

CO₂ CAPTURE SOLVENT SELECTION BY COMBINED ABSORPTION-DESORPTION ANALYSIS

Ugochukwu E. Aronu¹, Hallvard F. Svendsen¹, Karl Anders Hoff²

¹ Department of Chemical Engineering, Norwegian University of Science and Technology, N-7491 Trondheim, Norway; Email: ugochukwu.aronu@chemeng.ntnu.no, hallvard.svendsen@chemeng.ntnu.no

² SINTEF Materials and Chemistry, N-7465 Trondheim, Norway; Email: Karl.A.Hoff@sintef.no

Abstract

A method was developed for selection of promising solvents based on CO₂ absorption experiments at 40°C and 9.5 kPa CO₂ partial pressure followed by desorption of same solvents at 80°C down to 1.0 kPa CO₂ partial pressure. The experiments conducted under atmospheric conditions revealed the solvents absorption and desorption characteristics and were compared with 1.0M, 2.5M, 5.0M and 10.0M MEA. Results showed that only absorption or stripping data alone was not sufficient in making robust solvent selection decisions; combined data analysis was necessary. 1.0M tetraethylenepentamine (TEPA) and 5.0M MEA showed the best performance in terms of absorption rate. 1.5M Bis-(3-dimethylaminopropyl) amine (TMBPA) was easy to desorb, has high absorption capacity; and when promoted it has the best performance in terms of CO₂ carrying capacity. At the test conditions, 1.5M TMBPA promoted with 1.0M PZ showed the most outstanding potential for efficient CO₂ removal at reduced cost of all systems tested. Its cyclic capacity in molCO₂/mol amine was found to be 70% higher than 5M MEA.

Keywords: CO₂ absorption, desorption, screening, TEPA, TMBPA

1. Introduction

Climate change has been associated with increased emissions of carbon dioxide from anthropogenic sources and is identified as the most important contributing green house gas¹. It is thus pertinent that carbon dioxide emissions from combustion exhaust gases must be reduced. Many technologies exist today for separation and capture of CO₂ from gas streams² with absorption by amine based solvents being the most common for CO₂ removal from combustion exhaust gases. Commonly used amine absorbents include monoethanolamine (MEA) and Mitsubishi Heavy Industries, KS1. Efficient absorption has its challenges mainly from high energy demand of the process which is linked to the characteristics of the solvent used in the process. Development of more efficient solvents is thus crucial in reducing the cost of CO₂ capture.

This work aims at finding new solvents with high potential for low energy demand in CO₂ absorption by analysis of the absorption-desorption properties of pre-selected solvents including comparison with MEA. Solvent pre-selection focused mostly on solvents with potential for high absorption capacity and fast reaction kinetics. These features were accessed using structure and pKa considerations of solvents. Overall, an increase in absorption capacity with increase in chain length between different functional groups in alkanolamines³ is found, while increase in alkyl groups and also increased chain length between amine functional groups increases pKa⁴. Bis-(3-dimethylaminopropyl) amine TMBPA has 3 amine sites (one secondary and two tertiary) indicating a potential for high absorption capacity of 3molCO₂/mol and a loading of 2.9molCO₂/mol has been achieved⁵. Two tertiary amine sites could result in probably lower reaction rate⁶ but presence of one secondary amine site and longer chains (3 carbon atoms) between the secondary and tertiary sites, shows better possibilities for improved kinetics⁴ than would be expected for a tertiary amine. Because TMBPA has two tertiary amine sites it was suspected that the reaction rate could be low to some extent and it was decided to activate it with promoters which will act as a shuttle, as they react rapidly with CO₂ to reduce mass-transfer resistance and facilitate fast transport of CO₂ into the liquid phase^{6,7}. Mixing a primary or secondary amine with a tertiary amine, could improve the CO₂ selectivity in the presence of H₂S as well as reduce regeneration cost⁸. Promoters selected were 2,2-dimethyl-1,3-propanediamine (DMPDA), 3-methylaminopropylamine (MAPA), monoethanolamine (MEA) and piperazine (PZ). Structure and pKa considerations for other systems tested in this work have been described in earlier work⁹.

