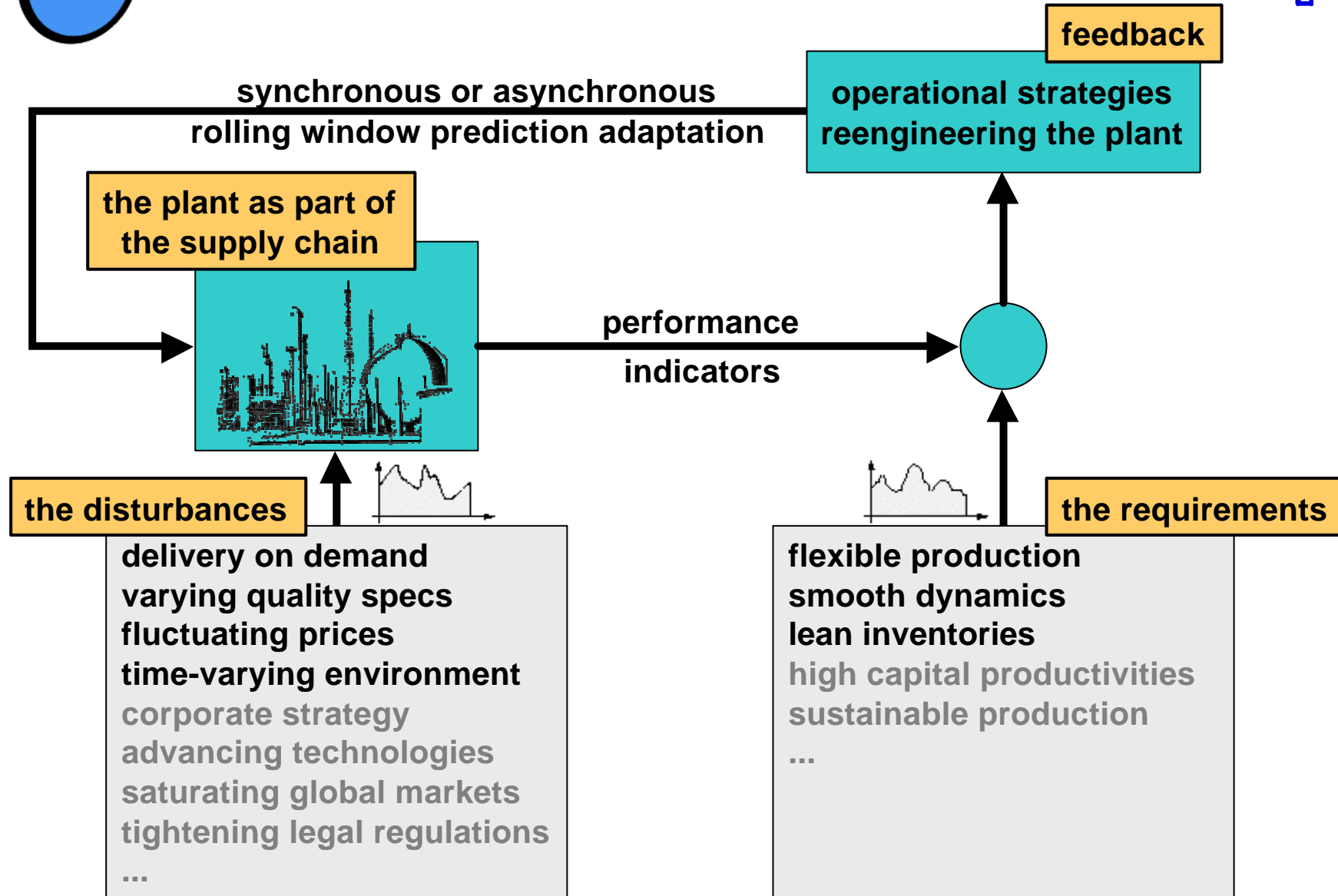


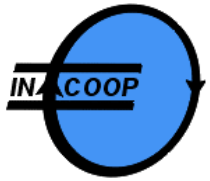
- plant in isolation
- steady-state operation
- limited flexibility
- disturbance handling
- largely autonomous



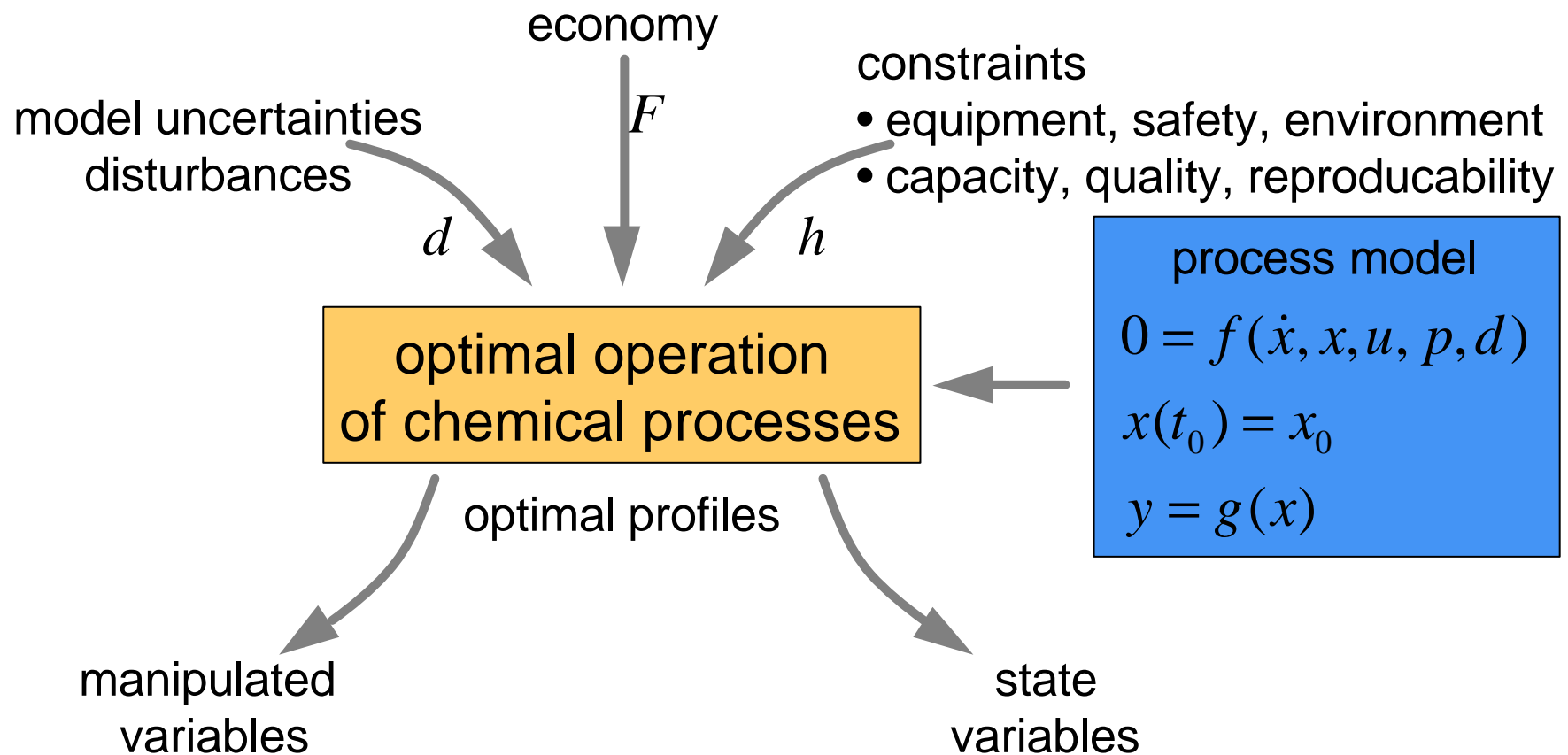


Manufacturing in the future

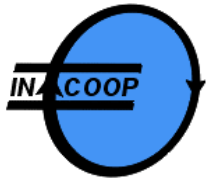




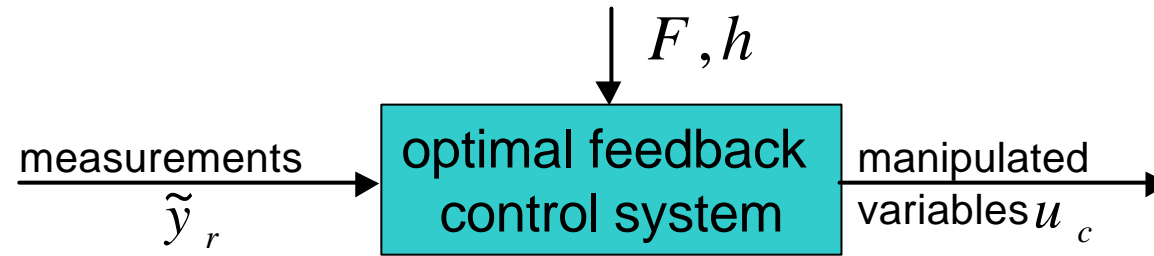
General operational objectives



Why should they be constant over time?



Optimization-based control



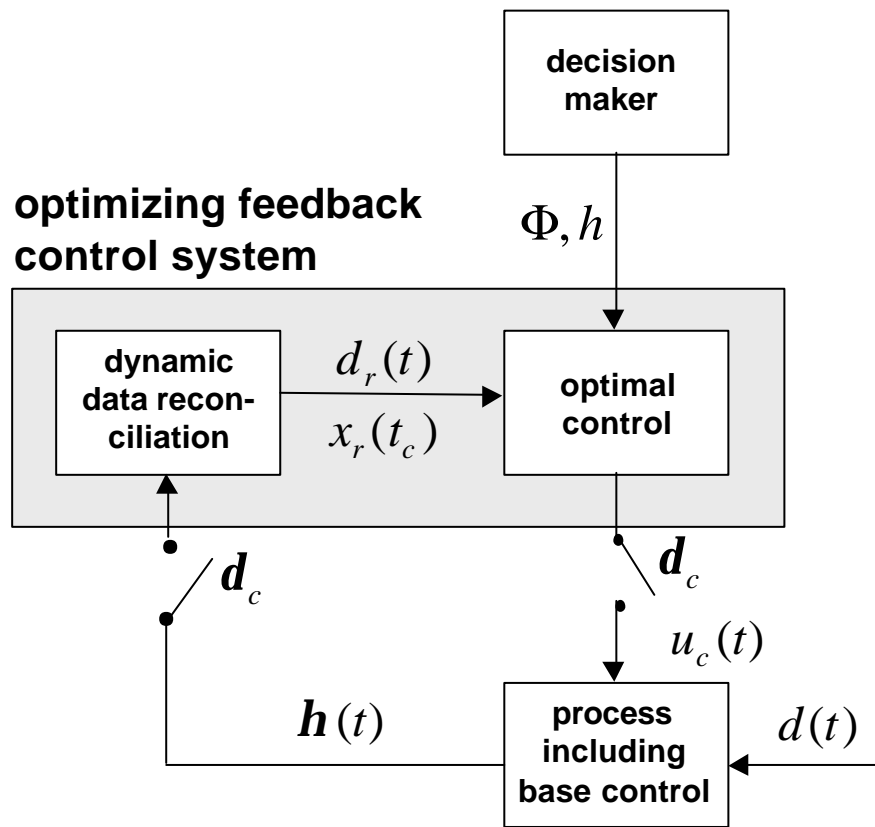
2 coupled problems:

dynamic data reconciliation

$$\begin{aligned} & \min_{x_{r,0}, d_r} \Phi_r(y_r, \mathbf{h}, x_{r,0}, d_r, t_c, t_f) \\ \text{s.t.} \quad & 0 = f(\dot{x}_r, x_r, u_r, d_r) \\ & y_r = g(x_r) \\ & x_r(t_r) = x_{r,0} \\ & u_r = U(u_c(\cdot)) \\ & 0 \geq h_r(x_r, d_r) \\ & t \in [t_r, t_c] \end{aligned}$$

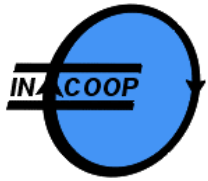
optimal control

$$\begin{aligned} & \min_{u_c} \Phi_c(x_c, u_c, t_c, t_f) \\ \text{s.t.} \quad & 0 = f(\dot{x}_c, x_c, u_c, d_c) \\ & y_c = g(x_c) \\ & x_c(t_c) = x_r(t_c) \\ & d_c = D(d_r(\cdot)) \\ & 0 \geq h_c(x_c, u_c) \\ & t \in [t_c, t_f] \end{aligned}$$

