

أرامكو السعودية
Saudi Aramco



Detailed Energy Assessment at Oil Refinery: Tools and Results

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Synopsis

- First Time Pinch Analysis was applied in SA Refinery (2003)
- Expected Savings ~ 10-15% of Baseline Energy Cost
- Actual Savings Identified \approx 37% (despite low fuel/power costs)

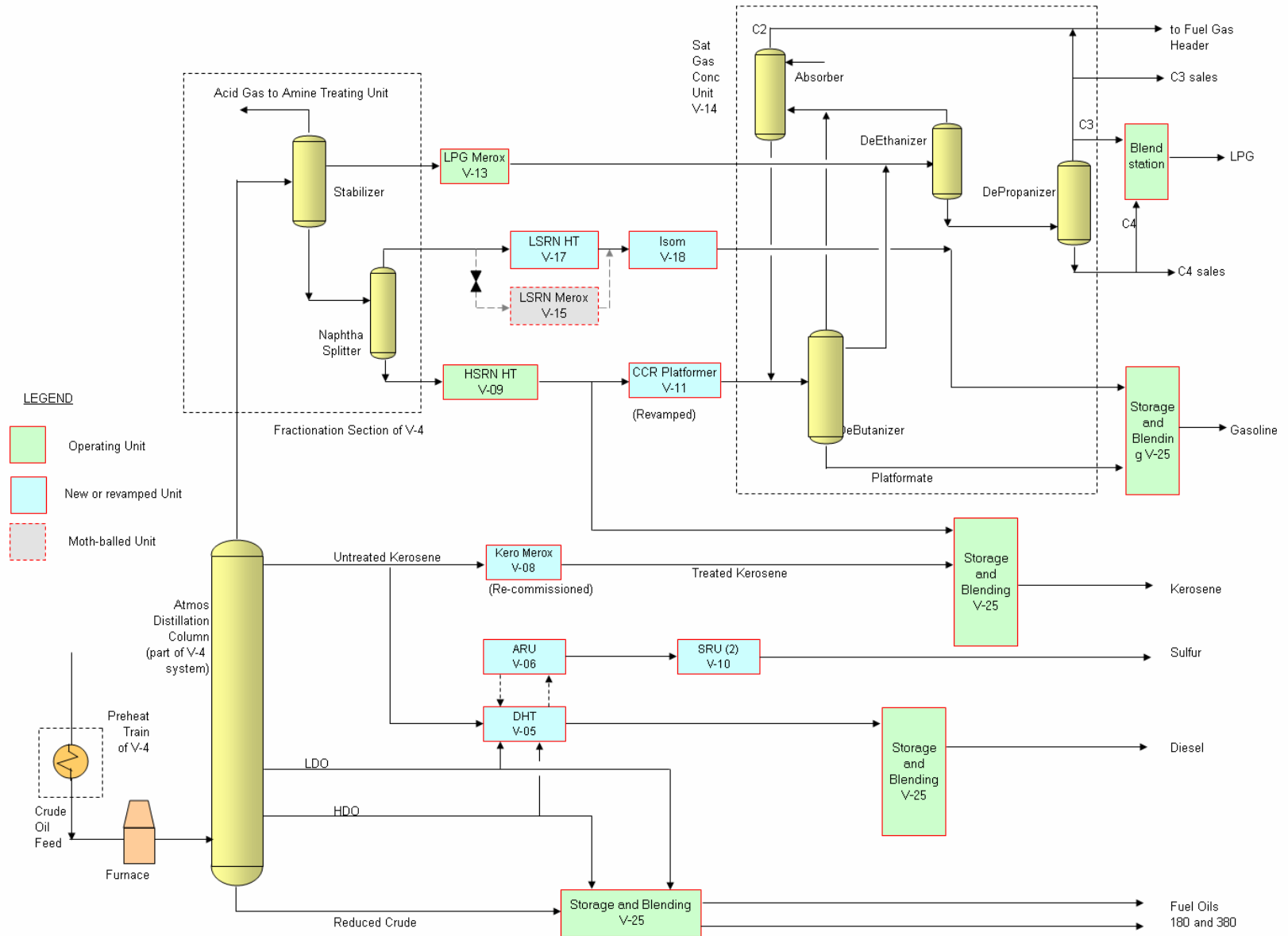
Introduction

- SA management adopted Energy Policy in 2000 with the goal of 50% reduction in corporate energy index over 10 years
- Energy Systems Unit was established to help plants w.r.t. technology transfer