2. Screening Experiments

2.1 Materials

Amine absorbents used with their purity were obtained as follows; monoethanolamine, MEA (Sigma-Aldrich, purity \geq 99.9 mass %); TMBPA (Aldrich, purity > 97 mass %); TEPA (Fluka, purity \sim 85% mass %); DMPDA (BASF, purity > 97.5 mass %); while MAPA (purity > 99 mass %); PZ (anhydrous 99%); 2-amino-2-methyl-1-propanol, AMP (purity > 99 mass %); N, N'-di- (2 hydroxyethyl) piperazine, DIHEP (purity > 99 mass %) and N-2-hydroxyethylpiperzine, HEP (purity > 98.5 mass %) were obtained from Acros Organics. The solvents were used without further purification. All solution samples were prepared with deionized water. The CO₂ (purity > 99.99mol %) and N₂ (purity > 99.99 mol %) gases used were obtained from AGA Gas GmbH.

2.2 Methods

Absorption and desorption experiments were carried out using a screening apparatus designed to operate at atmospheric conditions and up to 80°C. The method which involves absorption of CO₂ with solvent at 40°C up to 9.5 kPa CO₂ partial pressure and stripping of the same solvent at 80°C down to 1.0 kPa gas phase CO₂ concentration is used to acquire first hand knowledge on the behaviour of each solvent system in an absorption process. Experiments are as described in Ma'mun et al.¹⁰; however, the apparatus was modified to allow stripping operations, Aronu et al.^{9,11}. It gives a fast relative comparison of absorption rate and absorption capacity as well as the stripping rate; thus enables estimation of the relative cyclic capacity of each solvent. Apart from these factors, other properties such as foaming, precipitation and possible discolouration upon CO₂ loading which may be indicative of solvent degradation could be observed. The base case solvent used is MEA; thus to provide a broad basis for comparison, different concentrations of MEA, 1.0M, 2.5M, 5.0M and 10.0M were tested. It is however not possible to have all solvent in same molar concentration due to molecular weight and/or viscosity issues as well as solvent cost. In general, a concentration of 2.5M of each solvent or solvent mixture were used and at same time using concentrations not too far from 30 wt% of amine solutions. Due to high molecular weight and viscosity of TMBPA and TEPA, concentrations of 1.5M and 1.0M respectively of each were used. For DIHEP and HEP a mixture with same mole fractions, 0.42M DIHEP and 0.58M HEP, as proposed by Hakka and Ouimet¹² was used. It should be noted that comparison of the experimental data here is semi-quantitative since there is no guarantee that the bubble structure, and thus the gas-liquid interfacial area were exactly the same in all experiments. However, the superficial gas velocities were the same, so the differences would arise mainly due to interfacial tension, bubble coalescence properties and viscosity¹⁰.

3. Results and Discussion

3.1 Absorption

The absorption rates versus loading (molCO₂/mol amine) plots are presented in figure 1a. It shows that 1.0M TEPA has distinctively higher absorption rate and attained a highest loading of 1.916molCO₂/mol while 1.5M TMBPA show high absorption capacity. TMBPA promoted with PZ and MAPA shows higher absorption rate and loading in practically all the loading range compared to all MEA concentrations. High cost of DIHEP and HEP do not allow tests to be carried out at high concentrations, however, its mixture of total concentration 1.0M tested shows that it has both lower rate and capacity than 1.0M MEA. 2.5M AMP has the lowest initial rate, and its rate was improved by activating with PZ. A look at absorption rate versus total amount of CO₂ absorbed in solution (molCO₂ per litre solution) in figure 1b gives a different perspective on the solvents performance. It shows that 10.0M MEA maintained the highest rate and absorbs the highest amount of CO₂ in solution over all concentration ranges for all solvents (except for 1.0M TEPA which has higher initial rate up to concentration point 0.708 molCO₂/Lamine). This is because solvent CO₂ absorption capacity in (molCO₂ per litre solution) is a function of its molar concentration. Increase in molar concentration results in increasing solvent absorption capacity. It is therefore expected that increased concentrations of TEPA and TMBPA will increase absorption capacity. However, this could be limited by associated viscosity and foaming problems. Initial screening experiments were conducted where half of the initial concentrations were used, and the results showed less foaming. Present results from figure 1a shows 1.0M TEPA as the best solvent while in figure 1b it is 10.0M MEA. This shows that assessment of only absorption plots is not sufficient to give complete information on absorption characteristics of solvents for quick decision on solvent performance; other factors are necessary.