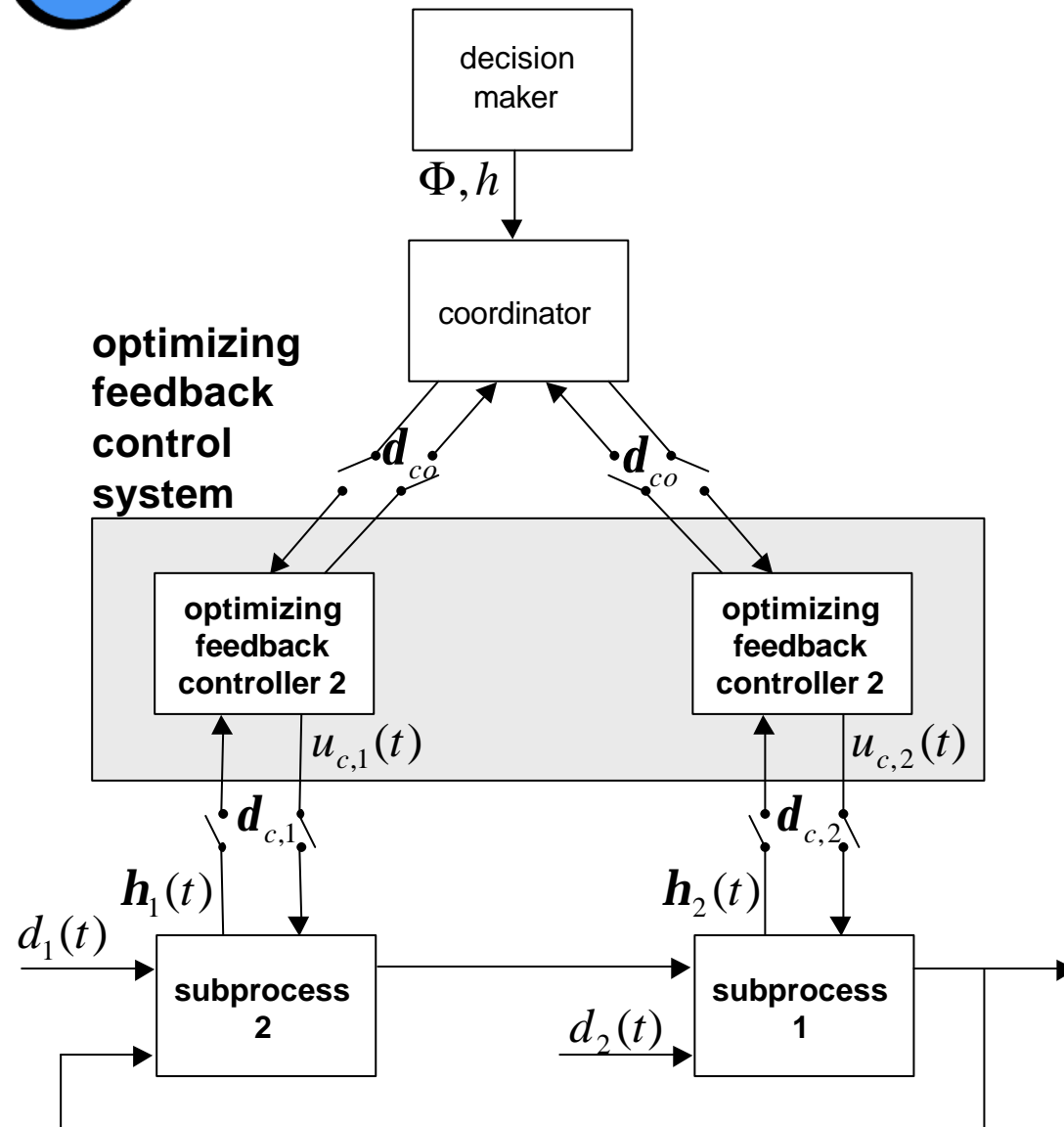


- solution of optimal control reconciliation problems at controller sampling frequency
- computationally demanding
- model complexity limited (INACOOP benchmarks ⇒ large models!)
- lack of transparency, redundancy and reliability

(Terwiesch et al., 1994;
 Helbig et al., 1998;
 Wisniewski & Doyle, 1996;
 Biegler & Sentoni, 2000)

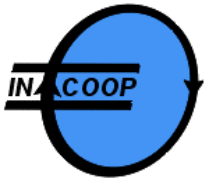


Horizontal decomposition

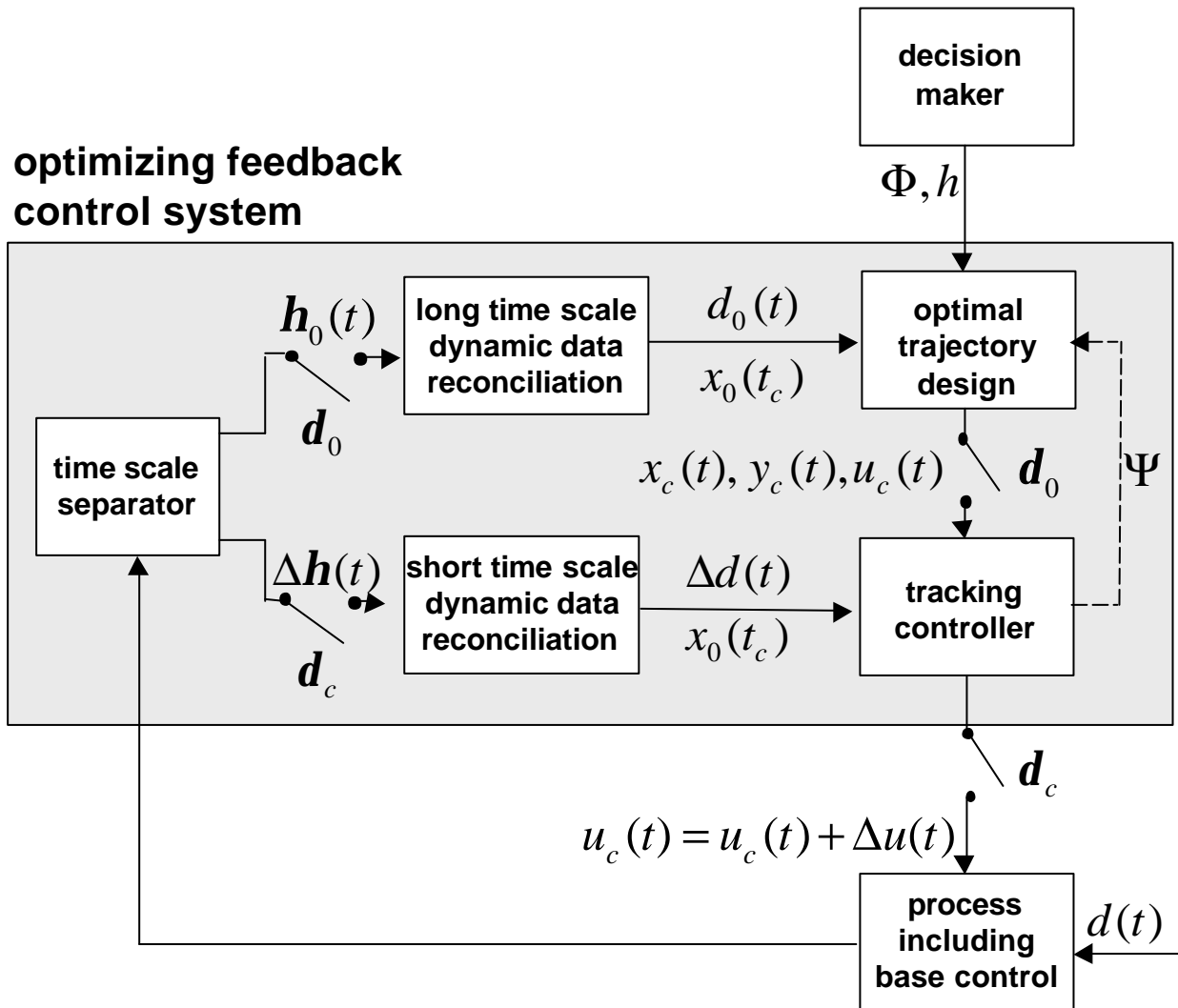


- decentralization typically oriented at functional constituents of the plant
- coordination strategies enable approximation of "true" optimum
- not adequately covered in optimization-based control and operations yet

(Mesarovic et al., 1970;
Findeisen et al., 1980;
Morari et al., 1980;
Lu, 2000)

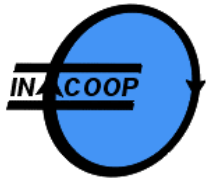


Vertical decomposition



- generalizes steady-state real-time optimization and constrained predictive control

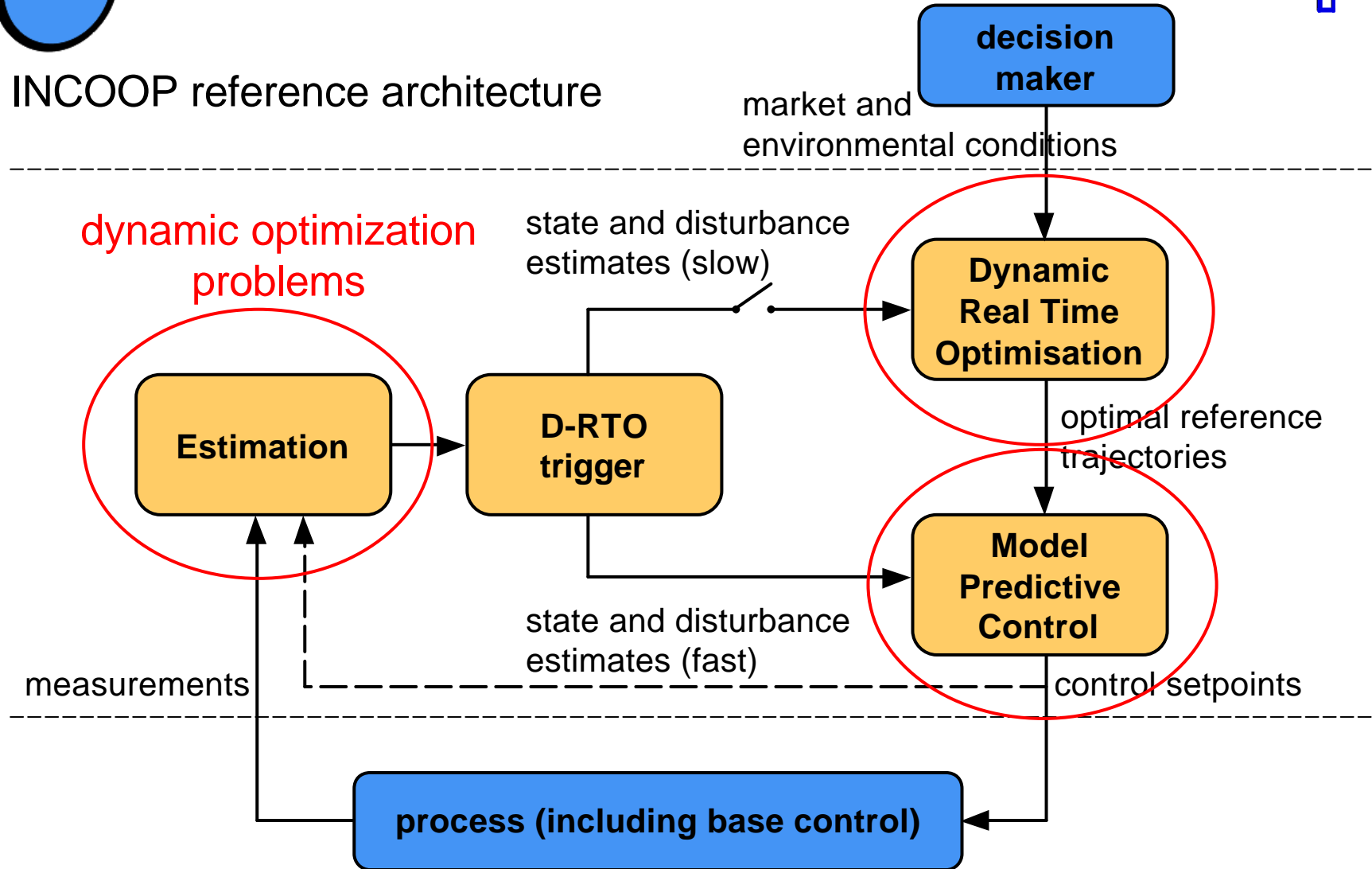
- requires (multiple) time-scale separation, e.g.
 $d(t) = d_0(t) + \Delta d(t)$
with
trend $d_0(t)$
zero mean fluctuation $\Delta d(t)$

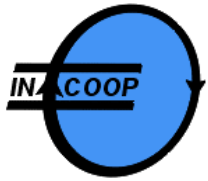


Vertical decomposition – INCOOP approach

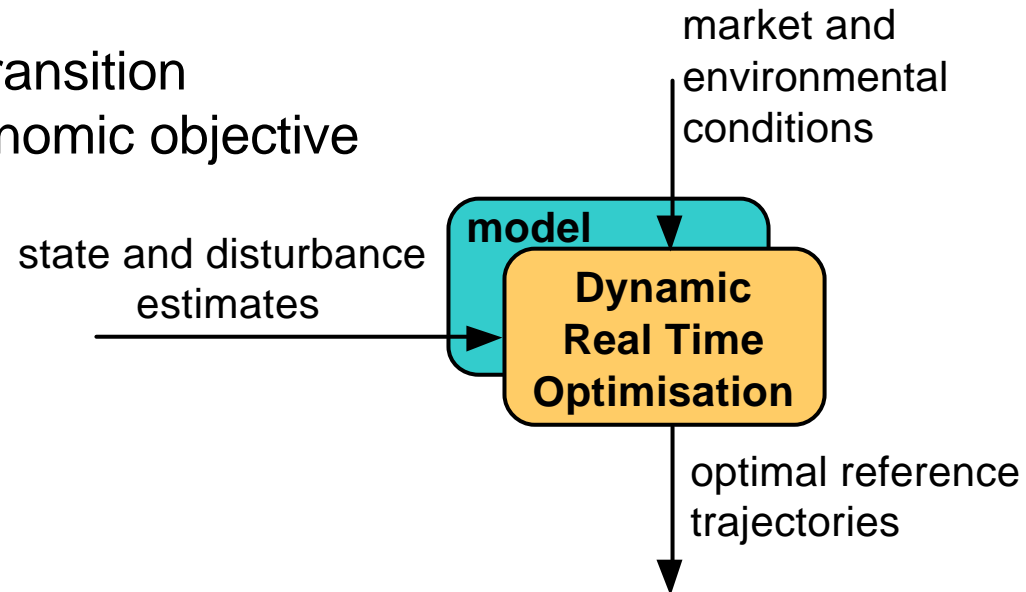


INCOOP reference architecture



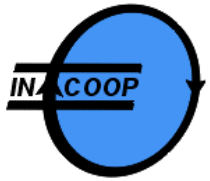


Goal: determine optimal transition trajectories using an economic objective function



Challenges:

- Develop numerical **solution methods** which solve the problem robustly and sufficiently fast
- Develop techniques for **triggering a re-optimization** based on external conditions
- Implement **software framework** for enabling interaction with MPC and estimator



Mathematical problem formulation

$$\min_{u(t), p, t_f} \Phi(x(t_f)) \quad \text{objective function (e.g. cost)}$$

s.t.

$$\left. \begin{aligned} M \dot{x} &= F(x, u, p, t), & t \in [t_0, t_f], \\ 0 &= x(t_0) - x_0, \end{aligned} \right\} \text{DAE system (process model)}$$

