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Decentralized and Fixed-Structure H_∞ Control in MATLAB

Pascal Gahinet and Pierre Apkarian

***Abstract*— This paper presents two new MATLAB-based tools for tuning linear control systems in the frequency domain: HINFSTRUCT and LOOPTUNE. These tools can directly tune control architectures with multiple feedback loops and multiple fixed-order, fixed-structure control elements. The controller parameters are tuned using non-smooth H_∞ optimization but little a-priori knowledge of H_∞ theory is required to use the tools. This makes them ideally suited for real-world applications where the control system structure and complexity are constrained.**

I. Introduction

H_∞ theory [1]–[4] provides powerful techniques for synthesizing controllers in the frequency-domain. Typical design requirements such as speed of response, control bandwidth, disturbance rejection, and robust stability can be expressed as constraints on the gain (H_∞ norm) of well-chosen closed-loop transfer functions. In turn, efficient algorithms and software tools are available to synthesize MIMO controllers that satisfy such gain constraints [1], [5], [6].

Yet existing H_∞ synthesis tools have practical limitations that have slowed their adoption in industry. H_∞ controllers are monolithic whereas most embedded control architectures are decentralized collections of simple control elements such as gains and PID controllers. H_∞ controllers tend to be opaque and complex (high number of states) whereas embedded controllers tend to be intuitive and have low complexity. And recasting the design requirements as a single aggregate H_∞ constraint can be challenging for engineers. As a result, hand tuning and optimization-based tuning tend to remain the norm for decentralized control systems.

This paper presents new MATLAB tools for *Structured H_∞ Synthesis* that overcome the limitations listed above. These tools are part of MathWorks' Robust Control Toolbox [6] and leverage state-of-the-art nonsmooth optimizers [7], [8] to directly and efficiently tune arbitrary control architectures. By "arbitrary," we mean any single- or multiple-loop block diagram arrangement containing any number and type of linear control elements, from simple gains and PIDs to more complex notch filters and observer-based controllers. Some of these tools also automate the H_∞ formulation, allowing users to tune the controller elements directly from high-level specifications. Finally, despite the lack of convexity, these tools perform well in practice, both in terms of speed of execution and quality of the solutions.

P. Gahinet is with The MathWorks, 3 Apple Hill, Natick, MA 01760-2098, USA `Pascal.Gahinet@mathworks.com`

Pierre Apkarian is with ONERA and Institut de Mathématiques, Université Paul Sabatier, 2, av. Ed. Belin, 31055, Toulouse, France `Pierre.Apkarian@onera.fr`

The paper is organized as follows. Section 2 discusses the standard formulation of structured H_∞ synthesis and the representation of tunable control elements. Section 3 presents HINFSTRUCT, a general-purpose tool for structured H_∞ synthesis. Section 4 presents LOOPTUNE, a more specialized tool that automates mainstream tuning tasks. Finally, Sections 5 and 6 illustrate the potential of this technology with two non-trivial examples.

II. Framework for Tuning Decentralized Control Structures

As mentioned earlier, our starting point is any linear control architecture with one or more fixed-structure blocks to tune, for example the feedback structure shown in Figure 6 where the shaded blocks are tunable. Since there are infinitely many possible architectures, we use a standardized representation called *Standard Form* that is both general and convenient to work with. The *Standard Form* is depicted in Figure 1 and consists of two main components:

- An LTI model $P(s)$ that combines all fixed (non tunable) blocks in the control system
- A structured controller $C(s) = \mathrm{Diag}(C_1(s), \ldots, C_N(s))$ that combines all tunable control elements. Each control element $C_j(s)$ is assumed to be linear time invariant and to have some prescribed structure.

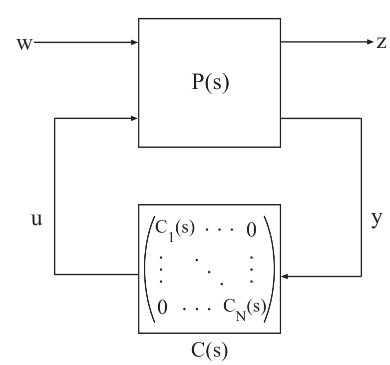

Fig. 1. Standard Form for Structured H_∞ Synthesis

External inputs to the system such as reference signals and disturbances are gathered in w and performance-related outputs such as error signals are gathered in z. With the partition