3.2 Desorption

The solvents attained different loadings and absorbed different amounts of CO₂ in solution. Desorption tests at 80°C give indication of the relative CO₂ carrying capacity for these solvent systems under these experimental conditions. Figure 1c shows stripping rate versus loading (molCO₂/mol amine). 2.5M AMP and 0.42M DIHEP + 0.58M HEP attained lowest lean loads, thus showing high desorption ability. The figure also shows that TMBPA attains both low lean loading (0.31) and high rich loading (1.62) while TEPA has high rich loadings (1.92) but much higher lean loading (0.81) under the same conditions when compared to MEA. This gives an indication of good desorption characteristics of TMBPA and its potential for lower regeneration energy demand than TEPA. In figure 1d the stripping rates are plotted for the amines showing the amount of CO₂ removed in mol/L solution. The curves show that 10.0M MEA absorbed the highest amount of CO₂ (4.74 molCO₂/L), however, only small amount of this could be desorbed at the conditions used, resulting in 2.73 molCO₂/L solution at the lean end. 2.5M AMP and 1.5M TMBPA clearly shows that low lean CO₂ concentrations are obtainable even though they achieved high rich loadings. Blends of 2.5M AMP with 0.5M PZ and all activated 1.5M TMBPA show low concentrations of CO₂ at the lean end but not in activation with 1.0M MAPA and 1.0M DMPDA. The plots also show that the lowest lean end concentration of CO₂ is achieved in 0.42M DIHEP + 0.58M HEP. This gives an indication of high desorption ability of this mixture when compared to 1.0M MEA and 1.0M TEPA. It is necessary however to observe that this solvent has the lowest rich concentration of CO₂ in solution.