Scope of Work

- Fuel Savings via Heat Recovery optimization (using Pinch Analysis)
- Power Reduction via ASDs
- Optimization of Combined Heat & Power (CHP) design and operation
- Development and deployment of on-line Energy Indices (Solomon EII)

Simplified Refinery schematic, 2006



Pinch Analysis - Scope

- Overall Plant Energy Balance
- Thermal Targets and HEN design for:
 - ◆ CDU (retrofit)
 - ◆ HSRN hydrotreater (retrofit)
 - ◆ DHT complex (new)
 - ◆ CCR (revamp)
 - ◆ LSRN hydrotreater and Isomerization (new)

Pinch Analysis – Procedure

- Prepare reconciled HMB from RIS for existing units (using Data Recon s/w package)
- Confirm HMB with PMT for new units
- Develop proposed new HEN designs
- Discuss with refinery/FPD/PMT for agreement
- HX sizing
- Capital cost estimating
- Project feasibility analysis
- Report preparation

Composite Curves – CDU

(c)DPI UMIST V:1.7 Beta

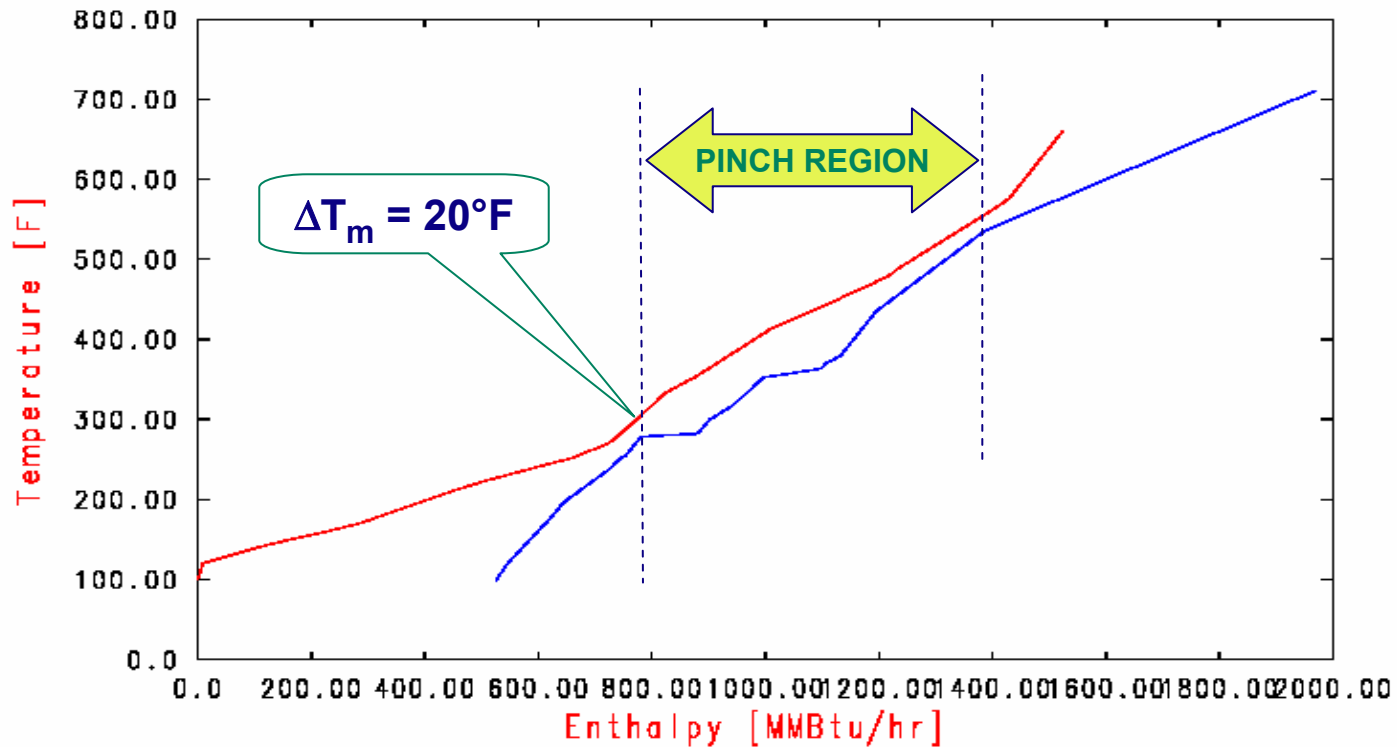
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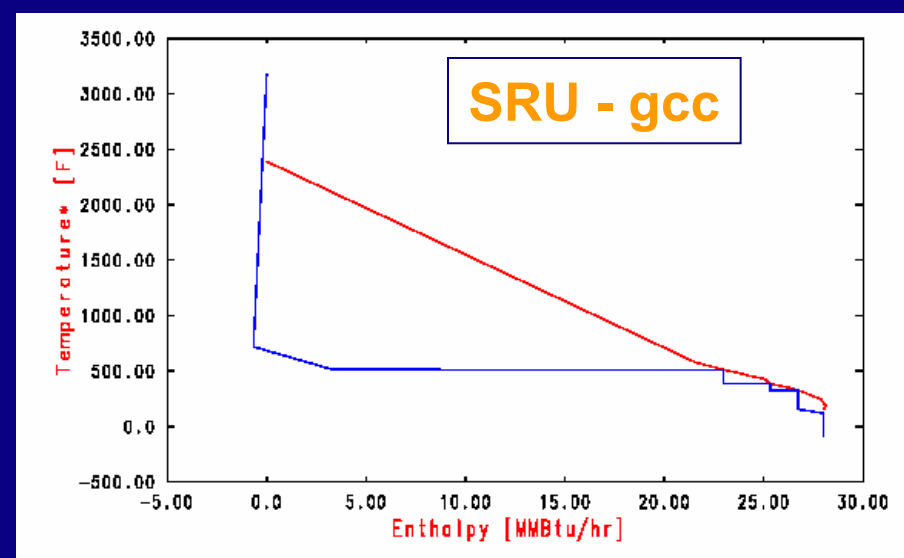
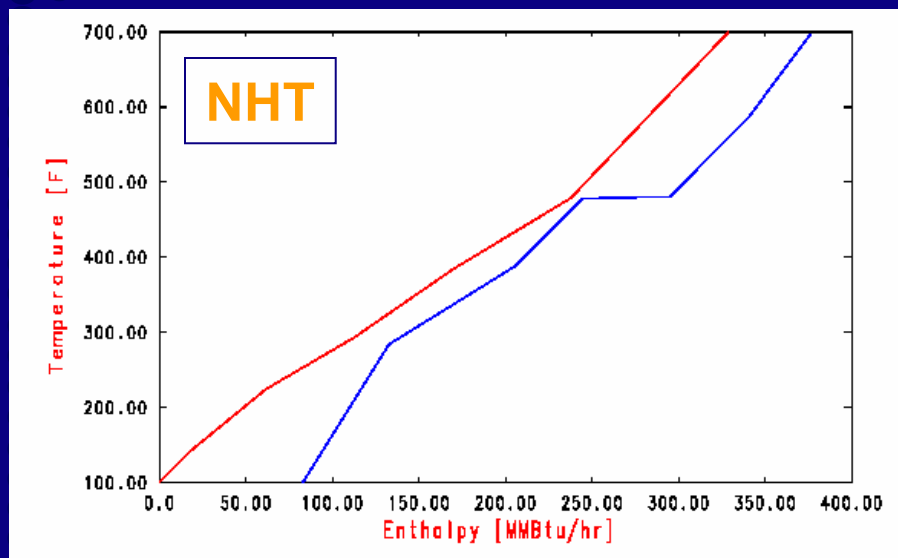
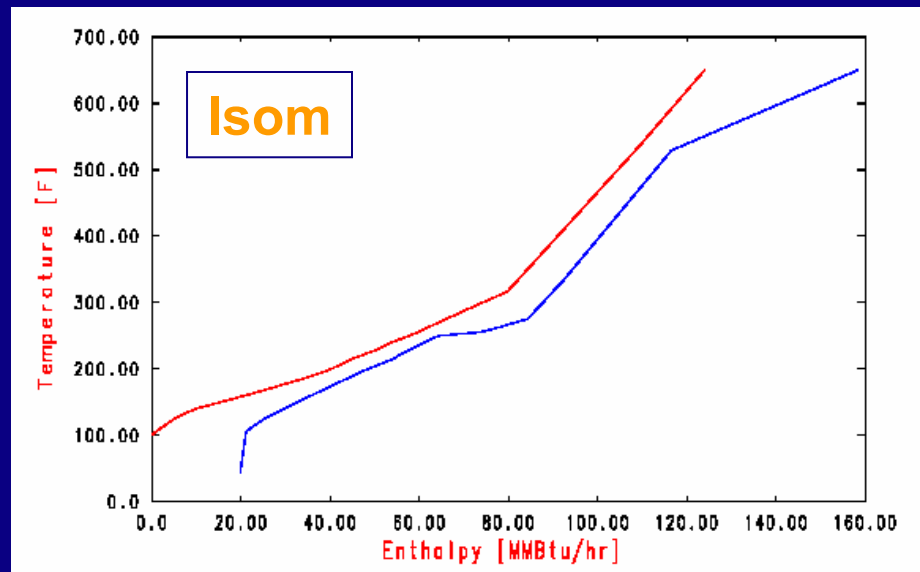
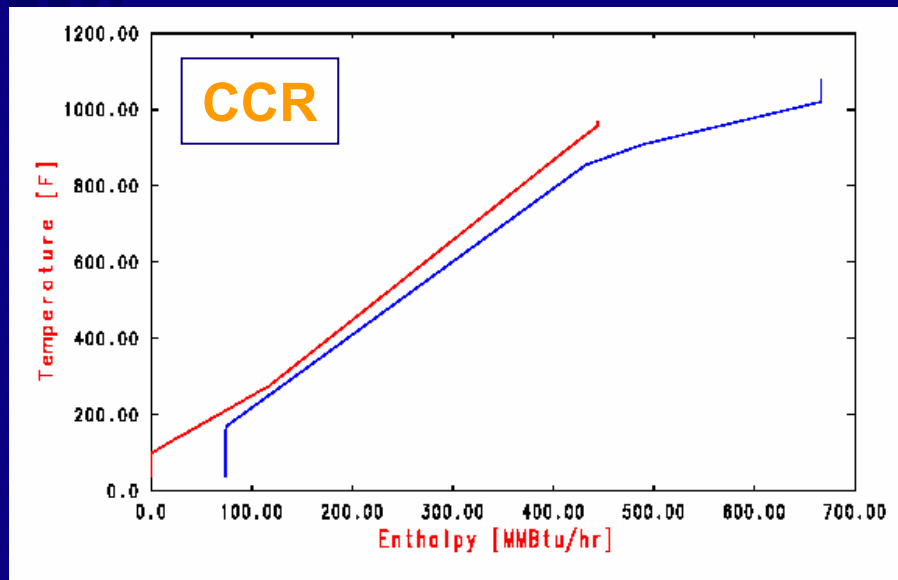
Composite Curves