$$\begin{pmatrix} z \\ y \end{pmatrix} = P \begin{pmatrix} w \\ u \end{pmatrix} = \begin{pmatrix} P_{11} & P_{12} \\ P_{21} & P_{22} \end{pmatrix} \begin{pmatrix} w \\ u \end{pmatrix},$$

the closed-loop transfer function from w to z is given by the linear-fractional transformation (LFT) [9]:

$$T_{wz}(s) = F_l(P, C) := P_{11} + P_{12}C(I - P_{22}C)^{-1}P_{21}. \quad (1)$$

It is well known from Robust Control theory that any block diagram can be rearranged into this Standard Form by isolating the tunable blocks and collapsing the rest of the diagram into $P(s)$. The resulting model has the same structure as the uncertain models used in μ analysis (with the uncertainty blocks $\Delta_j(s)$ replaced by the control elements $C_j(s)$) [10]–[12]. Figure 1 is also reminiscent of standard H_∞ synthesis [1] but differs in one key aspect, namely, the special structure of the controller $C(s)$. Since systematic procedures and automated tools are available to transform any architecture to the Standard Form of Figure 1, we henceforth assume that the control architecture is specified in this form.

The next challenge is to describe the tunable control elements. Again we are faced with a wide range of possible structures, from simple gains and PIDs to more complex lead-lag and observer-based controllers. Since our approach is based on optimization, it is natural to use parameterizations of such components. For example, a PID can be parameterized by four scalars K_p, K_i, K_d, T_f as

$$C_j(s) = K_p + \frac{K_i}{s} + \frac{K_d s}{T_f s + 1}. \quad (2)$$

Similarly, a state-space model with fixed order n can be parameterized by four matrices A, B, C, D of suitable sizes. This approach is useful to create a library of basic tunable blocks that includes static gains, PIDs, fixed-order transfer functions, and fixed-order state-space models. However, such library leaves out many useful control elements. For example, we cannot use the generic transfer function parameterization to model the lowpass and notch filters

$$\frac{a}{s+a}, \quad \frac{s^2 + 2\zeta_1\omega_0 s + \omega_0^2}{s^2 + 2\zeta_2\omega_0 s + \omega_0^2} \quad (3)$$

because of the couplings between numerator and denominator parameters.

Rather than growing the library of pre-defined tunable blocks, a more scalable approach is to let users create custom parameterizations of control elements. To do this, we introduce a basic building block called "real parameter" (`realp`). If a is a real parameter, then any well-posed rational function $R(a)$ can be written as the LFT:

$$R(a) = F_l(M, a \otimes I) \quad (4)$$

where M is a fixed matrix and $a \otimes I := \mathrm{Diag}(a, \ldots, a)$ [13]. More generally, any rational function of the scalar- or matrix-valued parameters $a_1, \ldots, a_M$ can be represented as an LFT model involving repeated copies of the parameters $a_1, \ldots, a_M$. Moreover, such LFT models can be constructed automatically by recasting `realp` arithmetic in terms of LFT model interconnections [14, p. 165]. Since any interconnection of LFT models is an LFT model, and the Standard Form of Figure 1 is itself an LFT model, it is easily seen that if the control element $C_j(s)$ is parameterized as a rational function of $a_1, \ldots, a_M$, the Standard Form can be rearranged so that $C_j(s)$ is replaced by a block-diagonal matrix with copies of $a_1, \ldots, a_M$ along the diagonal. In other words, we can absorb the specific structure of $C_j(s)$ into $P(s)$ and keep only the low-level tunable parameters $a_1, \ldots, a_M$ in the $C(s)$ block of Figure 1. Note that unlike μ-analysis, "repeated" blocks do not affect the optimization outcome and only incur some small overhead.