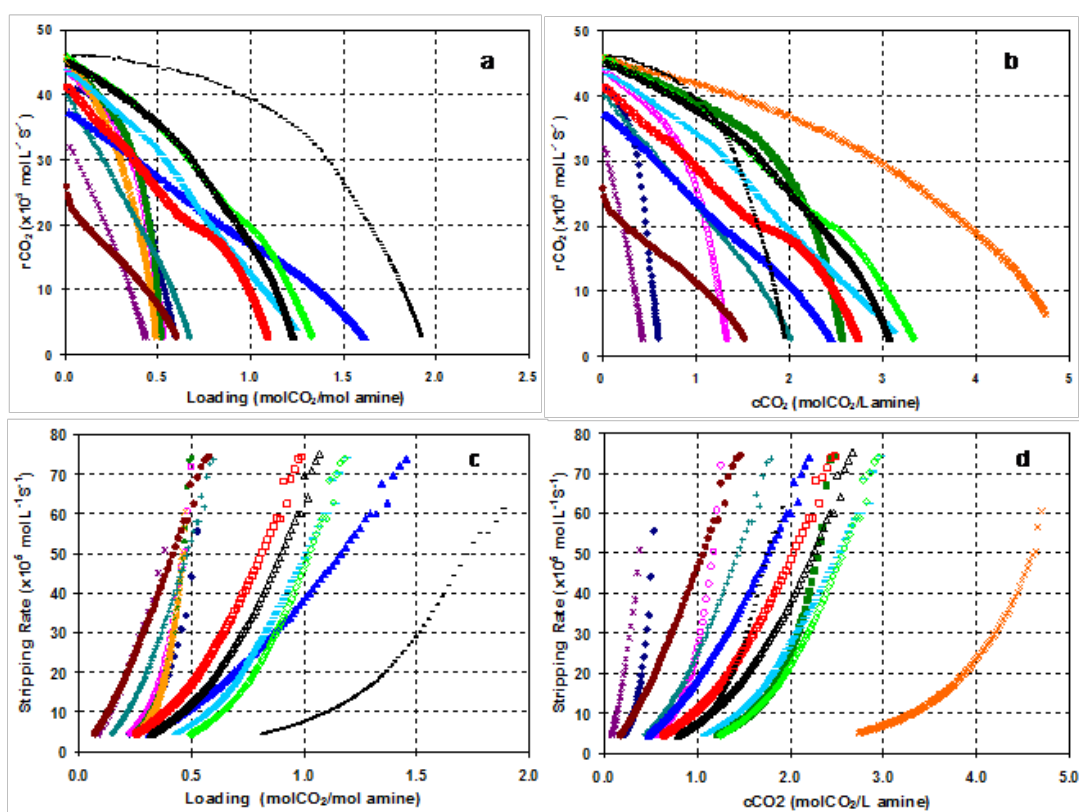


Figure 1. Screened amines absorption curves at 40°C; (a) absorption rate as function of loading in molCO₂/mol amine; (b) absorption rate versus amount of CO₂ in mol/L solution; Screened amines desorption curves at 80°C; (c) stripping rate as function of loading in molCO₂/mol amine; (d) stripping rate versus amount of CO₂ in mol/L solution ♦, 1.0M MEA; ○, 2.5M MEA; ■, 5.0M MEA; ×, 10.0M MEA; ✕, 0.42M DIHEP + 0.58M HEP; ●, 2.5M AMP; +, 2.5M AMP + 0.5M PZ; ▲, 1.5M TMBPA; —, 1.5M TMBPA + 1.0M DMPDA; ◇, 1.5M TMBPA + 1.0M MAPA; □, 1.5M TMBPA + 1.0M MEA; △, 1.5M TMBPA + 1.0M PZ; −, 1.0M TEPA.

3.3 Observed solvent characteristics

During desorption tests some of the solvents flashed or foamed up to the condenser as soon as N₂ was introduced to start the stripping process. Flashing was observed in AMP and TMBPA and in all the mixtures as well as in TEPA. Strongest flashing was observed in 2.5M AMP + 0.5M PZ, 1.5M TMBPA + 1.0M PZ, 1.5M TMBPA + 1.0M MAPA and 1.0M TEPA. Four factors are believed to be likely contributors to this phenomenon; high CO₂ desorption potential, foaming ability, solvent vapour

pressure and viscosity. Flashing of AMP and TMBPA is believed to be due to their high desorption potentials which allows high amounts of CO₂ in gas phase during the heating up process already at 80°C, thus it flashes off immediately when stripping starts with the introduction of N₂. High vapour pressures of PZ and MAPA contributes to flashing of their solvent mixtures. Foaming could also contribute to boiling up of TMBPA and TEPA as well as viscosity. It was generally believed that foaming is a contributor to flashing problems, thus to be able to strip the solvents under these conditions, flashing was suppressed using foam inhibitor. 1.0M TEPA changed from colourless to yellow solution during stripping while 1.5M TMBPA was found to changed from light yellow to light brown after stripping. 1.5M TMBPA + 1.0M MEA changed from light yellow to brownish orange and 10.0M MEA changed to yellow after absorption and stripping.

3.4 Absorption-desorption cycle analysis

Performance of each solvent system was also assessed by the consideration of their cyclic capacity (molCO₂/mol amine). Percent CO₂ removed during desorption as well as ΔCO₂ removed per litre solution allows for a true comparative analysis of the actual CO₂ carrying capacity (difference in CO₂ concentration in molCO₂/L solution between the rich and lean ends). Absorption rates at lean loading and 90% equilibrium loading were also determined. These give indications of how fast the lean solution reacts when pumped back to the absorber and the absorption rate towards equilibrium respectively. The absorption-desorption cycle calculation procedure is presented by Aronu et al.¹¹. Table 1 shows summary of absorption-desorption experiments results. It shows that the highest rich loading in molCO₂/mol amine was attained by 1.0M TEPA and lowest lean loading was achieved in 0.42M DIHEP + 0.58M HEP while 1.5M TMBPA has the highest cyclic capacity. Highest percent CO₂ removal per cycle was found in 2.5M AMP while all promoted 1.5M TMBPA show high carry capacity with highest value found in 1.5M TMBPA + 1.0M PZ. 1.0M TEPA has the highest absorption rate at lean loading while 5.0M MEA showed the highest absorption rate at 90% equilibrium approach.