Target Savings – CDU (details)

| $\Delta T = 20^{\circ}\text{F}$ | Actual PFD | Pinch Target | Savings Potential | | |
|---------------------------------|---------------|-----------------|-------------------|-------|--------|
| | | | MMBtu/h | % | K\$/yr |
| Total heating duty | 581.7 | 502.9 | 78.8 | 13.5 | |
| Total cooling duty | 661.4 | 581.8 | 79.6 | 12.0 | |
| Fuel supplied | 684.4 | 591.6 | 92.7 | 13.5 | 973.7 |
| Steam | 0.0 | 0.0 | 0.0 | 100.0 | 0.0 |
| 60 Steam Gen | 0.0 | 0.0 | 0.0 | 100.0 | 0.0 |
| Air cooling | 523.7 | 573.0 | -49.3 | -9.4 | -53.9 |
| Sea Water cooling | 137.7 | 8.8 | 128.9 | 93.6 | 909.5 |
| | | | | | 1829.3 |
| Energy Cost, K\$/yr | 8729 | 6900 | | 21.0 | 1829 |

Composite Curves for others ...



Overall Thermal Energy Targets

| Unit No. | Name | Normal feed rate | Optimum DT, °F | Actual Energy Consumption | | | Target Energy Consumption | | | Savings K\$/yr | Potential % |
|----------|------------------------|------------------|----------------|---------------------------|-----------------|-------------|---------------------------|-----------------|-------------|----------------|-------------|
| | | | | Heating MMBtu/h | Cooling MMBtu/h | Cost K\$/yr | Heating MMBtu/h | Cooling MMBtu/h | Cost K\$/yr | | |
| | | | | V-04 | CDU | 235 MBD | 20 | 581.7 | 661.4 | 8729 | 502.9 |
| V-09 | Heavy NHT | 37 MBD | 16 | 85.1 | 120.9 | 1332 | 49.3 | 85.1 | 468 | 864 | 64.8 |
| V-05 | DHT + ARU | 95 MBD | 24 | 255.2 | 347.8 | 4523 | 162.3 | 254.9 | 2369 | 2154 | 47.6 |
| V-10 | SRU (2 trains) | 190 TPD | 40 | 10.4 | 65.0 | -771 | 1.8 | 56.4 | -1013 | 242 | 31.4 |
| V-11 | CCR (revamp) | 47 MBD | 24 | 265.0 | 116.4 | 3645 | 222.4 | 73.8 | 3012 | 633 | 17.4 |
| V17, 18 | LSRN ht+isom | 12 MBD | 18 | 59.9 | 45.3 | 958 | 34.3 | 19.8 | 528 | 430 | 44.9 |
| V-32 | Utilities (CHP) | future | n/a | | | | | | | 0 | 0.0 |
| | | | | 1257.4 | 1356.8 | 18417 | 973.0 | 1071.8 | 12264 | 6152.5 | 33.4 |
| | Blue = New Unit | | | | | | | | | | |
| | Purple = Revamped Unit | | | | | | | | | | |
| | Black = Existing Unit | | | | | | | | | | |

SURPRISE ! Significant Cost Savings Potential even in new licensed processes !!

HEN simulation – CDU (1/3)

| | | E-1 | E-2 | E-3 | E-4 | E-5 | E-6 | E-7 | E-8 | E-9 |
|-------------------------|--------------------|----------------------|---------------|----------------------|-----------------------|-----------------------|----------------------|--------------------------|------------------|-------------------------|