To see how this comes together in MATLAB, first consider the lowpass filter $F(s) = \frac{a}{s+a}$ where a is tunable. This tunable element is specified by:

```
a = realp('a',1);  % a is initialized to 1
F = tf(a,[1 a]);   % creates a/(s+a)
```

This automatically builds the following LFT representation of $F(s)$:

$$F(s) = F_l\left(\begin{pmatrix} 0 & 0 & 1 \\ 1/s & -1/s & 0 \\ 1/s & -1/s & 0 \end{pmatrix}, \begin{pmatrix} a & 0 \\ 0 & a \end{pmatrix}\right). \quad (5)$$

Next consider the observer-based controller

$$\begin{aligned} \dot{\hat{x}} &= A\hat{x} + Bu + L(y - C\hat{x} - Du) \\ &= (A - BK - LC + LDK)\hat{x} + Ly \\ u &= -K\hat{x} \end{aligned} \quad (6)$$

where the gain matrices K, L are tunable. This observer structure is specified as:

```
% For a plant with nx states, nu controls,
% and ny measurements:
K = realp('K',zeros(nu,nx));
L = realp('L',ones(nx,ny));
OBC = ss(A-B*K-L*(C-D*K),L,-K,0);
```

The resulting LFT parameterization `OBC` of the observer structure has three copies of the parameter `K` and two copies of the parameter `L`. Note that in both examples, it is possible to construct more efficient parameterizations using a single copy of `a`, `K`, `L`. Yet the convenience of the syntax shown above more than makes up for the small overhead incurred by the extra block copies.

III. Structured H_∞ Synthesis

Now that we have a framework for describing arbitrary control architectures and linear control elements, we turn to the question of using H_∞ synthesis to tune the controller parameters in the Standard Form of Figure 1. H_∞ synthesis is a frequency-domain method for enforcing typical control design requirements. At the heart of the method is the H_∞ norm, which measured the peak input/output gain of a given transfer function:

$$\|H(s)\|_\infty := \max_\omega \overline{\sigma}(H(j\omega)). \quad (7)$$

In the SISO case, this norm is just the peak gain over frequency. In the MIMO case, it measures the peak 2-norm of the frequency response $H(j\omega)$ over frequency.

It is well-known from robust control theory [15] that classical design requirements (bandwidth, roll-off, disturbance attenuation, stability margins) can be recast as normalized H_∞ constraints of the form

$$\|W_j(s)T_j(s)\|_\infty < 1 \quad (8)$$

where $T_j(s)$ is some suitable closed-loop transfer function and $W_j(s)$ is a weighting function that reflects the requirement nature and parameters. So a typical controller tuning task consists of adjusting the controller parameters to satisfy the constraints

$$\|W_j(s)T_j(s)\|_\infty < 1, \quad j = 1, \ldots, M. \quad (9)$$

Each transfer function T_j can be expressed as an LFT model depending on the structured controller $C(s) := \mathrm{Diag}(C_1(s), \ldots, C_N(s))$. Now, introduce

$$H(s) := \mathrm{Diag}(H_1(s), \ldots, H_M(s)). \quad (10)$$

Clearly (9) is equivalent to $\|H(s)\|_\infty < 1$ and the Standard Form of $H(s)$ is of the form

$$H(s) = F_l\left(P(s), \mathrm{Diag}(C(s), \ldots, C(s))\right) \quad (11)$$

where $P(s)$ is a fixed LTI model. So constraining two or more closed-loop transfer functions $T_j(s)$ leads to repeating the controller $C(s)$ multiple times in the Standard Form. The resulting block-diagonal controller structure is beyond the scope of standard H_∞ algorithms but poses no problem in our framework since this merely amounts to repeating the tunable blocks along the diagonal (see Section II for a discussion of repeated blocks). This is an important advantage over traditional H_∞ synthesis where all requirements must be expressed in terms of a *single* closed-loop transfer function.

Summing up, decentralized controller tuning can be recast as a structured H_∞ synthesis problem where the controller has a block-diagonal structure, each block being parameterized and possibly repeated. In turn, we can use the nonsmooth algorithms described in [7], [16], [17] to optimize the controller parameters and enforce the constraint $\|H(s)\|_\infty < 1$. The MATLAB sofware described here is based on [7], [18] and consists of three main components:

- Simple objects to specify tunable parameters (`realp`) and elementary control elements such as gains, low-order transfer functions, and PIDs
- Overloaded arithmetic and interconnection algebra to automatically build the Standard Form of $H(s)$ by combining/connecting together ordinary LTI models, tunable elements, and weighting functions
- The `hinfstruct` function for minimizing the H_∞ norm of $H(s)$ with respect to the tunable controller parameters. This function can be seen as the counterpart of `hinfsyn` for structured H_∞ synthesis

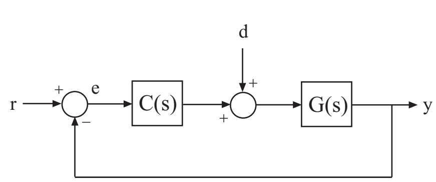

Fig. 2. Elementary feedback loop.