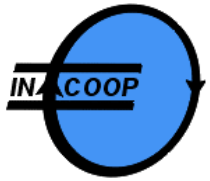
$$0 \geq P(x, u, p, t), \quad t \in [t_0, t_f], \quad \text{path constraints (e.g. temp. bound)}$$

$$0 \geq E(x(t_f)) \quad \text{endpoint constraints (e.g. prod. spec.)}$$

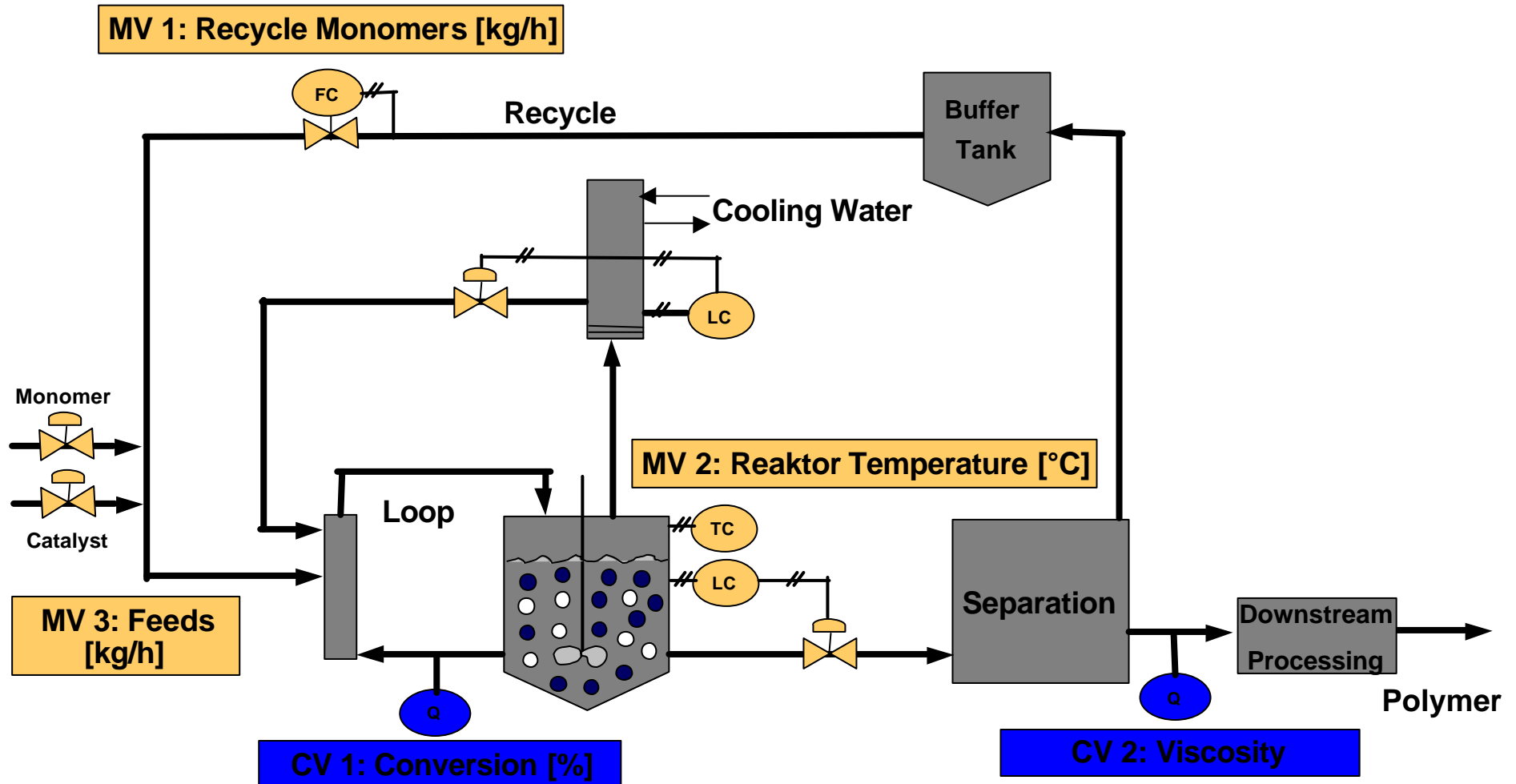
Degrees of freedom: $u(t)$ time-variant control variables

p time-invariant parameters

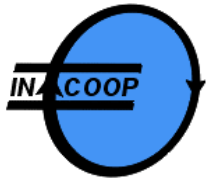
t_f final time



Example: Bayer Benchmark Process (I)



(From: Dünnebier & Klatt: Industrial challenges and requirements for optimization of polymerisation processes)
Dynamic real-time optimization

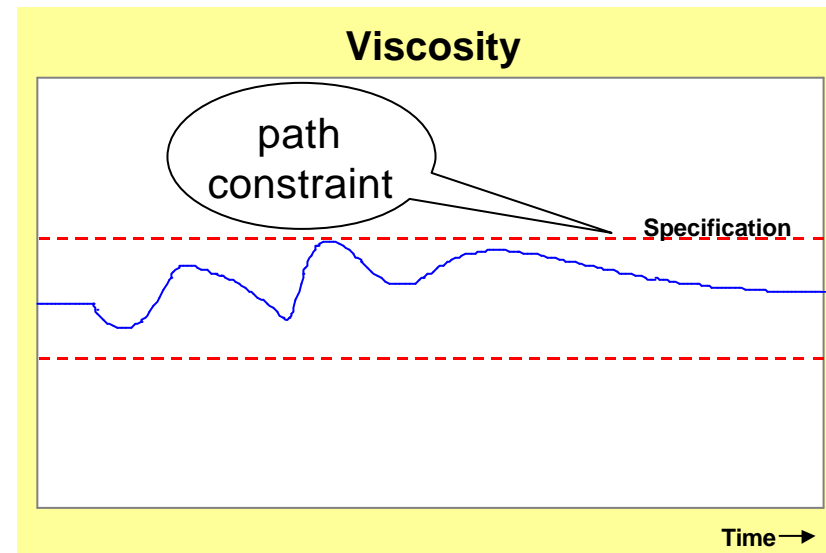
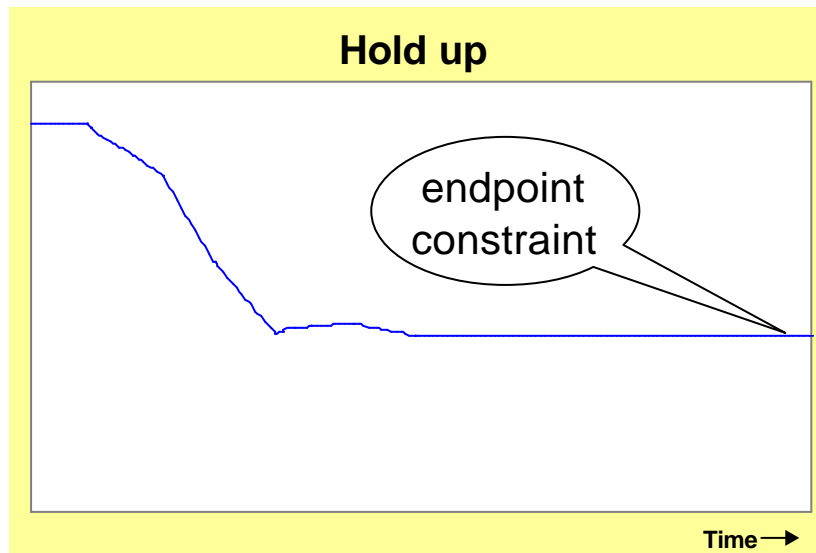
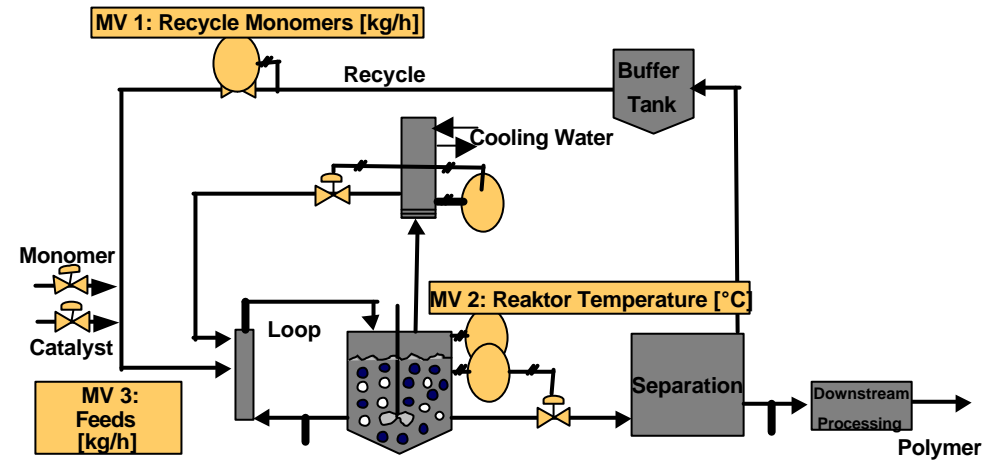


Example: Bayer Benchmark Process (II)

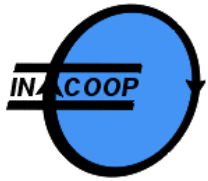


Polymerization process

- minimize time for load change
- three degrees of freedom
- path constraints on specifications



(From: Dünnebier & Klatt: Industrial challenges and requirements for optimization of polymerisation processes)
Dynamic real-time optimization



Indirect solution methods

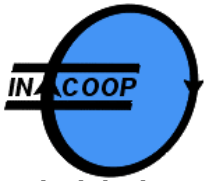
Necessary optimality conditions lead to multipoint boundary value problems:

- Highly accurate solutions with shooting techniques.
- Solution requires detailed a-priori knowledge of the optimal solution structure and appropriate estimates for adjoint variables.

Direct solution methods

Conversion of dynamic optimization problem into nonlinear programming problem (NLP) by discretization...

- ...of state and control variables.
(simultaneous method, i.e. collocation, multiple shooting)
used in INCOOP
- ...of control variables only.
(sequential method, i.e. single shooting)
- Successfully applied with large-scale process models



Solution algorithm



initial values: u^0, p^0, t_f^0
specify Φ, P, E

Discretization

$$z^0 = \{c^0, p^0, t_f^0\}$$

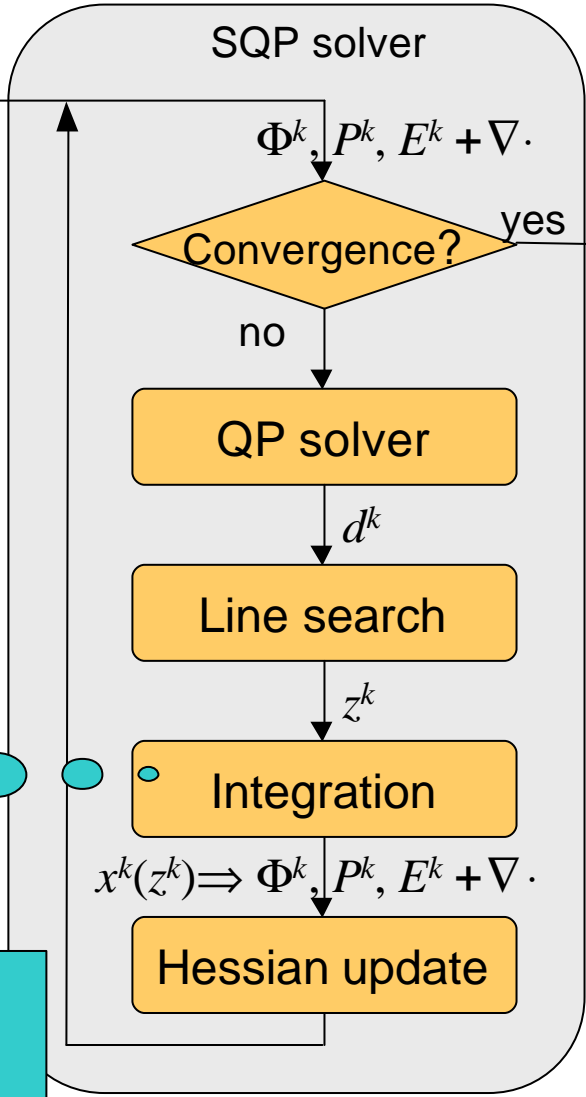
Integration

$$x^0(z^0) \Rightarrow \Phi^0, P^0, E^0$$
$$s^0(z^0) \Rightarrow \nabla\Phi^0, \nabla P^0, \nabla E^0$$

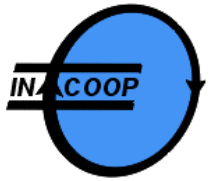
expensive!
> 90 % of CPU time

Potential improvements:

- most efficient integration
- as few NLP steps as possible



optimal solution:
 $c^*, p^*, t_f^*, \Phi^*, P^*, E^*$
optimal trajectories:
 $u(t), x(t)$

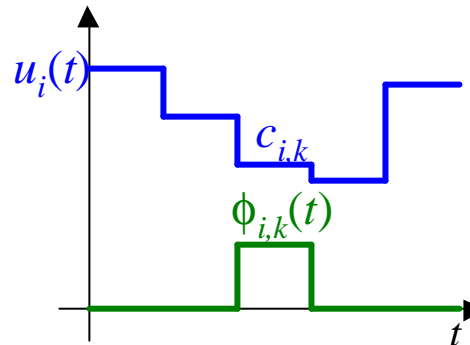


Sequential approach → single shooting



Control vector parameterization

$$u_i(t) \approx \sum_{k \in \Lambda_i} c_{i,k} \mathbf{f}_{i,k}(t)$$



$\mathbf{f}_{i,k}(t)$ parameterization functions

$c_{i,k}$ parameters

⇒ Reformulation as nonlinear programming problem (NLP)

$$\min_{c,p,t_f} \Phi(x(c,p,t_f))$$

$$\text{s.t.} \quad 0 \geq P(x,c,p,t_i), \quad \forall t_i \in T,$$

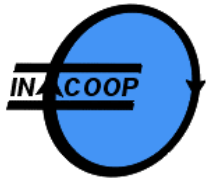
$$\cdot \quad 0 \geq E(x(t_f))$$

DAE system solved by underlying numerical integration

- DAE system solved by underlying numerical integration
- Gradients for NLP solver typically obtained by integration of sensitivity systems