Table 1. Absorption-desorption summary

| Solvent | α_{abs} | α_{strp} | Cyclic Capacity | % CO ₂ Removed Per Cycle | Absorption Rate at Lean Loading | Absorption rate at 90% Equilibrium Loading | cCO ₂ Rich end molCO ₂ /L | cCO ₂ Lean end molCO ₂ /L | ΔcCO ₂ Per Cycle molCO ₂ /L |
|-------------------------|----------------|-----------------|-----------------|-------------------------------------|---------------------------------|--|---|---|---|
| 1.0M MEA | 0.593 | 0.224 | 0.368 | 62.15 | 37.724 | 6.171 | 0.598 | 0.226 | 0.371 |
| 2.5M MEA | 0.529 | 0.224 | 0.303 | 57.29 | 37.371 | 8.624 | 1.332 | 0.569 | 0.763 |
| 5.0M MEA | 0.518 | 0.247 | 0.271 | 52.39 | 37.544 | 11.683 | 2.568 | 1.223 | 1.345 |
| 10.0M MEA | 0.475 | 0.273 | 0.201 | 42.40 | 31.996 | 9.226 | 4.743 | 2.732 | 2.011 |
| 0.42M DIHEP + 0.58M HEP | 0.430 | 0.080 | 0.350 | 81.43 | 28.847 | 4.791 | 0.430 | 0.080 | 0.350 |
| 2.5M AMP | 0.600 | 0.078 | 0.523 | 87.02 | 20.907 | 4.459 | 1.527 | 0.198 | 1.329 |
| 2.5 AMP + 0.5M PZ | 0.671 | 0.147 | 0.524 | 78.09 | 32.869 | 5.551 | 2.013 | 0.441 | 1.572 |
| 1.5M TMBPA | 1.615 | 0.311 | 1.304 | 80.76 | 31.713 | 5.349 | 2.451 | 0.472 | 1.980 |
| 1.5M TMBPA + 1.0M DMPDA | 1.245 | 0.431 | 0.815 | 65.42 | 33.386 | 6.048 | 3.113 | 1.077 | 2.037 |
| 1.5M TMBPA + 1.0M MAPA | 1.332 | 0.499 | 0.833 | 62.53 | 35.560 | 7.089 | 3.329 | 1.247 | 2.082 |
| 1.5M TMBPA + 1.0M MEA | 1.096 | 0.257 | 0.838 | 76.53 | 33.611 | 6.891 | 2.740 | 0.643 | 2.097 |
| 1.5M TMBPA + 1.0M PZ | 1.231 | 0.320 | 0.911 | 74.02 | 39.756 | 8.130 | 3.076 | 0.799 | 2.277 |
| 1.0M TEPA | 1.916 | 0.810 | 1.106 | 57.73 | 41.770 | 9.517 | 1.935 | 0.818 | 1.117 |

Units: α_{abs} , α_{strp} and cyclic capacity (molCO₂/mol amine); Absorption Rate ($\times 10^3$ molL⁻¹S⁻¹)