To get a feel for these tools, consider the simple scenario where the requirements for the feedback loop of Figure 2 can be expressed as

$$\|w_S S\|_\infty < 1, \quad \|w_T T\|_\infty < 1 \quad (12)$$

where $S = 1/(1 + L)$, $T = L/(1 + L)$, $L = GC$, and w_S, w_T are suitable frequency-weighting functions. Also assume that $C(s)$ is constrained to be a PID controller. Using the sofware, you can construct a parametric model of $H(s) = \mathrm{Diag}(w_S S, w_T T)$ as follows:

```
G = tf([1 2],[1 5 10]);       % plant model
C = ltiblock.pid('C','pid'); % tunable PID
S = feedback(1,G*C);
T = feedback(G*C,1);
H0 = blkdiag(wS * S, wT * T);
```

The result `H0` is a MATLAB representation of the (untuned) Standard Form for $H(s)$ and depends on the tunable PID block `C`. Next invoke `hinfstruct` to tune the PID controller gains so as to enforce $\|H(s)\|_\infty < 1$:

```
H = hinfstruct(H0);
```

The output `H` contains the tuned Standard Form of $H(s)$. Note that `hinfstruct` actually minimizes the H_∞ norm of $H(s)$ but can be configured to terminate as soon as the target value of 1 is achieved. You can now access the tuned value of the PID controller `C` with

```
getBlockValue(H,'C')
```

or plot the magnitude of $H(j\omega)$ with

```
bodemag(H)
```

Note that `hinfstruct` can be configured to automatically run multiple optimizations from randomly generated starting points. This helps mitigate the local nature of the optimizer and increases the likelihood of finding parameter values that meet the design requirements. See [19], [20] for more details and examples regarding `hinfstruct`.

IV. Automatic Tuning of Feedback Loops

While `hinfstruct` addresses the first two practical limitations of traditional H_∞ synthesis tools, it still requires expertise for turning typical design specifications into a well-posed H_∞ optimization problem. This difficulty is exacerbated in multi-loop control systems because of scaling and coupling issues. For example, a poor choice of units in one feedback channel may skew the sensitivity function and lead to an ill-posed H_∞ problem [15, p. 5-8]. Also, classical one-loop-at-a-time stability margins may be misleading when cross-coupling exists between feedback loops [21]. Such challenges led us to seek ways to automate the H_∞ formulation of high-level requirements. This turns out to be possible and to often lead to satisfactory results. We now discuss this "push-button" approach and the `looptune` function that embodies it.

Our starting point is the generic MIMO feedback loop of Figure 3 where G represents the "plant" and C represents the overall controller. Any control structure can be rearranged in this fashion by using the measurement signals y and control signals u to separate the controller from the plant. Both G

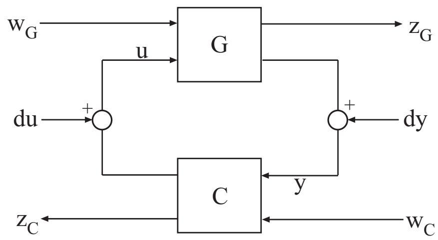

Fig. 3. Generic MIMO feedback loop.

and C may contain tunable elements, which allows for co-tuning of plant and controller parameters. To formulate an H_∞ synthesis problem for this feedback system, observe that most controller tuning tasks involve some combination of the following requirements:

1) **Performance**: The feedback loops should have high gain at low frequency to reject disturbances and follow setpoint changes
2) **Roll off**: The feedback loops should have low gain at high frequency to guard against unmodeled dynamics and measurement noise
3) **Stability**: The feedback loops should be stable with enough margin to sustain typical amounts of gain and phase variations at the plant inputs and outputs.

Typically, the first two requirements amount to shaping the open-loop response to have integral action at low frequency and roll off in excess of -20 dB/decade at high frequency. The transition from high to low open-loop gain occurs in the *gain crossover band* (an interval in the MIMO case since in general it is neither possible nor desirable to make all loops cross at the same frequency). The gain crossover band determines the response time and bandwidth of the control system. Using the standard "mixed-sensitivity" formulation, we can express these loop-shaping requirements as

$$\left\| \begin{pmatrix} W_{LF} S_i \\ W_{HF}(I - S_i) \end{pmatrix} \right\|_\infty < 1 \tag{13}$$

where S_i is the sensitivity function at the plant inputs u and the weighting functions W_{LF}, W_{HF} reflect the desired loop shape. Note that S_i should be replaced by the sensitivity S_o at the plant outputs if there are more controls u than measurements y.