| Name / Service | | Crude vs Naphtha P/A | Crude vs Kero | Crude vs LDO Product | Crude vs No 1 LDO P/A | Crude vs No 2 LDO P/A | Crude vs HDO Product | Crude vs Cold Red. Crude | Crude vs HDO P/A | Crude vs Hot Red. Crude |
| No. of shells/coils | | 8 | 2 | 4 | 4 | 4 | 2 | 16 | 4 | 8 |
| | series | 2 | 1 | 2 | 2 | 2 | 1 | 4 | 2 | 4 |
| | parallel | 4 | 2 | 2 | 2 | 2 | 2 | 4 | 2 | 2 |
| Area per shell, ft2 | | 4078 | 4530 | 4821 | 4327 | 4327 | 4004 | 3197 | 4714 | 5072 |
| Total area, ft2 | | 32624 | 9060 | 19282 | 17308 | 17308 | 8008 | 51149 | 18858 | 40579 |
| Max duty, MMBtu/h | | | | | | | | | | |
| <u>Hot stream</u> | | | | | | | | | | |
| Description | | Heavy Naphtha P/A | Kero Prod | LDO Prod | LDO PA 1 | LDO PA 2 | HDO Prod | Cold Red. Crude | HDO PA 1 | Hot Red. Crude |
| Flow | tag no. | | | | | | | | | |
| | mean - μ | 480.4 | 152.9 | 178.4 | 200.8 | 280.3 | 48.2 | 308 | 319.6 | 307.8 |
| | std dev - σ | | | | | | | | | |
| | units | m3/h | m3/h | m3/h | m3/h | m3/h | m3/h | m3/h | m3/h | m3/h |
| | conversion | 1.338 | 1.415 | 1.454 | 1.415 | 1.415 | 1.314 | 1.737 | 1.282 | 1.309 |
| | Klb/h meas | 643 | 216 | 259 | 284 | 397 | 63 | 535 | 410 | 403 |
| | Klb/h used | 1810 | 212 | 558 | 262 | 393 | 414 | 1174 | 584 | 1174 |
| | phase | liquid | liquid | liquid | liquid | liquid | liquid | liquid | liquid | liquid |
| | HHV, Btu/lb | | | | | | | | | |
| | furnace eff | | | | | | | | | |
| Specific gravity | | 0.660 | 0.717 | 0.792 | 0.789 | 0.789 | 0.859 | 0.949 | 0.855 | 0.949 |
| Liquid density, g/cc | | 0.607 | 0.642 | 0.660 | 0.642 | 0.642 | 0.596 | 0.788 | 0.582 | 0.594 |
| Temp In | tag no. | | | | | | | | | |
| | °C mean - μ | 149.0 | 173.0 | 226.2 | 239.7 | 239.7 | 316.4 | 227.7 | 324.2 | 353.6 |
| | std dev - σ | | | | | | | | | |
| | deg F | 300 | 343 | 439 | 463 | 463 | 602 | 442 | 616 | 668 |
| Enthalpy, Btu/lb | | 156 | 186 | 246 | 261 | 261 | 350 | 251 | 359 | 389 |
| Temp Out | tag no. | | | | | | | | | |
| | °C mean - μ | 71.2 | 85.1 | 88.4 | 116.2 | 136.4 | 154.4 | 173.2 | 188.1 | 227.8 |
| | std dev - σ | | | | | | | | | |
| | deg F | 160 | 185 | 191 | 241 | 278 | 310 | 344 | 371 | 442 |
| Enthalpy, Btu/lb | | 75 | 92 | 96 | 126 | 148 | 171 | 191 | 208 | 251 |
| Specific heat, Btu/lb-F | | 0.583 | 0.597 | 0.605 | 0.605 | 0.605 | 0.614 | 0.612 | 0.614 | 0.612 |
| X = (T1+T2)/200, F | | 2.30 | 2.64 | 3.15 | 3.52 | 3.70 | 4.56 | 3.93 | 4.93 | 5.55 |
| film h, Btu/ft2-h-F | | 120 | 121 | 104 | 108 | 109 | 93 | 51 | 94 | 63 |
| Duty | MMBtu/h | 147.9 | 20.0 | 83.7 | 35.2 | 44.20 | 74.2 | 70.5 | 87.9 | 162.7 |