⇒ Numerical integration computationally most expensive (> 90 % of CPU time)

⇒ Computational effort strongly depends on size and complexity of process model



Sensitivity integration is expensive

State integration is expensive

Improve efficiency of sensitivity integration

Reduce number of sensitivity parameters

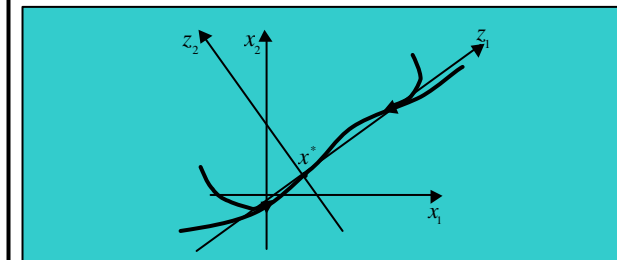
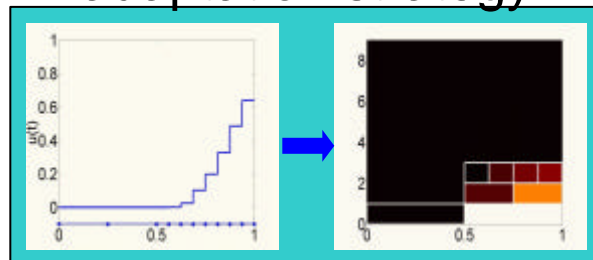
Reduce model complexity

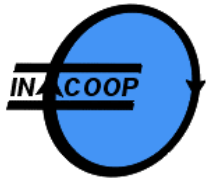
New solver for sensitivity integration

Control grid adaptation strategy

Methods for model reduction

$$X_{k+1} = X_k - \begin{bmatrix} A - \frac{M}{h_j} & & & & \\ & A_1 & A - \frac{M}{h_j} & & \\ & \vdots & \ddots & \ddots & \\ & A_{n_z} & & & A - \frac{M}{h_j} \end{bmatrix}^{-1} f(X_k, z)$$





Dynamic optimization problem:

$$\begin{aligned} & \min_z \Phi(x, z, t) \\ \text{s.t. } & M \dot{x} = f(t, x, z) \\ & 0 = x(t_0) - x_0 \\ & 0 \geq P(x, z, t) \\ & 0 \geq E(x(t_f)) \end{aligned}$$

$\frac{\partial}{\partial z}$ \rightarrow

$z = \{c, p, t_f\}$

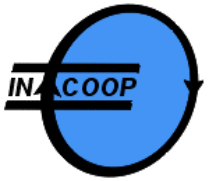
$$M \dot{s} = \begin{pmatrix} \frac{\partial f}{\partial x} \end{pmatrix} s_i + \frac{\partial f}{\partial z_i} \quad i = 1, \dots, n_z$$

Typical solution approaches based on BDF-type integrators

- Caracotsios & Stewart (1985), Maly & Petzold (1996), Feehery et al. (1997)

New idea: Use one-step extrapolation method

- Based on LIMEX algorithm (Deuffhard et al. (1983,87))
- Extension for sensitivity computation: Schlegel et al. (2002)



Combined state and sensitivity system



$$M \dot{x} = F(x, z, t)$$

$$M \dot{s}_i = \underbrace{\left(\frac{\partial F}{\partial x} \right)}_{=: A} s_i + \frac{\partial F}{\partial z_i} \quad i = 1, \dots, n_z$$

$$M \dot{X} = f(X, z, t)$$

$$\text{with } X = [x, s_1, \dots, s_{n_z}]^T$$

Efficient solution of the combined system

- M is identical in both systems.
- A is already required for state integration.

Linear-implicit Euler discretization

$$X_{k+1} = X_k -$$

$$\left[A - \frac{M}{h_j} \right]$$

$$\begin{bmatrix} A_1 \\ \vdots \\ A_{n_z} \end{bmatrix}$$

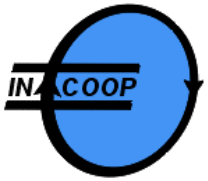
$$A - \frac{M}{h_j}$$

$$A - \frac{M}{h_j}$$

$$f(X_k, z)$$

neglect off-diagonal elements

Reuse LU decomposition



Solution algorithm



Extrapolation algorithm for simultaneous state and sensitivity integration

Compute $A_0 = \frac{\partial}{\partial y}(f(y_0, p))$

for $j=1, \dots, j_{max}$ while convergence criterion not satisfied

$$h_j = H / j$$

$$LU = A_0 - \frac{B}{h_j}$$

for $k=0, \dots, j-1$

$$y_{k+1} = y_k - (LU)^{-1} f(y_k, p)$$

$$s_{i,k+1} = s_{i,k} - (LU)^{-1} \left(A(y_k) s_{i,k} + \frac{\partial f}{\partial p_i}(y_k) \right) \quad i = 1, \dots, n_z$$

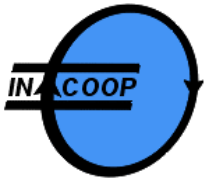
$$T_{j,1} = Y_j$$

if $j > 1$ compute $T_{j,j}$ and check convergence

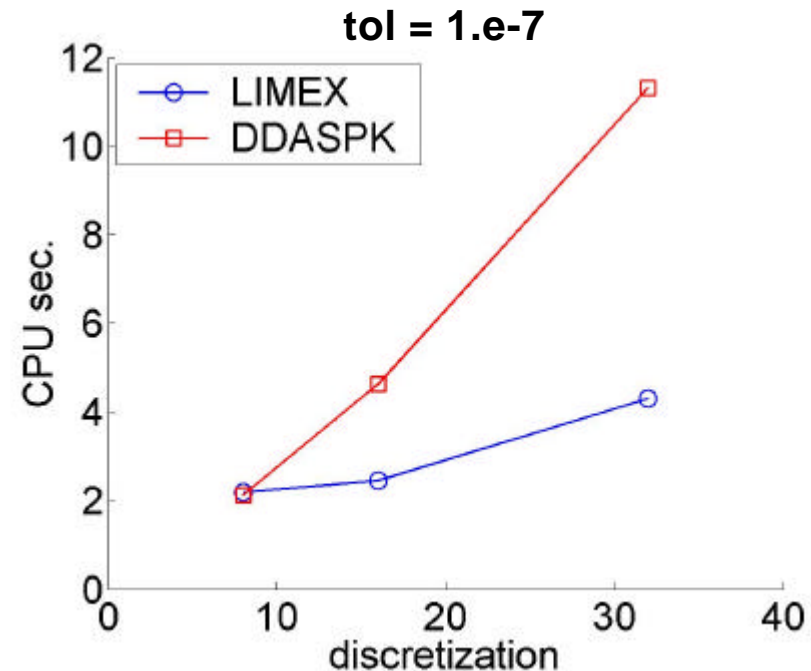
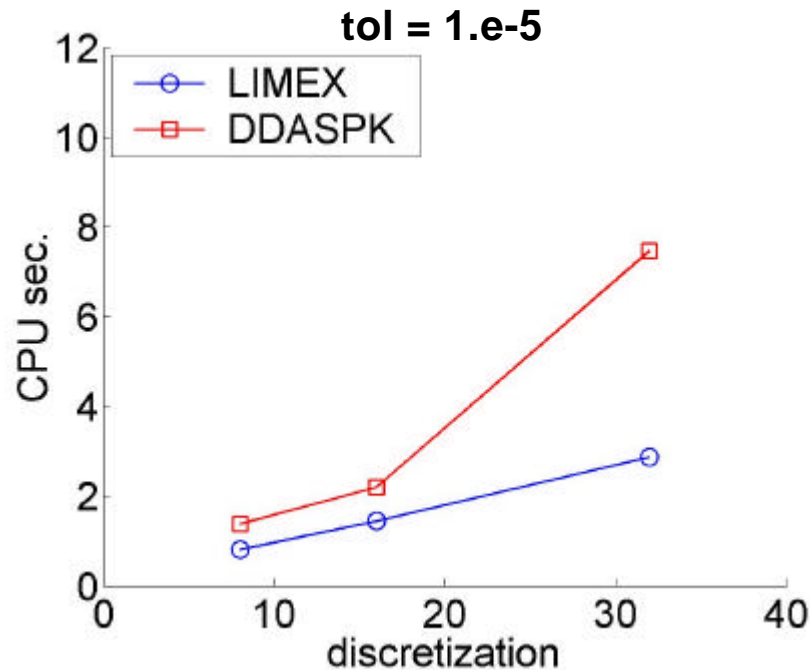
$$X_{new} = X_{j,j}$$



(here simplified for $M = \text{const.}$)



Small example problem, solved for two different tolerances



⇒ One-step extrapolation faster than multistep BDF with increasing level of discretization

⇒ Used as standard for optimization of INCOOP benchmark problems

Sensitivity integration
is expensive

State integration
is expensive

Improve efficiency
of sensitivity integration

Reduce number
of sensitivity parameters

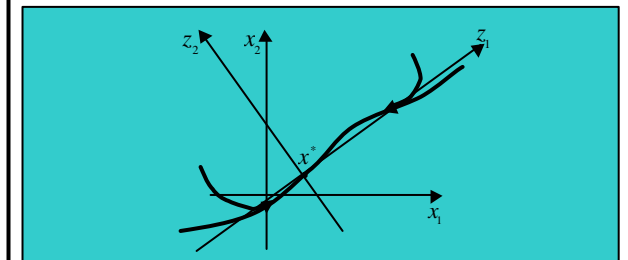
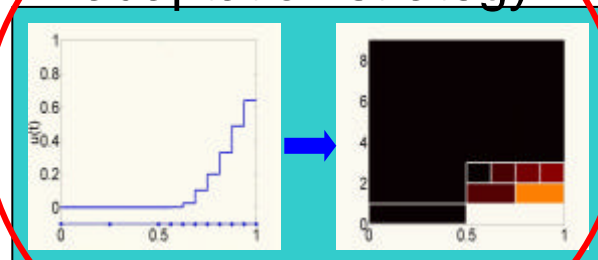
Reduce
model complexity

New solver for
sensitivity integration

Control grid
adaptation strategy

Methods for
model reduction

$$X_{k+1} = X_k - \begin{bmatrix} A - \frac{M}{h_j} & & & \\ & A_1 & A - \frac{M}{h_j} & \\ & \vdots & \ddots & \\ & A_{n_z} & & A - \frac{M}{h_j} \end{bmatrix}^{-1} f(X_k, z)$$



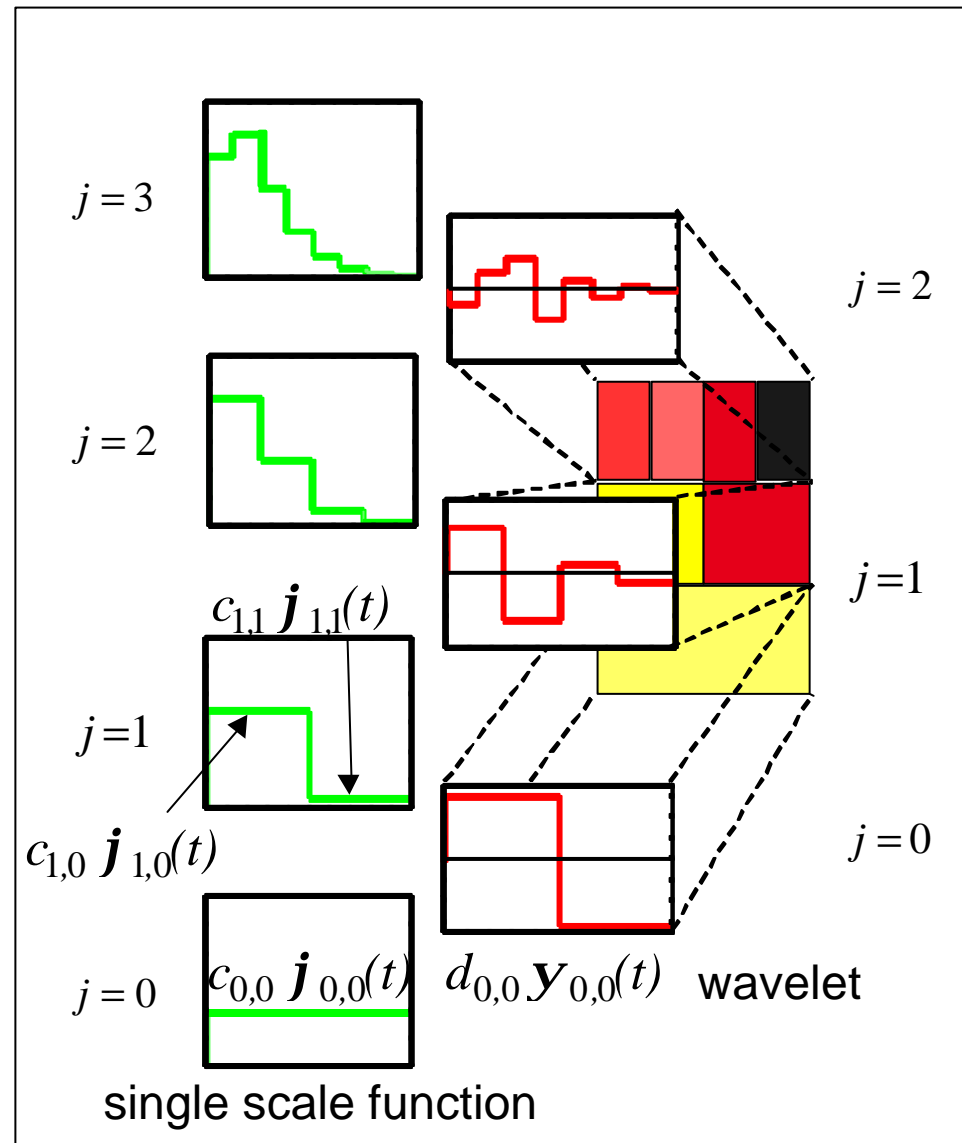
Different **representations** of the **same function** ...