For the stability requirement, we use the notion of multivariable disk margins discussed in [21]. This measure guarantees robustness against simultaneous gain and phase variations at all plant inputs and outputs, which is much stronger than one-loop-at-a-time stability margins. With the notation

$$L(s) = \begin{pmatrix} 0 & G(s) \\ C(s) & 0 \end{pmatrix}, \quad X(s) = (I + L)(I - L)^{-1}, \tag{14}$$

the robust stability condition is

$$\mu(X(s)) < 1/\alpha \tag{15}$$

where $\mu(.)$ denotes the structured singular value for a diagonal block structure [4] and the parameter α is a function of the desired gain and phase margins [21]. For tractability reasons, we replace this condition by:

$$\min_D \max_{\omega \in [\omega_1, \omega_2]} \| D^{-1} X(jw) D \| < 1/\alpha \tag{16}$$

where D is a constant and diagonal scaling matrix and $[\omega_1, \omega_2]$ is some interval containing the gain crossover band. The rationale for this simplification is that (a) stability margins are worst near the gain crossovers, and (b) the gain crossover band is typically narrow enough that we can get away with a constant rather than frequency-dependent D-scaling in the $\mu(.)$ upper bound.

Note that the scaling $D = \begin{pmatrix} D_o & 0 \\ 0 & D_i \end{pmatrix}$ is equivalent to the plant I/O scaling $G \to D_o^{-1} G D_i$. In other words, D automatically corrects scaling issues in the vector signals u and y, e.g., u having both small and large entries due to a poor choice of units. Because the H_∞ norm is not invariant under I/O scaling, this turns out to be essential to formulate a meaningful H_∞ synthesis problem [15, Remark 1]. Finally, (16) is tractable in our framework if we treat the diagonal entries of D as tunable parameters ($D^{-1} X(jw) D$ is an LFT in the controller and scaling matrix D).

Summing up, for a given crossover frequency/band, tuning the controller amounts to finding a scaling D and controller parameter values that satisfy

$$\left\| \begin{pmatrix} W_{LF} D_i^{-1} S_i D_i \\ W_{HF}(I - D_i^{-1} S_i D_i) \end{pmatrix} \right\|_\infty < 1 \tag{17}$$

$$\max_{\omega \in [\omega_1, \omega_2]} \| \alpha D^{-1} X(jw) D \| < 1. \tag{18}$$

Note that we use the scaled input sensitivity $D_i^{-1} S_i D_i$ instead of S_i to take advantage of the u scaling provided by D.

The `looptune` function [6] formulates and solves this H_∞ optimization problem. The basic interface is

```
[G,C] = looptune(G0,C0,wc,Req1,Req2,...)
```

where `G0,C0` are (untuned) parametric models of G and C, `wc` is the target crossover frequency/band, and the optional arguments `Req1,Req2,...` specify additional requirements such as maximum gain or setpoint tracking. Note that `wc` can be omitted and replaced by more sophisticated loop shaping requirements, thus providing a fair amount of flexibility.

Is this approach too simplistic to be useful? While we made some generalizations and cannot expect good results in all situations, `looptune` has proven very effective in many realistic and non trivial applications (see examples below). Meanwhile `looptune` brings some key benefits:

- It only requires a basic understanding of frequency-domain notions such as bandwidth, gains, and open-loop response
- It enforces a strong notion of stability margins
- It automatically takes care of subtle signal scaling issues.

Altogether this makes `looptune` a valuable tool for quickly tuning decentralized and fixed-structure control systems.

V. Distillation Column Example

This first example applies `looptune` to the control of a distillation column [15]. The control architecture is shown in Figure 4 and consists of a 2-by-2 decoupling matrix in series with two PI controllers for the reflux `L` and boilup `V`. The goal is to independently control the tops and bottoms concentrations `yD` and `yB` with a response time of 10 minutes. The plant model is

$$G(s) = \frac{1}{75s+1}\begin{pmatrix} 87.8 & -86.4 \\ 108.2 & -109.6 \end{pmatrix}$$

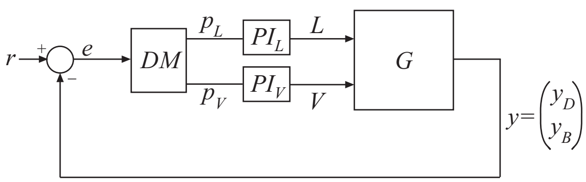

Fig. 4. Control architecture for distillation column.