4. Solvent Performance Analysis

Cycle analysis results show that it is difficult to make any selection decision on the most promising solvent by consideration of single characteristics of the solvents. More concise solvent selection decision requires combined analyses of these properties. Combined absorption-desorption characteristics analysis was made possible using dot plots. In the plots solvents with best characteristics should appear at the top right hand corner. Figure 2a shows plots for amine absorption rates at lean loading as function of percent CO₂ removed. It shows that 1.0M TEPA followed by 1.5M TMBPA +1.0M PZ has the highest absorption rate for the lean solution, but 1.0M TEPA has lower desorption potential. 1.5M TMBPA +1.0M PZ shows both high absorption rates at lean loading and high desorption ability. Amine absorption rate at lean loading is plotted against the ΔCO₂ removed per cycle for each solvent system in figure 2b. This plot clearly shows that 1.5M TMBPA with all its mixtures as well as 10.0M MEA has particularly high carrying capacity compared to other amines. TMBPA and its family are of particular interest in this case considering their lower molar concentrations when compared to 5.0M and 10.0M MEA. They show high CO₂ carrying capacity with high desorption ability. The figure further shows that 1.5M TMBPA + 1.0M PZ has the best performance when absorption rate at lean loading is combined with solvent carrying capacity.

It is necessary to have an idea of the reaction rate of the solvents upon approach to equilibrium. In general the absorption rate is expected to decrease on equilibrium approach but a solvent with characteristics of fast reaction towards equilibrium is desired. Figure 2c, shows plots for absorption rate at 90% equilibrium loading against ΔCO_2 removed per cycle. It shows that 5.0M MEA has the highest absorption rate towards equilibrium followed by 1.0M TEPA and 10.0M MEA. 1.5M TMBPA + 1.0M PZ maintained a reasonable rate.

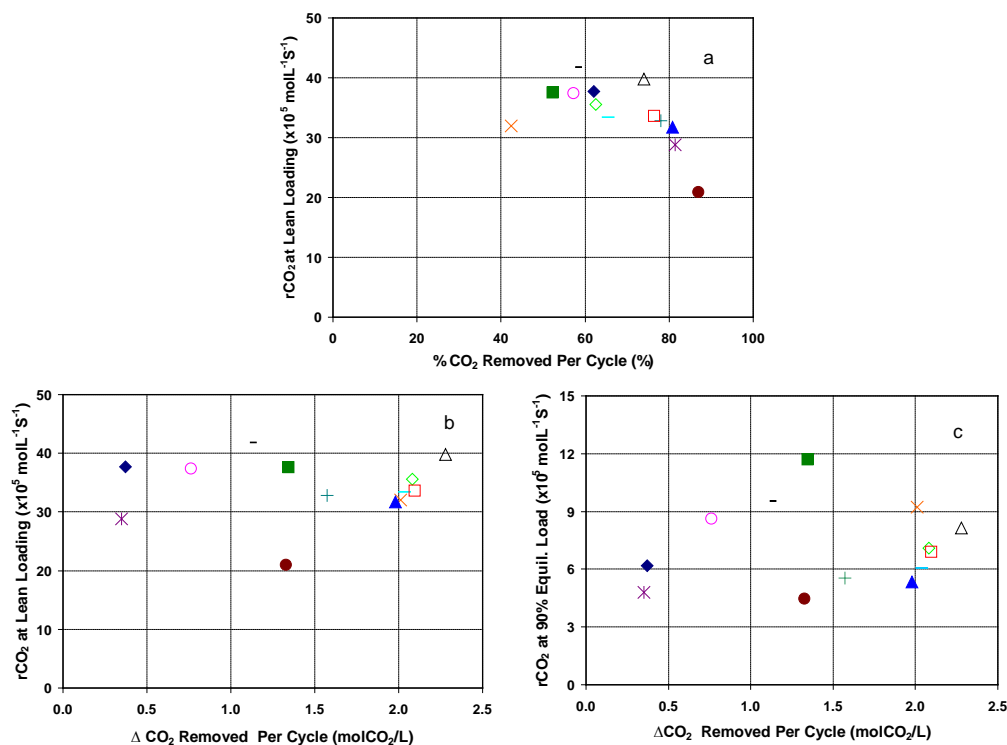


Figure 2. (a) Absorption rate at lean loading versus percentage of CO₂ removed per cycle; (b) Absorption rate at lean loading versus ΔCO_2 removed per litre solution per cycle; (c) amines Absorption Rate at 90% Equilibrium Loading vs Amount of CO₂ Removed per litre solution.: ◆, 1.0M MEA; ○, 2.5M MEA; ■, 5.0M MEA; ×, 10.0M MEA; ✕, 0.42M DIHEP + 0.58M HEP; ●, 2.5M AMP; +, 2.5M AMP + 0.5M PZ; ▲, 1.5M TMBPA; —, 1.5M TMBPA + 1.0M DMPDA; ◇, 1.5M TMBPA + 1.0M MAPA; □, 1.5M TMBPA + 1.0M MEA; △, 1.5M TMBPA + 1.0M PZ; -, 1.0M TEPA.