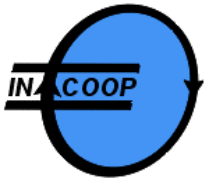
... for problem discretization:

$$u = \sum_{(j,k) \in \Lambda_j} c_{j,k} \mathbf{j}_{j,k}(t)$$

... for grid point elimination analysis:

$$u = c_{0,0} \mathbf{j}_{0,0}(t) + \sum_{(j,k) \in \Lambda_y} d_{j,k} \mathbf{y}_{j,k}(t)$$



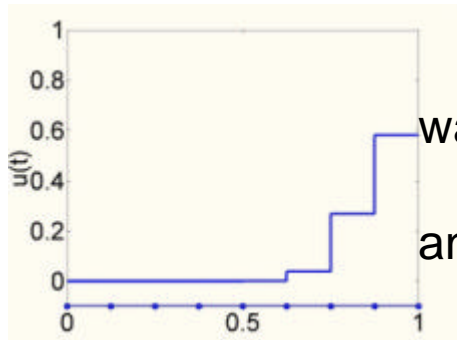


Adaptive refinement algorithm



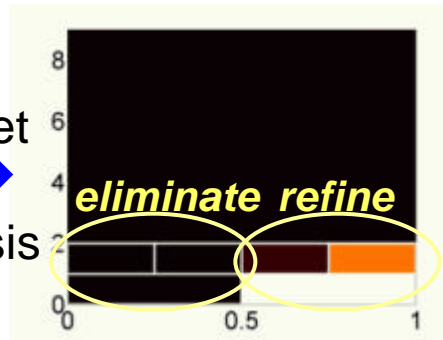
Mesh analysis

- Concepts from signal analysis
- Grid point elimination
- Grid point insertion

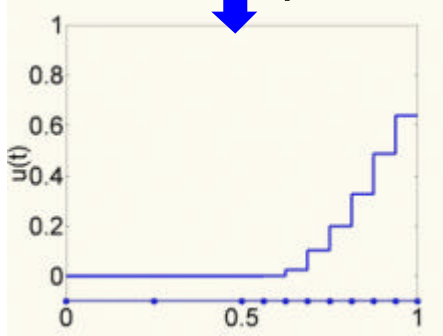


coarse initial mesh

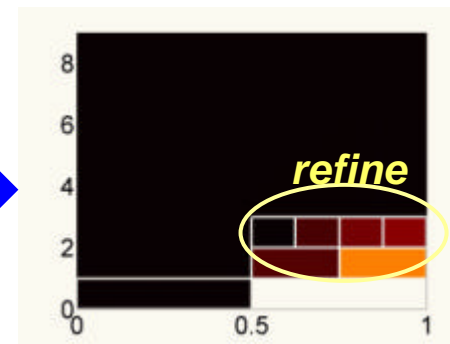
wavelet
analysis



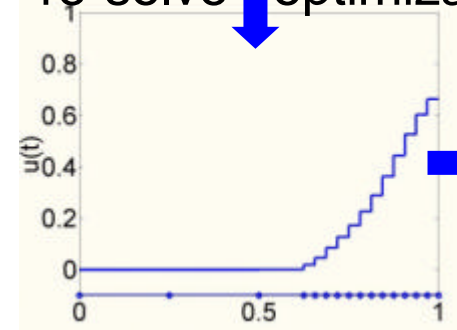
re-solve optimization



→



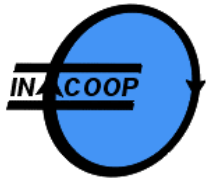
re-solve optimization



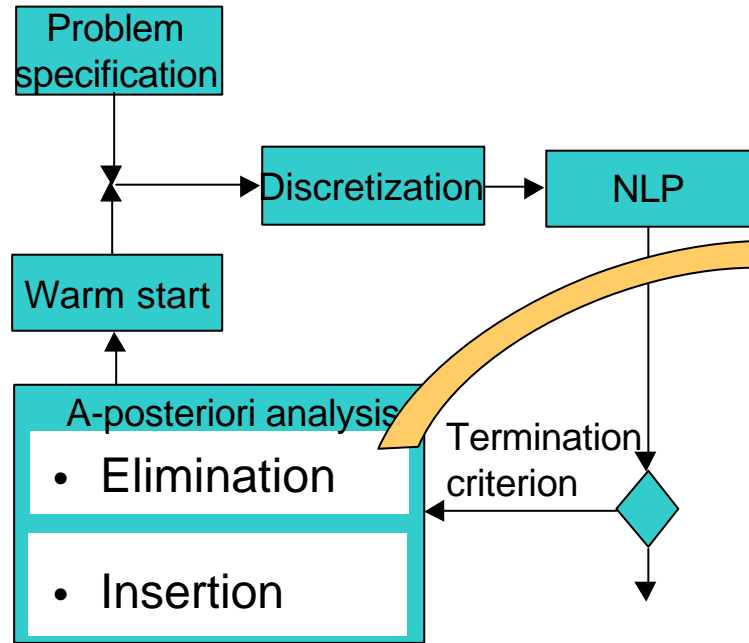
→ until
stopping
criterion
met.

Repetitive procedure

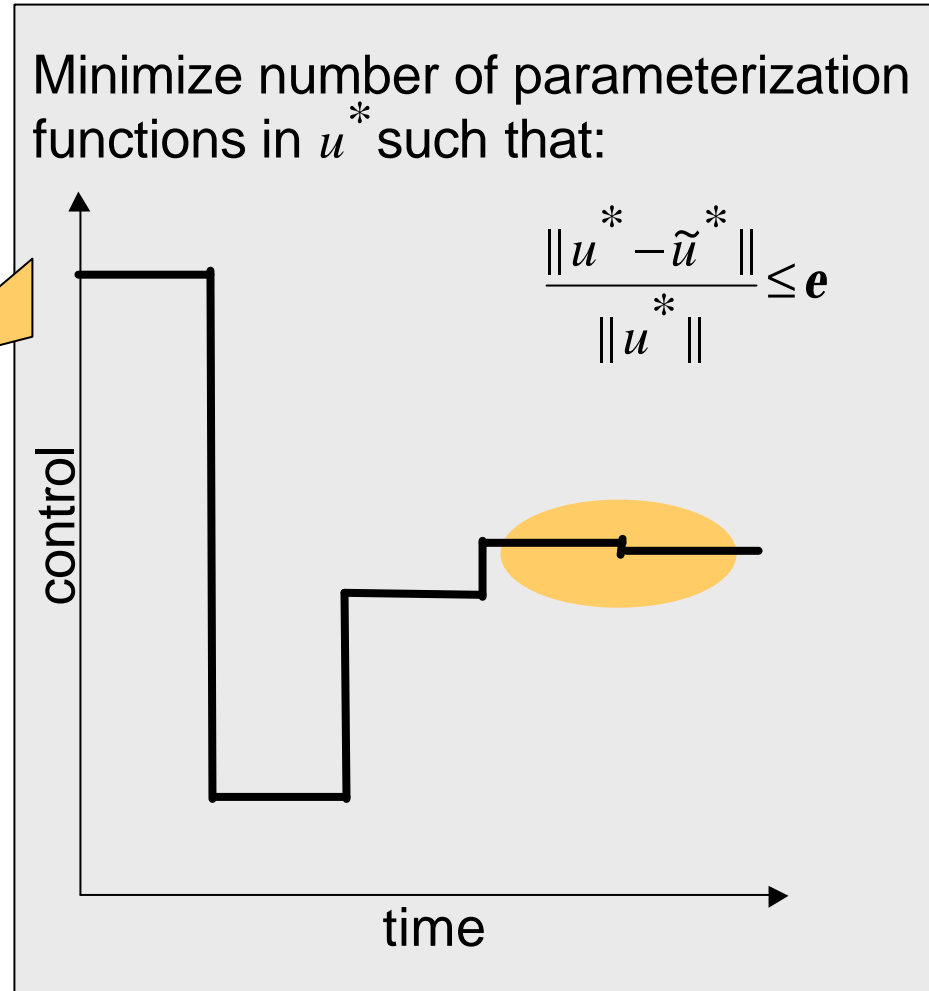
- Re-optimize problem on refined mesh
- Profile from previous solution as initial guess
- Decouple optimization and adaptation



Elimination of parameterization functions



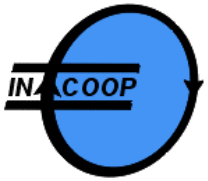
Analysis of wavelet coefficients of control variables



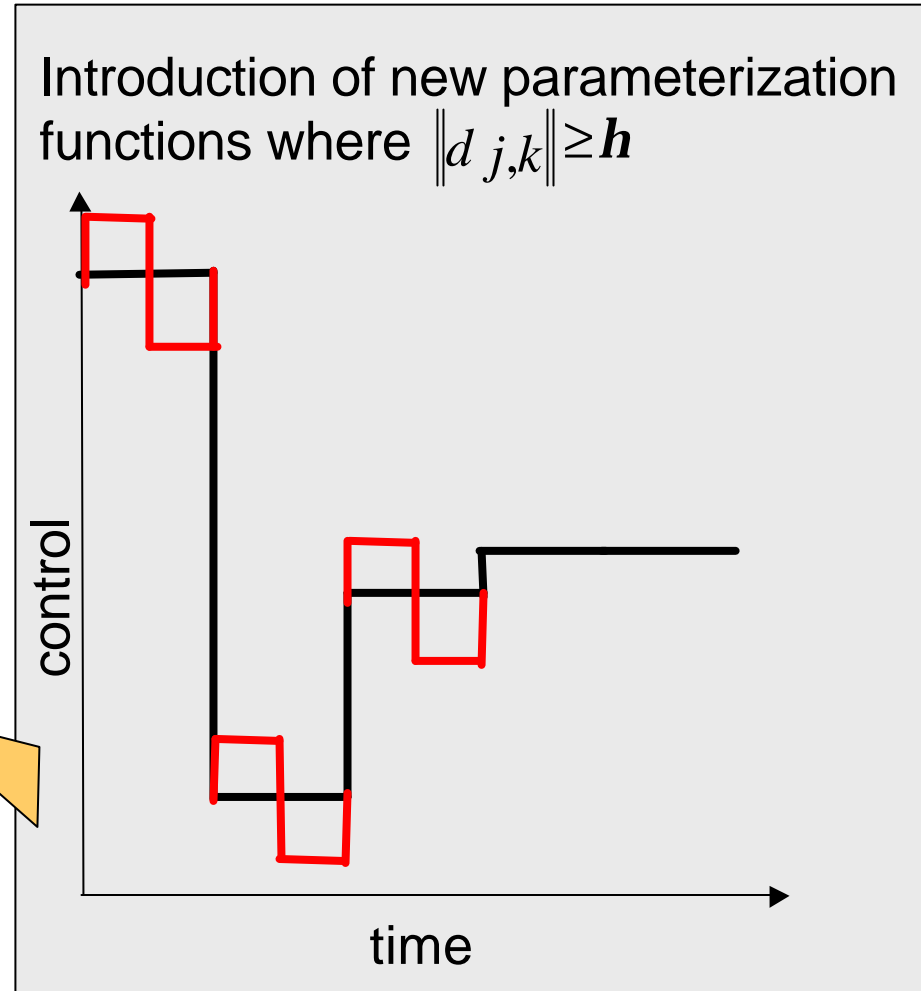
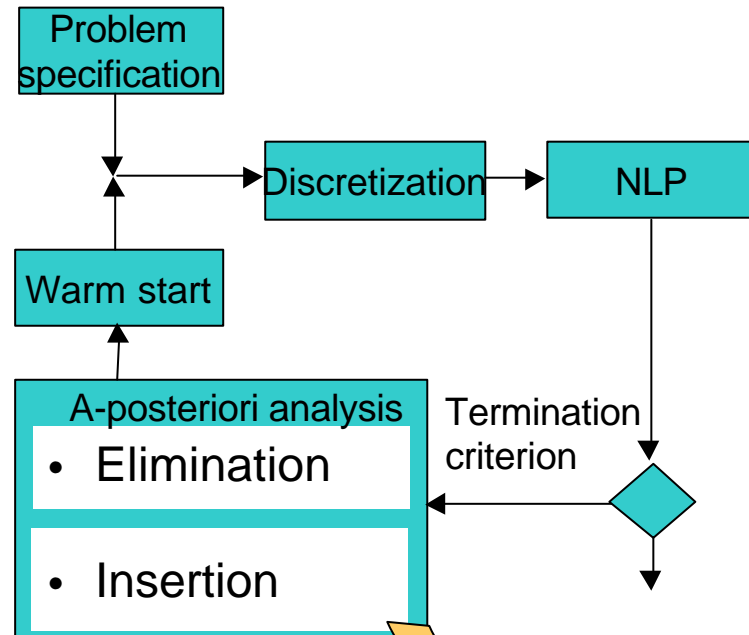
Approximation: Norm equivalence

$$\|u\|_{L_2} \sim \|d\|_{l_2} \quad \rightarrow$$

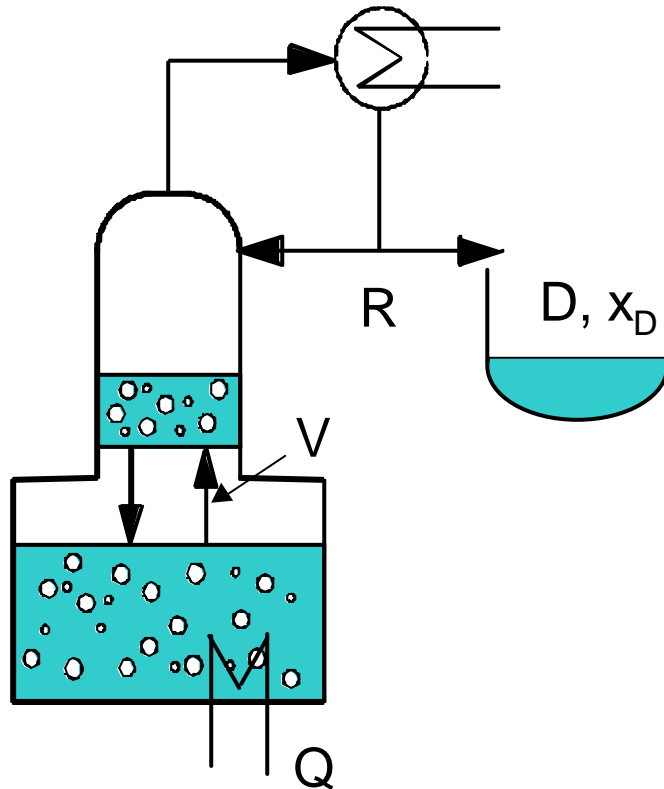
Discarding small $d_{j,k}$ causes only small changes in approximate representation