To tune this control system, first create parametric models for each control element:

```
DM = ltiblock.gain('Decoupler',eye(2));
PI_L = ltiblock.pid('PI_L','pi');
PI_V = ltiblock.pid('PI_V','pi');
```

Then construct a parametric model of the overall controller with inputs $\begin{pmatrix} r \\ y \end{pmatrix}$ and outputs $u = \begin{pmatrix} L \\ V \end{pmatrix}$:

```
I = eye(2);
C0 = blkdiag(PI_L,PI_V) * DM * [I,-I];
```

Finally, call `looptune` with $[0.1, 1]$ as target gain crossover band (0.1 rad/min corresponds to a 10 minutes response time):

```
wc = [0.1,1];
[~,C] = looptune(G,C0,wc);
```

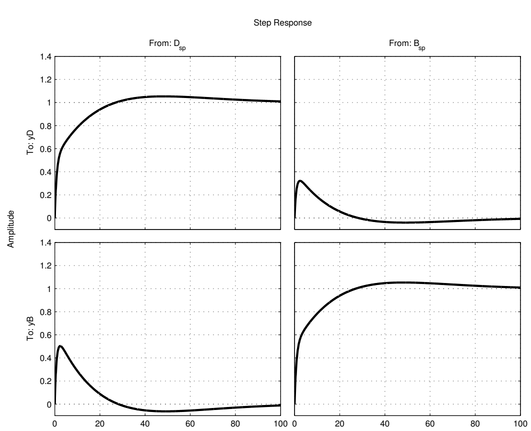

Fig. 5. Response to setpoint changes in tops and bottoms concentrations.

Starting from the initial values $PI_L(s) = PI_V(s) = 0.001/s$ and $DM = I_2$, `looptune` minimizes the H_∞ norms in (17)-(18) and terminates with a norm of 1.24, close to the target value 1. The output `C` is the tuned controller with the following values for the decoupling matrix and PI gains:

$$\begin{aligned} PI_L(s) &= 2.18 + 0.079/s \\ PI_V(s) &= 1.46 + 0.053/s. \\ DM &= \begin{pmatrix} 1.09 & -0.67 \\ 1.26 & -1.30 \end{pmatrix}. \end{aligned}$$

The corresponding responses to step changes in tops and bottoms setpoints are shown in Figure 5. Further analysis shows that this design has good disturbance rejection properties and stays clear from inverting the plant at DC, a strategy that yields excellent setpoint tracking but poor disturbance rejection and stability margins (see demo in [6] for details).

VI. Helicopter Example

This second example tackles a more challenging helicopter control problem. We use an 8-state model of the Westland Lynx helicopter at the hovering trim condition. The controller generates commands d_s, d_c, d_T in degrees for the longitudinal cyclic, lateral cyclic, and tail rotor collective using measurements of θ, ϕ, p, q, r (pitch and roll angles and roll/pitch/yaw rates). For details and data, see [22] and the demo in [6]. The controller structure is shown in Figure 6 and consists of two feedback loops:

- The inner loop (static output feedback SOF) provides stability augmentation and decoupling
- The outer loop (PI controllers PI1-PI3) provides the desired setpoint tracking performance.

The main control objective is to track setpoint changes in θ, ϕ, r with zero steady-state error, settling times of about 2 seconds, minimal overshoot, and minimal cross-coupling.

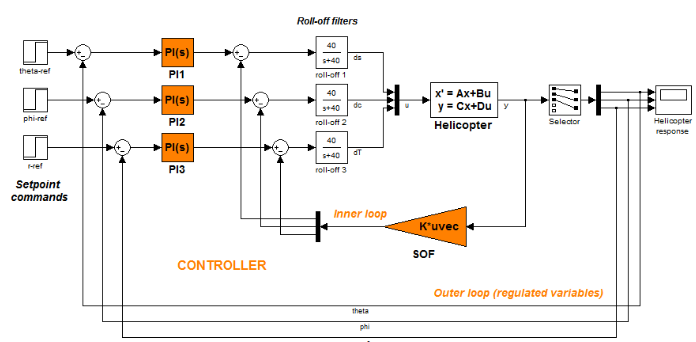

Fig. 6. Control architecture for Westland Lynx helicopter.