4.1 Overall performance in terms of CO₂ absorption rate

Overall solvent performances in terms of rate were deduced using a plot of absorption rate at lean loading against absorption rate at 90% equilibrium loading, figure 3a. This shows how fast the lean solvent will react when returned to the absorber and how fast the rate will be maintained towards equilibrium. Solvents with best rate performance have potential of reducing absorber dimension; thus capital cost as well as operating cost. The figure shows that 1.0M TEPA and 5.0M MEA shows overall best performance in terms of rate while 2.5M AMP has poorest performance. 1.5M TMBPA + 1.0M PZ maintained a comparatively high rate performance.

4.2 Overall performance in terms of CO₂ carrying capacity

A plot of amount of ΔCO_2 removed per cycle against percent CO₂ removed in figure 3b gives an indication of the overall performance of each solvent system in terms of CO₂ carrying capacity; it gives a comparative indication of how much of the CO₂ absorbed by the solvent is finally removed. Solvents with best carrying capacity will reduce solvent circulation rate. Figure 3b shows that 1.5M TMBPA and its mixtures have the highest CO₂ carrying capacity with 1.5M TMBPA + 1.0M PZ, 1.5M TMBPA + 1.0M MEA and 1.5M TMBPA having the best performance. MEA at its various concentrations show generally lower carrying capacity with the best performance in 10.0M MEA. 1.5M TMBPA + 1.0M PZ appears to have the overall best performance of all the solvent systems tested and analysed. In terms of absorption rate, it shows high initial rate, high rate at 90% equilibrium approach and also high absorption rate at lean loading. In terms of absorption capacity, it attains a comparatively high loading of 1.231mol CO₂/mol amine, absorbs large amounts of CO₂ per litre

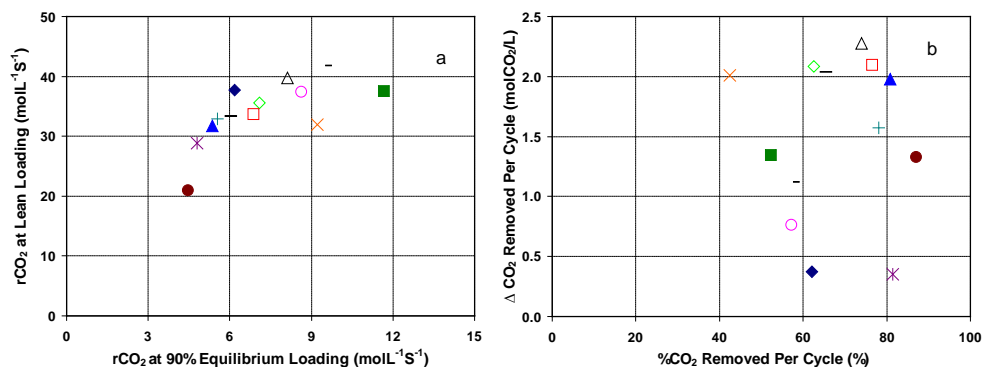


Figure 3. Solvents performance in terms CO₂ absorption of rate (a); Solvent performance in terms of CO₂ carrying capacity (b): ◆, 1.0M MEA; ○, 2.5M MEA; ■, 5.0M MEA; ×, 10.0M MEA; ✕, 0.42M DIHEP + 0.58M HEP; ●, 2.5M AMP; +, 2.5M AMP + 0.5M PZ; ▲, 1.5M TMBPA; —, 1.5M TMBPA + 1.0M DMPDA; ◇, 1.5M TMBPA + 1.0M MAPA; □, 1.5M TMBPA + 1.0M MEA; △, 1.5M TMBPA + 1.0M PZ; —, 1.0M TEPA.