Insertion of parameterization functions



Analysis of wavelet coefficients of control variables



Objective:

Minimize energy demand with given:

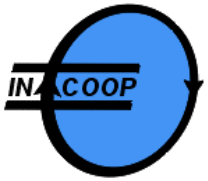
- Fixed batch time
- Amount of distillate $D \geq 6.0$ kmol
- Product purity $x_D \geq 0.46$

Controls:

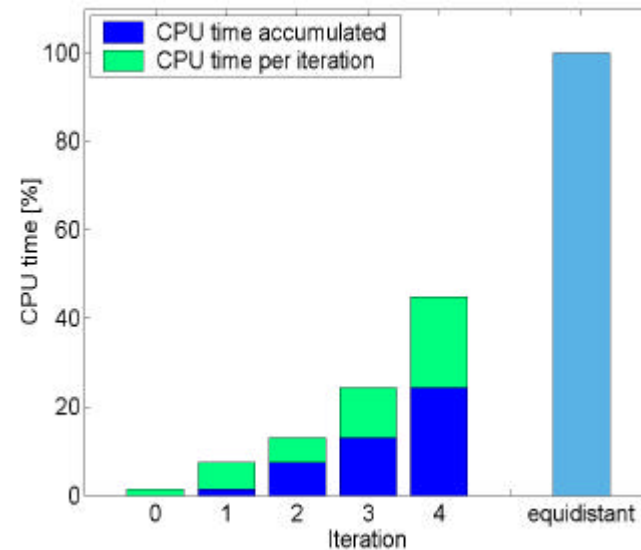
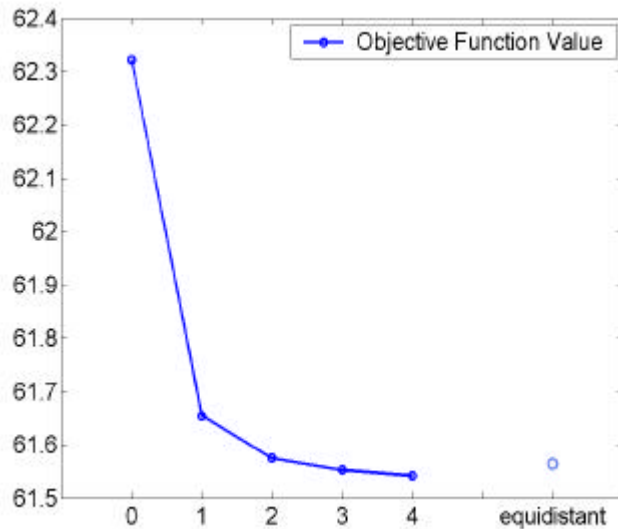
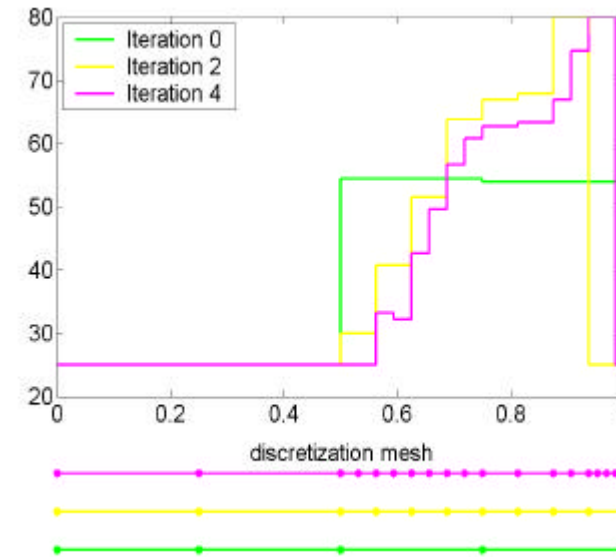
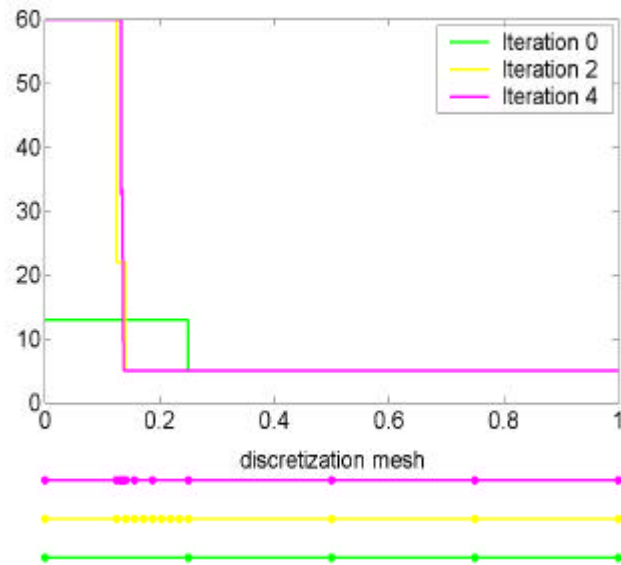
- Reflux ratio $R(t)$
- Vapor rate $V(t)$

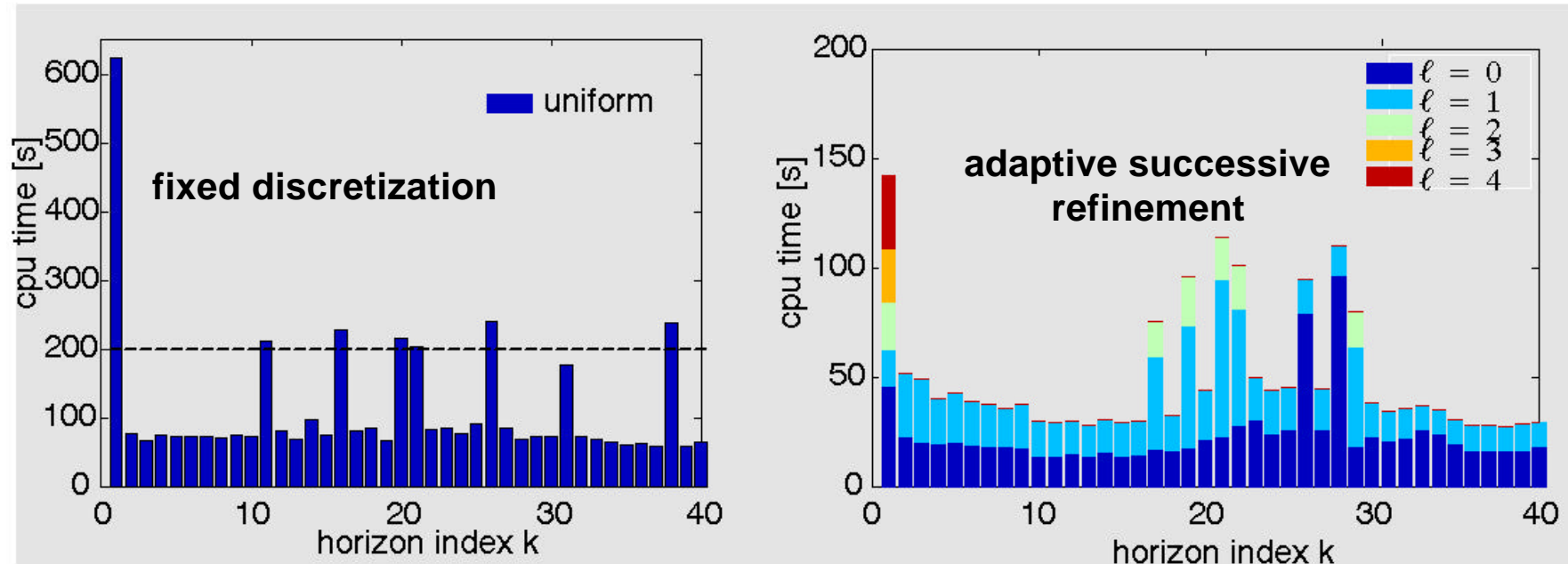
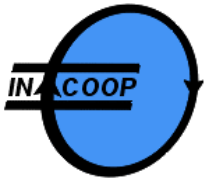
Dynamic model:

- 10 theoretical trays
- gPROMS model contains 418 DAEs
(63 differential equations)



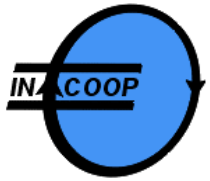
Results: Batch reactive distillation



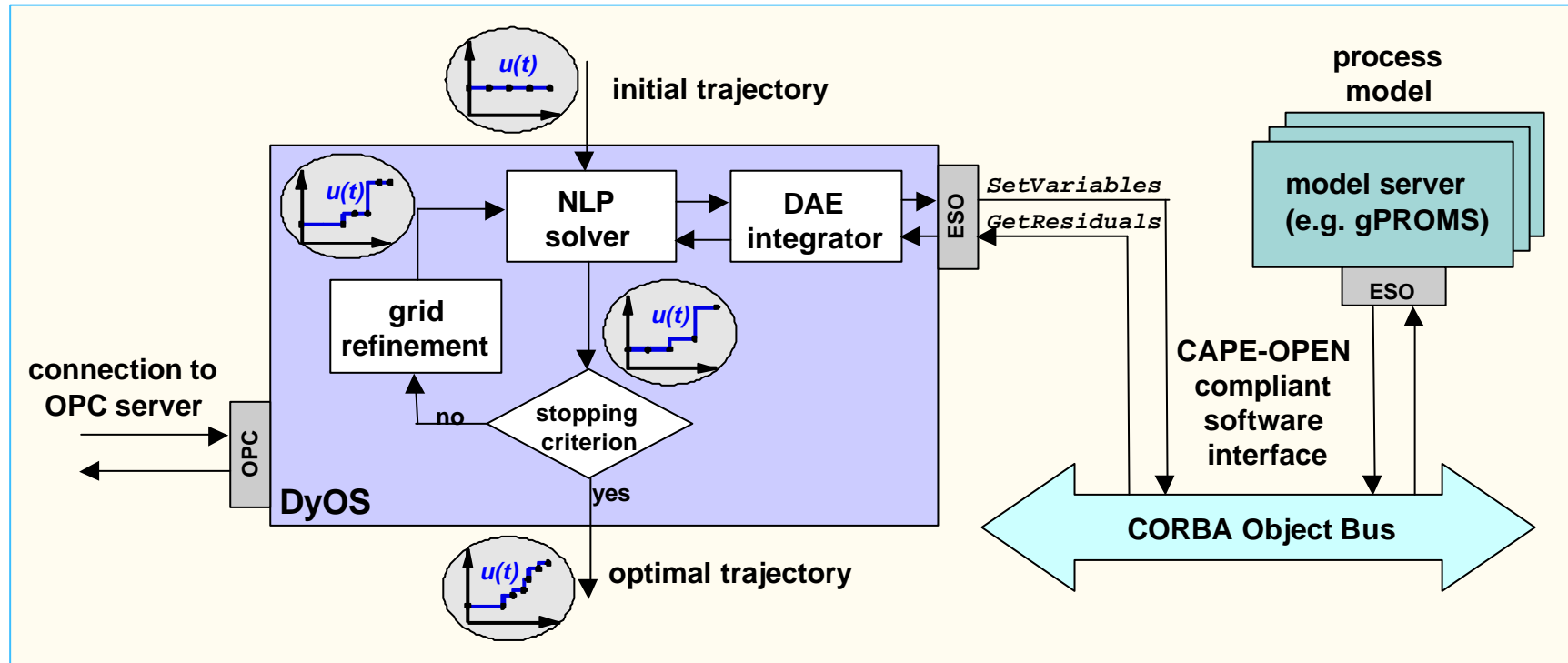


Adaptive approach (Binder et al., 2000):

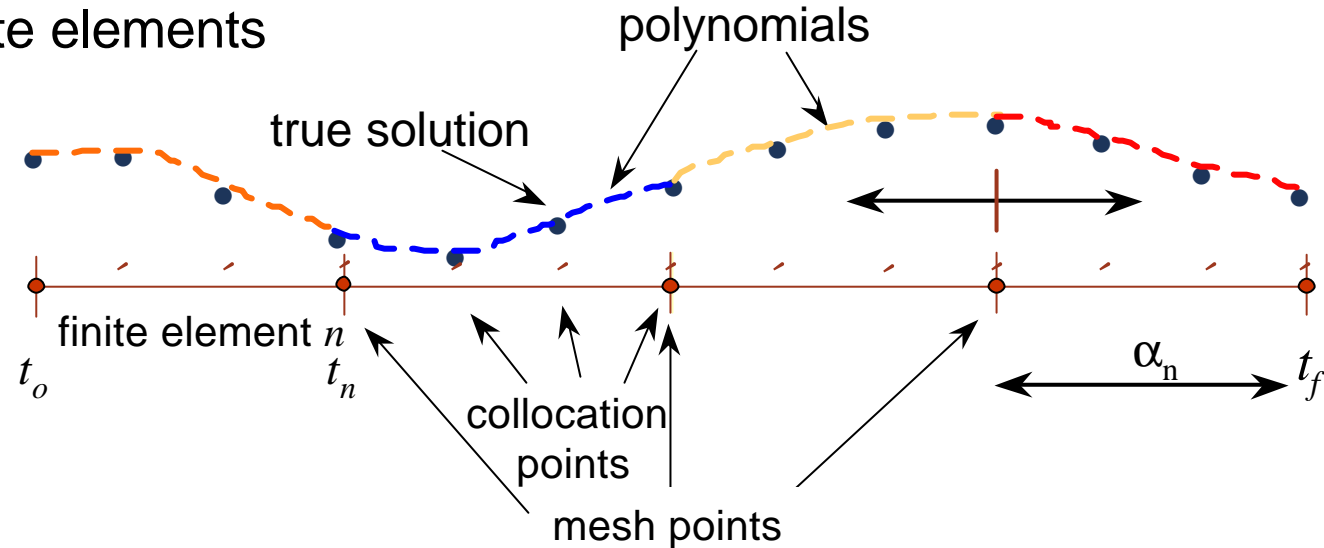
- numerical lower for the adaptive refinement approach
- intermediate solutions are available
 - back-up values in real-time environment
 - direct employment on the process at early time