HEN simulation -- CDU (2/3)

| | | E-1 | E-2 | E-3 | E-4 | E-5 | E-6 | E-7 | E-8 |
|----------------------|--------------------|----------------------|----------------|----------------------|-----------------------|-----------------------|----------------------|--------------------------|------------------------------|
| Name / Service | | Crude vs Naphtha P/A | Crude vs Kero | Crude vs LDO Product | Crude vs No 1 LDO P/A | Crude vs No 2 LDO P/A | Crude vs HDO Product | Crude vs Cold Red. Crude | Crude vs HDO P/A |
| <u>Cold stream</u> | | | | | | | | | |
| Description | | Crude Oil Feed | Crude Oil Feed | Crude Oil Feed | Crude Oil Feed | DS Crude Oil Feed | DS Crude Oil Feed | DS Crude Oil Feed | DS Crude Oil from flash drum |
| Flow | tag no. | | | | | | | | |
| | mean - μ | 1569 | 1569 | 1569 | 1569 | 1569 | 1569 | 1569 | 1427 |
| | std dev - σ | | | | | | | | |
| | units | m3/h | m3/h | m3/h | m3/h | m3/h | m3/min | m3/min | m3/h |
| | conversion | 1.784 | 1.759 | 1.751 | 1.712 | 1.695 | 1.670 | 1.625 | 1.627 |
| | Klb/h meas | 2799 | 2799 | 2799 | 2799 | 2799 | 2799 | 2799 | 2322 |
| | Klb/h used | 2803 | 2803 | 2803 | 2803 | 2803 | 2803 | 2803 | 2663 |
| | phase | liquid | liquid | liquid | liquid | liquid | liquid | liquid | liquid |
| Specific gravity | | 0.816 | 0.816 | 0.816 | 0.816 | 0.816 | 0.816 | 0.816 | 0.833 |
| Liquid density, g/cc | | 0.809 | 0.798 | 0.794 | 0.777 | 0.769 | 0.758 | 0.738 | 0.738 |
| Temp In | tag no. | | | | | | | | |
| | °C mean - μ | 43.5 | 71.1 | 79.0 | 111.0 | 123.0 | 139.0 | 165.0 | 181.4 |
| | std dev - σ | | | | | | | | |
| | deg F | 110.3 | 160.0 | 174.2 | 231.8 | 253.4 | 282.2 | 329.0 | 358.5 |
| Enthalpy, Btu/lb | | 36.0 | 60.2 | 67.4 | 97.2 | 108.8 | 124.6 | 151.0 | 168.1 |
| Temp Out | tag no. | | | | | | | | |
| | °C mean - μ | 102.0 | 79.0 | 111.0 | 124.0 | 139.0 | 165.0 | 187.0 | 212.0 |
| | std dev - σ | | | | | | | | |
| | deg F | 215.6 | 174.2 | 231.8 | 255.2 | 282.2 | 329.0 | 368.6 | 413.6 |
| Enthalpy, Btu/lb | | 88.7 | 67.4 | 97.2 | 109.8 | 124.6 | 151.0 | 174.1 | 201.2 |
| Sp heat, Btu/lb-F | | 0.501 | 0.502 | 0.518 | 0.536 | 0.547 | 0.564 | 0.583 | 0.600 |
| X = (T1+T2)/200, F | | 1.63 | 1.67 | 2.03 | 2.44 | 2.68 | 3.06 | 3.49 | 3.86 |
| film h, Btu/ft2-h-F | | 68.6 | 69.6 | 77.5 | 84.9 | 88.5 | 92.9 | 96.0 | 97.2 |
| Duty | MMBtu/h | 147.7 | 20.0 | 83.7 | 35.2 | 44.2 | 74.0 | 64.7 | 88.0 |

