

Modelling and simulation of a direct synthesis of dimethyl ether (DME) in a tubular reactor with a hybrid catalyst bed

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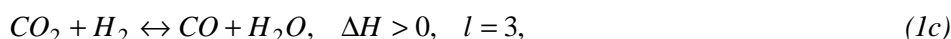
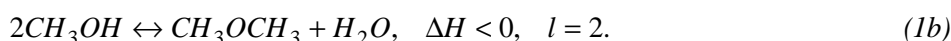
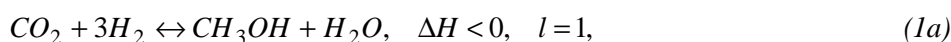
1. Summary

This work includes a modelling and simulation of dimethyl ether direct synthesis in a tubular type reactor with hybrid catalysts bed. The results of simulation show that the loading ratio of methanol synthesis and dehydration catalysts has a important influence on product yield.

Keywords: simulation, zeolite, hybrid catalyst bed, dimethyl ether

2. Extended Abstract

For a reaction system describing a direct synthesis of methyl ether from carbon dioxide and hydrogen:



a mathematical model was created of an adiabatic tubular reactor with a plug flow. It was assumed that reference reagents are DME and CO₂. For carbon dioxide a change in number of moles was established, as concluded from reactions (1a) and (1c). Using the definition of the reaction progress number, ξ , running numbers of moles of DME and CO₂ were established. Defined was the dwell time, t and then a dimensionless time related to the maximum dwell time: $\tau = t \cdot t_{\max}^{-1}$. Using these equations a differential control volume was written: $dV = \dot{F}_{ov} \cdot t_{\max} \cdot d\tau$. The differential mass balance for individual reference compounds, including the initial conditions was written in the form:

$$\dot{F}_{on} \cdot d(y_{CO_2}^0 - \xi_1 - \xi_3) = -\dot{F}_{ov} \cdot t_{\max} \cdot \rho_{z,1} \cdot r_1 \cdot d\tau, \quad \xi_1(0) = 0, \quad (2a)$$

$$\dot{F}_{on} \cdot d\xi_2 = \dot{F}_{ov} \cdot t_{\max} \cdot \rho_{z,2} \cdot r_2 \cdot d\tau, \quad \xi_2(0) = 0, \quad (2b)$$

$$\dot{F}_{on} \cdot d(y_{CO_2}^0 - \xi_1 - \xi_3) = -\dot{F}_{ov} \cdot t_{\max} \cdot \rho_{z,1} \cdot r_3 \cdot d\tau, \quad \xi_3(0) = 0, \quad (2c)$$

$$F_v \cdot \rho \cdot c_p \cdot dT = \left[\sum_{i=1}^3 (-\Delta H_i) \cdot r_i \cdot \rho_{z,i} \right] \cdot F_{ov} \cdot t_{max} \cdot d\tau, \quad T(0) = T_p. \quad (2d)$$

In the set of equations (2) values appear that are related to the hybrid bed: $\rho_{z,1}$ means the density of catalyst in reaction (1a), and $\rho_{z,2}$ is the density of zeolite. The third reaction takes place in the presence of a catalyst of methanol synthesis. For further discussion the average density ρ_z of a hybrid bed was introduced, and also defined was a new value x as a dimensionless mass fraction of a zeolite catalyst in a mixed bed. Because of this, a notation $\rho_{z,1} = (1-x) \cdot \rho_z$ and $\rho_{z,2} = x \cdot \rho_z$ could be used. Used here was the established in the Ph.D. work (Anna Ptaszek, *Modelling of DME direct synthesis*, Gliwice, 2004) kinetic equation of methanol dehydration on a zeolite catalyst:

$$r_2 = k \cdot \frac{K_{MeOH}^2 \cdot a_{pMeOH}^2 \cdot \left(1 - \frac{a_{pH_2O} \cdot a_{pDME}}{K_{ap} \cdot a_{pMeOH}^2} \right)}{\left(1 + K_{MeOH} \cdot a_{pMeOH} + K_{DME} \cdot a_{pDME} + K_{H_2O} \cdot a_{pH_2O} \right)^2} \quad (3)$$

Based on the available literature, selected were a methanol synthesis kinetics and kinetics of a reaction (1c) given by Vanden Bussche and Froment. Integrations of the system of equations (2) were performed for two sets of substrate compositions: $y_{H_2}^0 = 0.8$; $y_{CO_2}^0 = 0.2$ (fig.1a) and $y_{H_2}^0 = 0.6$; $y_{CO_2}^0 = 0.2$; $y_{CO}^0 = 0.2$ (fig. 1b) under the following conditions: $T_p=500$ K, pressure changing from 1 to 5 MPa. In calculations it was also assumed that $t_{max}=1$, $\rho_z=1000$ and $x=0.5$. Therefore $\rho_{z,1}=\rho_{z,2}=500$.

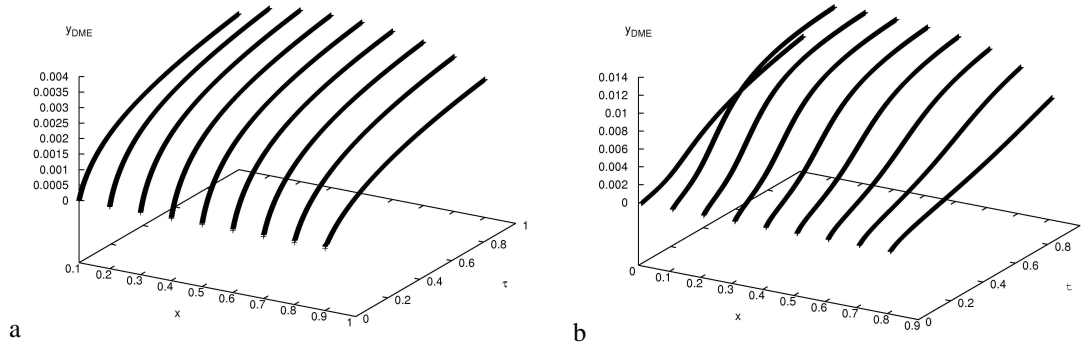


Figure 1: Dependence of DME molar fraction on dimensionless mass fraction of zeolite in a hybrid catalyst bed x and dimensionless time τ for two substrate compositions:

(a) $y_{H_2}^0 = 0.8$; $y_{CO_2}^0 = 0.2$, (b) $y_{H_2}^0 = 0.6$; $y_{CO_2}^0 = 0.2$; $y_{CO}^0 = 0.2$.

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References

Vanden Bussche K. M, Froment G., (1996), *Journal of Catalysis*, 161, 1-10