Dynamic optimization software DyOS (LPT)



Collocation on finite elements



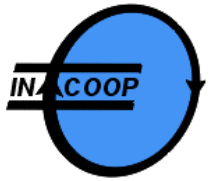
element n

$$z(t) = z_{n-1} + (t - t_{n-1}) \sum_{q=1}^k g^q(t) \frac{dz^q}{dt_n}$$

differential variables
continuous

$$y(t) = \sum_{q=1}^k g^q(t) y_n^q \quad u(t) = \sum_{q=1}^k g^q(t) u_n^q$$

algebraic and control variables
discontinuous



Simultaneous approach → collocation (II)



Conversion into NLP problem yields

$$\min \mathbf{y}(z_i, y_{i,j}, u_{i,j}, p, t_f)$$

$$\text{s.t.} \left(\frac{dz}{dt} \right)_{i,j} = F \left(z_{i-1}, \frac{dz}{dt}_{i,j}, z_i, y_{i,j}, u_{i,j}, p \right)$$

$$0 = G \left(z_{i-1}, \frac{dz}{dt}_{i,j}, z_i, y_{i,j}, u_{i,j}, p \right)$$

$$z_i = f \left(\frac{dz}{dt}_{i-1,j}, z_{i-1} \right)_i$$

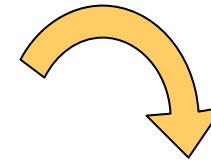
$$z_0^o = z(0)$$

$$z_i^l \leq z_i \leq z_i^u$$

$$y_{i,j}^l \leq y_{i,j} \leq y_{i,j}^u$$

$$u_{i,j}^l \leq u_{i,j} \leq u_{i,j}^u$$

$$p^l \leq p \leq p^u$$

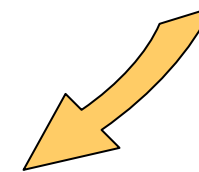


large-scale NLP problem

$$\min_{x \in R^n} f(x)$$

$$\text{s.t. } c(x) = 0$$

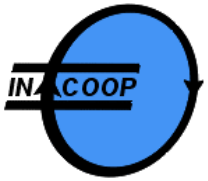
$$x^L \leq x \leq x^u$$



Requires specially tailored solution techniques:

- advanced interior-point solver
- filter-line search techniques

(implemented as IPOPT, Biegler et al., 2001)



Barrier function formulation



original formulation

$$\begin{aligned} \min_{x \in R^n} & f(x) \\ \text{s.t.} & c(x) = 0 \\ & x \geq 0 \end{aligned}$$

can be generalized for

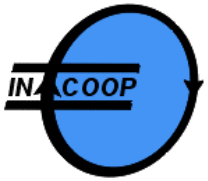
$$a \leq x \leq b$$



barrier approach

$$\begin{aligned} \min_{x \in R^n} & \mathbf{j}_m(x) = f(x) - \mathbf{m} \sum_{i=1}^n \ln s_i \\ \text{s.t.} & c(x) = 0 \\ & s - x = 0 \end{aligned}$$

$$\Rightarrow \text{as } \mathbf{m} \rightarrow 0, \quad \mathbf{x}^*(\mathbf{m}) \rightarrow \mathbf{x}^*$$



Solution of the barrier problem (I)



⇒ Newton Directions (KKT System)

$$\nabla f(x) + A(x)\mathbf{l} - v = 0$$

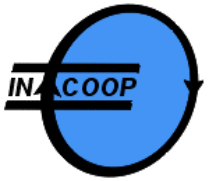
$$S\mathbf{V}e - \mathbf{m}e = 0$$

$$c(x) = 0$$

$$s - x = 0$$

⇒ solve primal-dual version

$$\begin{bmatrix} H & 0 & A & -I \\ 0 & S^{-1}V & 0 & I \\ A^T & 0 & 0 & 0 \\ -I & I & 0 & 0 \end{bmatrix} \begin{bmatrix} d_x \\ d_s \\ d_l \\ d_v \end{bmatrix} = - \begin{bmatrix} \nabla f + A\mathbf{l} - v \\ v - \mathbf{m}S^{-1}e \\ c \\ 0 \end{bmatrix}$$



⇒ Range Space Step

$$A^T d_x + c = 0$$

$$\Rightarrow d_R = -C^{-1}c$$

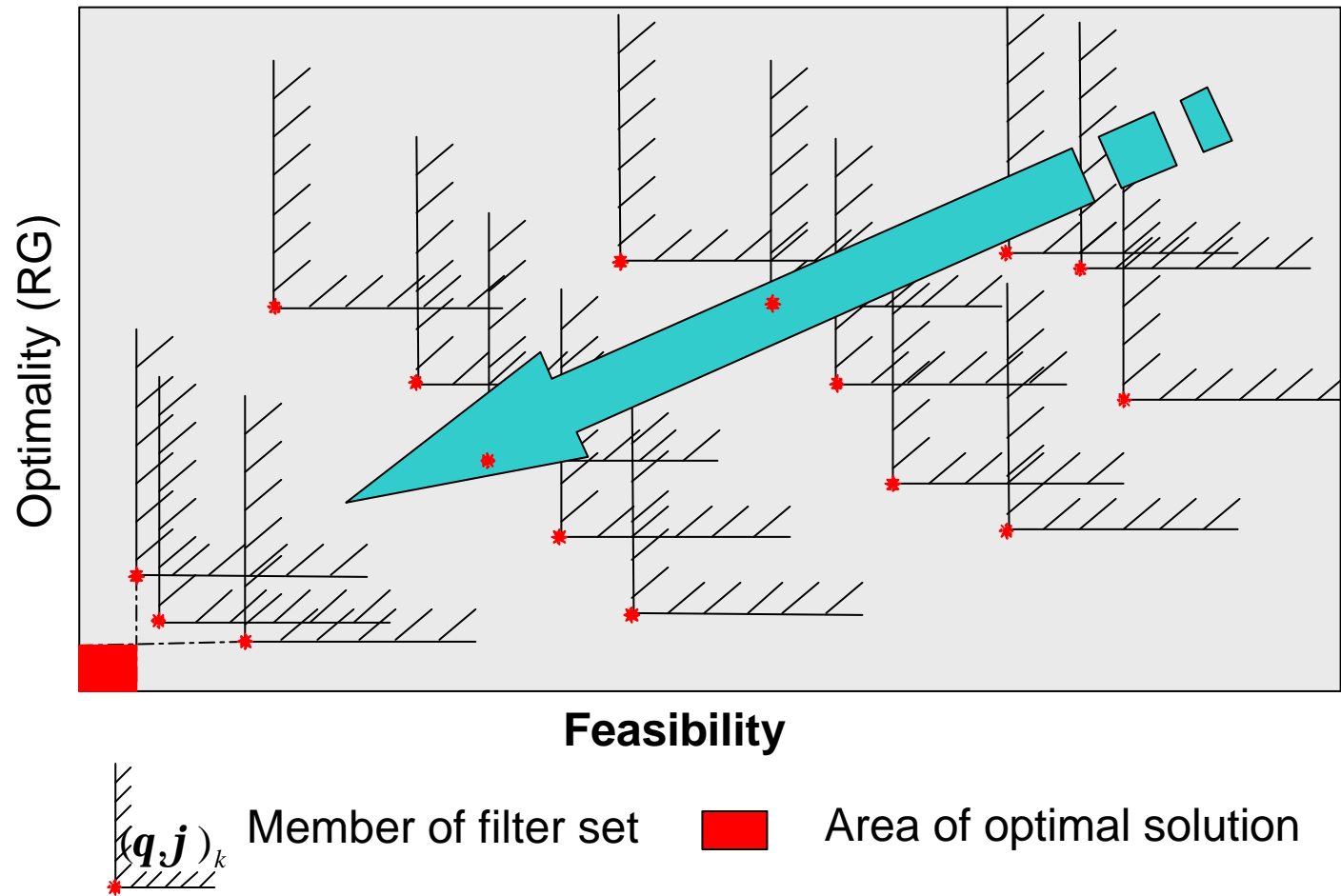
⇒ Null Space Step (reduced QP)

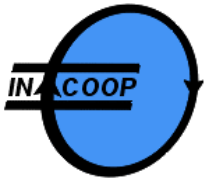
$$\min_{d_Q} \left(Q^T \nabla \mathbf{j}_m + Q^T (H + \Sigma) R d_R \right)^T d_Q + \frac{1}{2} d_Q^T Q^T (H + \Sigma) Q d_Q$$

$$d_Q = - \left[Q^T (H + \Sigma) Q \right]^{-1} \left(Q^T \nabla \mathbf{j}_m + Q^T (H + \Sigma) R d_R \right)$$

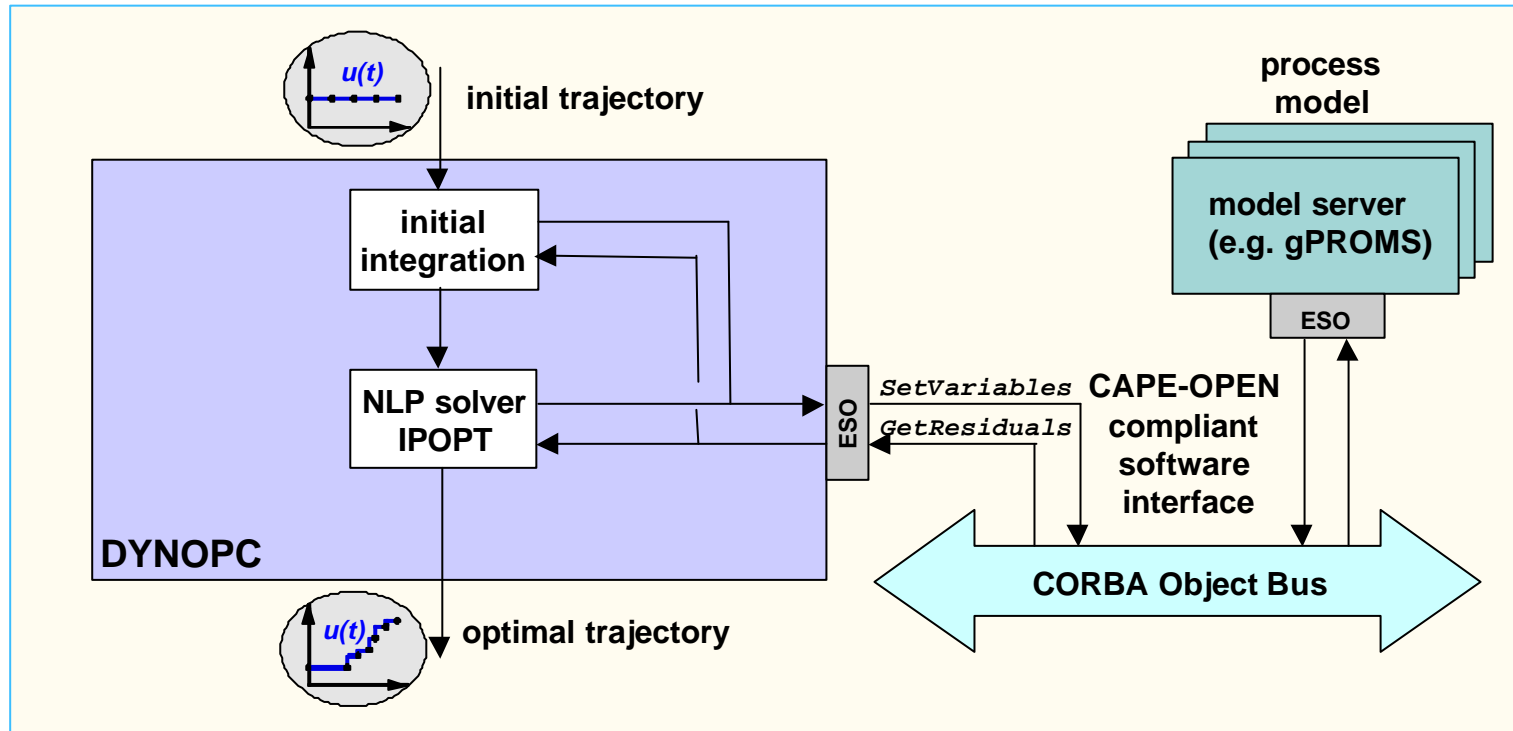
reduced Hessian

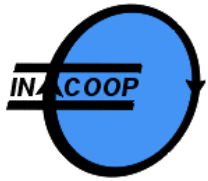
cross term





Dynamic optimization software DYNOPC/IPOPT (CMU)