solution (3.076mol CO₂/L) and desorbs about 74% of the CO₂ absorbed under the experimental conditions, making it the solvent with highest CO₂ carrying capacity (2.277mol CO₂/L). Its cyclic capacity in molCO₂/mol amine and ΔCO₂ per liter solution per cycle are respectively 70% and 41% more than 5M MEA. It did not show a significant discolouration during the experiments indicating some degree of stability; flashing and foaming were however observed. Flashing could be result of high desorption ability of TMBPA, high vapour pressure of PZ, foaming of the solvent system or a combination of these factors. High desorption of 1.5M TMBPA + 1.0M PZ at 80°C shows potentials for lower regeneration energy; its high carrying capacity will result in lower solvent circulation rate. This solvent system thus appears to have a high potential for more efficient CO₂ removal at reduced cost.

5. Conclusions

Method of combined data analysis using absorption-desorption dot plots was very useful in solvent assessment from rapid screening experiments. Bis-(3-dimethylaminopropyl) amine (TMBPA) and tetraethylenepentamine (TEPA) showed good potential as solvents for CO₂ absorption. TEPA has both high absorption rate and capacity but lower desorption ability under the experimental conditions. TMBPA showed very high carrying capacity for CO₂ and relatively good kinetics. It requires a promoter for increased absorption rate, particularly on approach to equilibrium. Promoting 1.5M TMBPA with 1.0M MEA and 1.0M DMPDA showed higher foaming tendency while promoting with 1.0M MAPA showed lower desorption degree. Promoting 1.5M TMBPA with 1.0M PZ was found to have the best overall performance in terms of potential for efficient CO₂ removal at reduced cost for all the systems tested. Its cyclic capacity in molCO₂/mol amine was found 70% more than 5M MEA and it removes 41% more CO₂ per cycle per liter solution than 5M MEA at test conditions.

Acknowledgements

This publication forms a part of the BIGCO₂ project, performed under the strategic Norwegian research program Climit. The authors acknowledge the partners: StatoilHydro, GE Global Research, Statkraft, Aker Kværner, Shell, TOTAL, ConocoPhillips, ALSTOM, the Research Council of Norway (178004/I30 and 176059/I30) and Gassnova (182070) for their support.

References

1. R.K. Pachauri and A. Reisinger, (Eds.), *Climate Change 2007: Synthesis Report*, IPCC (2007).
2. A. B. Rao and E. S. Rubin, *Environ. Sci. Technol.* 36 (2002) 4467-4475.
3. P. Singh, J. P. M. Niederer and G. F. Versteeg, *Int. J. Greenh. Gas Con.* 1(2007) 5-10.
4. U. E. Aronu and H. F. Svendsen, *Rochelle Research Review Meeting*, Jan 10 -11, 2008.
5. A. Dallos, T. Altsach and L. Kotsis, *J. Therm. Anal. Calori.* 65(2001) 419-423.
6. G. F. Versteeg, L. A. J. Van Duck, W. P. M. Van Swaaij, *Chem. Eng. Commun.* 144 (1996) 113-158.
7. G. Xu, C. Zhang, S. Qin, and Y. Wang, *Ind. Eng. Chem. Res.* 31 (1992) 921-7.
8. T. Chakravarty, U. K. Phukan and R.H. Weiland, *Chem. Eng. Prog.* 81(1985) 32-6.
9. U. E. Aronu, H. F. Svendsen, K. A. Hoff and O. Juliussen, *Energy Procedia* 1 (2009) 1051-1057
10. S. Ma'mun, H. F. Svendsen, K. A. Hoff and O. Juliussen, *Energy Convers. Manage.* 48(2007) 25-258.
11. U. E. Aronu, H. F. Svendsen and K. A., *Int. J. Greenh. Gas Con.* (2010) article in press
12. L. E. Hakka and A. M. Ouimet, Canadian Patent 2528205, Dec. 23, 2004.