Since the helicopter is modeled in Simulink we use the `slTunable` interface to quickly set up the `looptune` optimization. With this interface you just specify the Simulink blocks to tune, the measurement and control signals (controller I/Os), and the I/O signals of interest for closed-loop analysis:

```
ST0 = slTunable('helico',...
                {'PI1','PI2','PI3','SOF'});
ST0.addControl('u')
ST0.addMeasurement('y')
ST0.addIO({'theta_ref','phi_ref','r_ref'},'in')
ST0.addIO({'theta','phi','r'},'out')
```

This information is used to automatically parameterize the tuned blocks and linearize the Simulink model to extract the plant model G and a parametric model of the controller C. Note that the static-output-feedback gain is initialized to zero and the PI controllers to $1 + 1/s$, values for which the closed-loop response is unstable.

We want the outer loop to settle in about 2 seconds so the open-loop bandwith should be at least 2 rad/s (based on first-order characteristics). The inner loop must typically be faster so we seek a gain crossover band between 10 and 30 rad/s:

```
wc = [10,30];
```

Because there are fewer actuators (3) than measurements (5), integral action in the open-loop response is not enough to guarantee that θ, ϕ, r will track the setpoint commands $\theta_{\rm ref}, \phi_{\rm ref}, r_{\rm ref}$. We therefore add an explicit tracking requirement stipulating a 2-second response time and a maximum steady-state error of 0.001:

```
TR = TuningGoal.Tracking(...
        {'theta_ref','phi_ref','r_ref'},...
        {'theta','phi','r'},2,0.001);
```

We can now tune the controller parameters with `looptune`:

```
ST = ST0.looptune(wc,TR);
```

The final H_∞ norm is 1.28, again close to 1, and the closed-loop step responses are shown in Figure 7. These responses settle in less than two seconds with no overshoot and small cross-coupling. The tuned values are:

$$\begin{aligned}
PI_1(s) &= 0.52 + 11.9/s \\
PI_2(s) &= -0.13 - 9.27/s \\
PI_3(s) &= -0.86 - 8.53/s \\
SOF &= \begin{pmatrix} 6.24 & -0.97 & -0.0048 & 1.07 & -0.046 \\ -0.63 & -2.47 & -0.0062 & -0.083 & -0.18 \\ -0.81 & 1.23 & -1.44 & -0.21 & 0.13 \end{pmatrix}
\end{aligned}$$

Tuning these 21 parameters starting from an unstable initial guess took 20 seconds on a 64-bit PC with a 2.4 GHz dual-core processor and 6 GB of RAM.

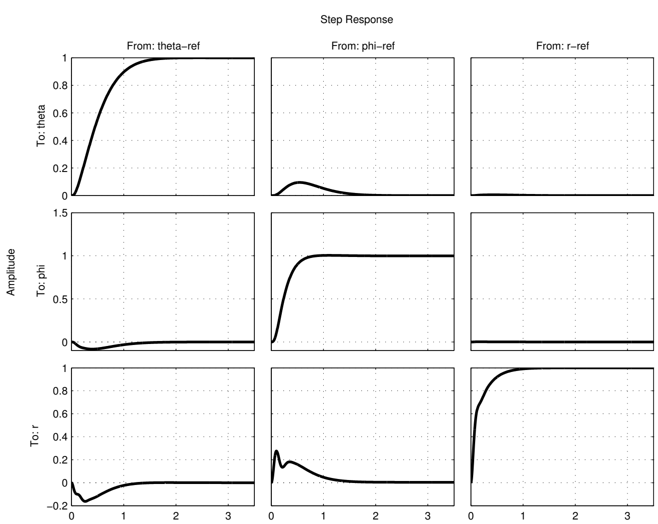

Fig. 7. Closed-loop responses to θ, ϕ, r commands.

Conclusion

We have presented a new methodology and tool set for tuning fixed-structure SISO or MIMO control systems. While our approach is rooted in H_∞ theory, it is clear that these tools and techniques are not restricted to Robust Control applications and can be seen as a systematic framework for tuning decentralized control architectures and exploring the trade-offs between performance and complexity.

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