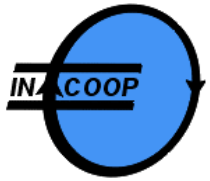
Comparison of approaches



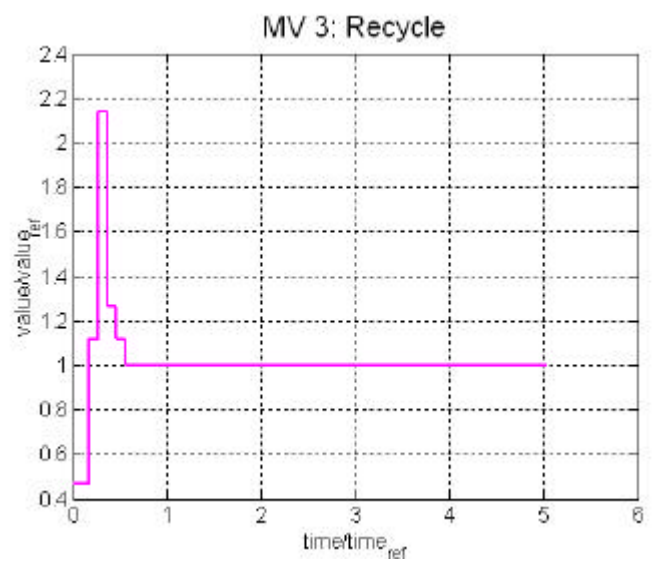
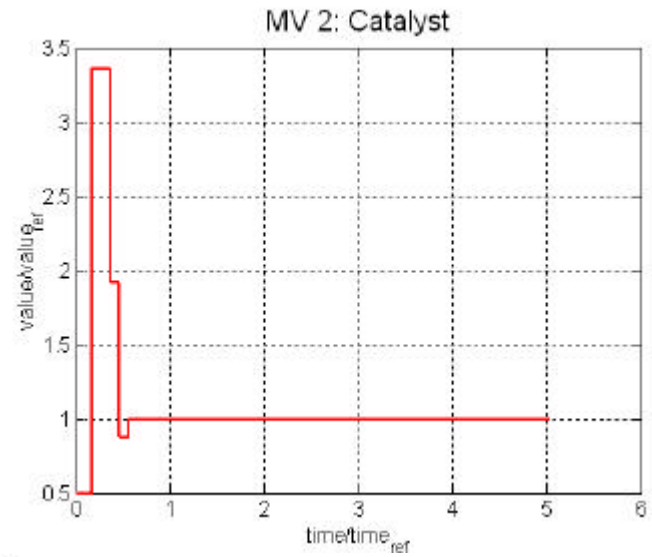
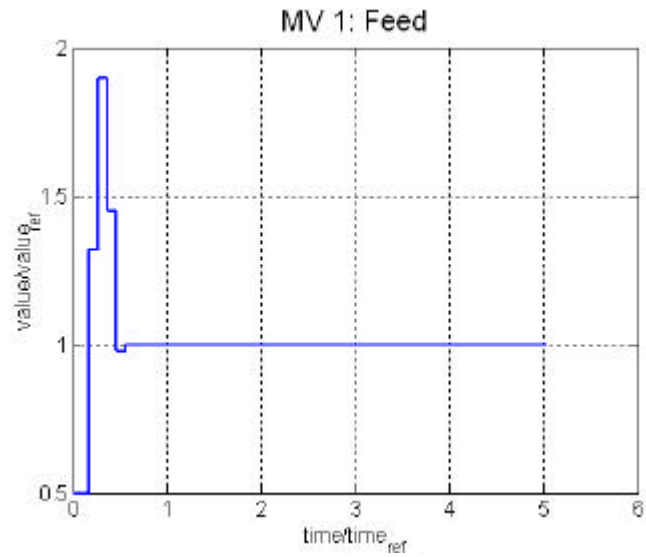
	Sequential approach	Simultaneous approach
size of NLP	small	large
DAE model fulfilled in each step?	yes	no
initial guess required for...	controls	states and controls

Experience from solving INCOOP benchmark problems

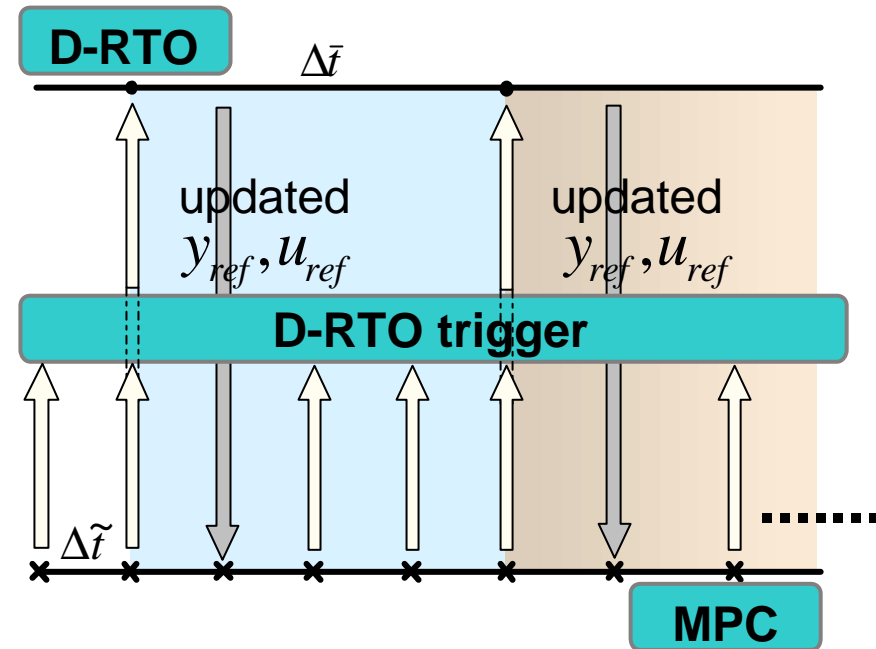
- sequential approach more robust and capable of handling bigger problems
- simultaneous approach can be faster with good initial guess, but more sensitive to initial guess
- accuracy problems with simultaneous approach for stiff problems
(error controlled integration vs. fixed-grid collocation)

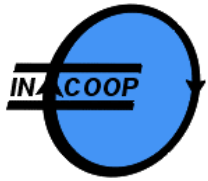


Results for Bayer Benchmark Problem



- Soft constraints can be moved from MPC to D-RTO
- Longer time horizon for D-RTO to ensure feasibility
- D-RTO trigger for a possible re-optimization
- Delta-mode MPC computes updates to the control profiles for tracking the process in the strict operation envelope: rejects fast frequency process disturbances



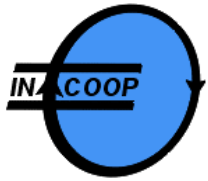


Lagrange function sensitivities w.r.t. all estimated disturbances

$$\text{compute } S_j = dL_j / d\hat{d}_j \Big|_{\tilde{t}_{0j}} ;$$

$$L_j = \bar{\Phi}(u_i^{ref}, \hat{d}_j) + \mathbf{m}_i^T h(u_i^{ref}, \hat{d}_j)$$

- One sensitivity integration of process model at each sampling time \tilde{t}_{0i} using previous D-RTO results (and active constraint set) at \tilde{t}_{0j} is required
- Compute change in sensitivities ($\Delta S_j = S_j - S_i$) and Lagrange function ($\Delta L_j = L_j - L_i$) can be then calculated



D-RTO trigger (II)



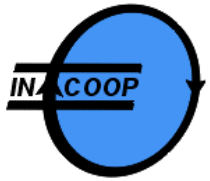
Optimal solution sensitivities w.r.t. all estimated disturbances

$$\text{compute } U_j = \left. \frac{du_j^{ref}}{d\hat{d}_j} \right|_{\tilde{t}_{0,j}}$$

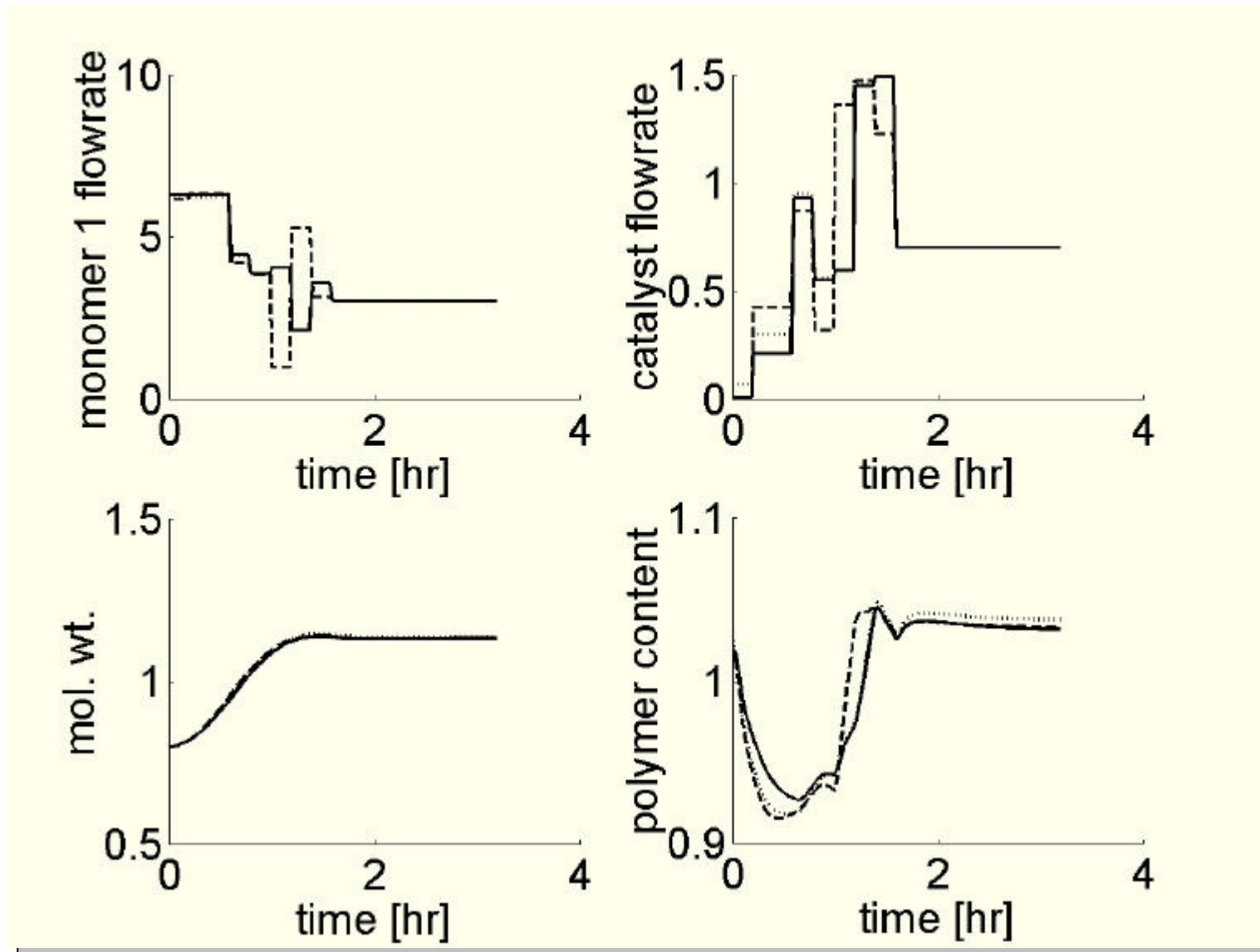
and changed active constraint set

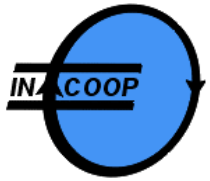
- Solution to QP problem:
 - using second order information (Hessian of Lagrange function)
 \Rightarrow *optimal sensitivities*
 - using first order information
 \Rightarrow *feasible only sensitivities*
- updates as $u_j^{ref} = u_i^{ref} + U_i^T (\hat{d}_j - \bar{d}_i)$

- If ΔS_j and ΔL_j are larger than a threshold value S_{th} and changed active constraint set is predicted, a re-optimization should be done
- Else linear updates based on optimal solution sensitivities U_j are sufficient

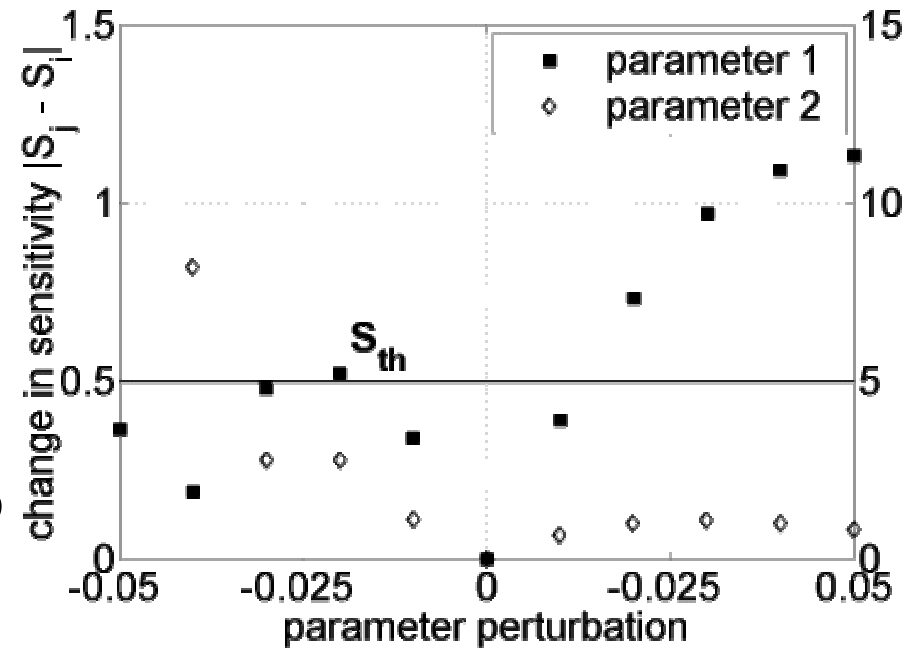


results with re-optimization and feasible updates

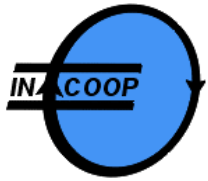




- Reaction parameters randomly perturbed between their bounds
- Re-optimization done only when necessary
⇒ steer to desired grade
- Feasible updates only possible up to +4% change in parameter 1



- D-RTO problem needs to be solved only necessary
- the hybrid integrated D-RTO and control with embedded sensitivity analysis is well suited for large-scale industrial process operation



Off-line dynamic optimization:

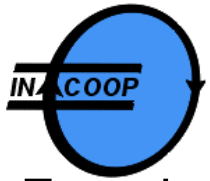
Today already many numerical and software techniques available for efficient and convenient solution of such problems

but...

dynamic optimization still not state-of-the-art (especially not in industry):

- Though pure solution time for solving one mathematical problem only in the order of *hours*,
- overall engineering time to solve the real application problem in the order of *weeks or months*.
- Problems: Modeling issues, problem formulation, convergence problems, ...

It is still not “pushing the button”.



Experience from INCOOP: for large-scale process models application of dynamic optimization in real-time still time-critical

Dynamic real-time optimization

- further enhance sequential approach dynamic optimization
- more elaborate adaptation strategies
- interaction NLP solver / integrator
- adapt integration accuracy
- incorporate second order information

Integration of control and optimization

- further exploit re-optimization features
- apply adaptation strategies in real-time context
- gain speed by feasible-first optimizations
- interlink MPC and D-RTO by shifting the prediction to the D-RTO level