HEN simulation – CDU (3/3)

| | E-1 | E-2 | E-3 | E-4 | E-5 | E-6 | E-7 | E-8 |
|------------------------------------|----------------------|---------------|----------------------|-----------------------|-----------------------|----------------------|--------------------------|------------------|
| Name / Service | Crude vs Naphtha P/A | Crude vs Kero | Crude vs LDO Product | Crude vs No 1 LDO P/A | Crude vs No 2 LDO P/A | Crude vs HDO Product | Crude vs Cold Red. Crude | Crude vs HDO P/A |
| <u>Exchanger</u> | | | | | | | | |
| Avg Duty, MMBtu/h | 147.8 | 20.0 | 83.7 | 35.2 | 44.2 | 74.1 | 67.6 | 87.9 |
| Error in Q, % | 0.1% | 0.1% | 0.0% | 0.1% | 0.0% | 0.2% | 8.5% | 0.1% |
| Hot end DT approach | 84.6 | 169.2 | 207.4 | 208.3 | 181.3 | 272.5 | 73.3 | 201.96 |
| Cold end DT approach | 49.86 | 25.2 | 16.92 | 9.36 | 24.12 | 27.72 | 14.76 | 12.06 |
| Avg temp approach | 67.2 | 97.2 | 112.1 | 108.8 | 102.7 | 150.1 | 44.0 | 107.01 |
| No. of HTU (approx) | 2.1 | 1.6 | 2.2 | 2.0 | 1.8 | 1.9 | 2.2 | 2.3 |
| LMTD, deg F | 65.7 | 75.6 | 76.0 | 64.1 | 77.9 | 107.1 | 36.5 | 67.4 |
| Correction factor, Ft | 1 | 0.8 | 0.8 | 1 | 1 | 0.8 | 1 | 0.8 |
| Corrected MTD, F | 65.7 | 60.5 | 60.8 | 64.1 | 77.9 | 85.7 | 36.5 | 53.9 |
| Actual U, Btu/ft ² -h-F | 68.9 | 36.5 | 71.4 | 31.7 | 32.8 | 108.0 | 38.2 | 86.5 |
| Design U | 43.6 | 44.1 | 44.5 | 47.5 | 48.9 | 46.3 | 33.2 | 47.8 |
| % Error in U | 46% | -19% | 48% | -41% | -40% | 87% | 9% | 60% |
| Design A (for new HX) | 51542 | 7501 | 30950 | 11569 | 11605 | 18854 | 55812 | 34125 |
| Type of HX | S&T | S&T | S&T | S&T | S&T | S&T | S&T | S&T |
| a | 13000 | 13000 | 13000 | 13000 | 13000 | 13000 | 13000 | 13000 |
| b | 465 | 465 | 465 | 465 | 465 | 465 | 465 | 465 |
| n | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 |
| Cap Cost, K\$ | 731 | 143 | 414 | 235 | 235 | 237 | 1006 | 438 |
| Installation factor | 2.3 | 2.3 | 2.3 | 2.3 | 2.3 | 2.3 | 2.3 | 2.3 |
| Installed new cost, K\$ | 1681 | 328 | 951 | 540 | 541 | 545 | 2315 | 1007 |
| Retrofit cost, K\$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Errors must be reconciled before optimization

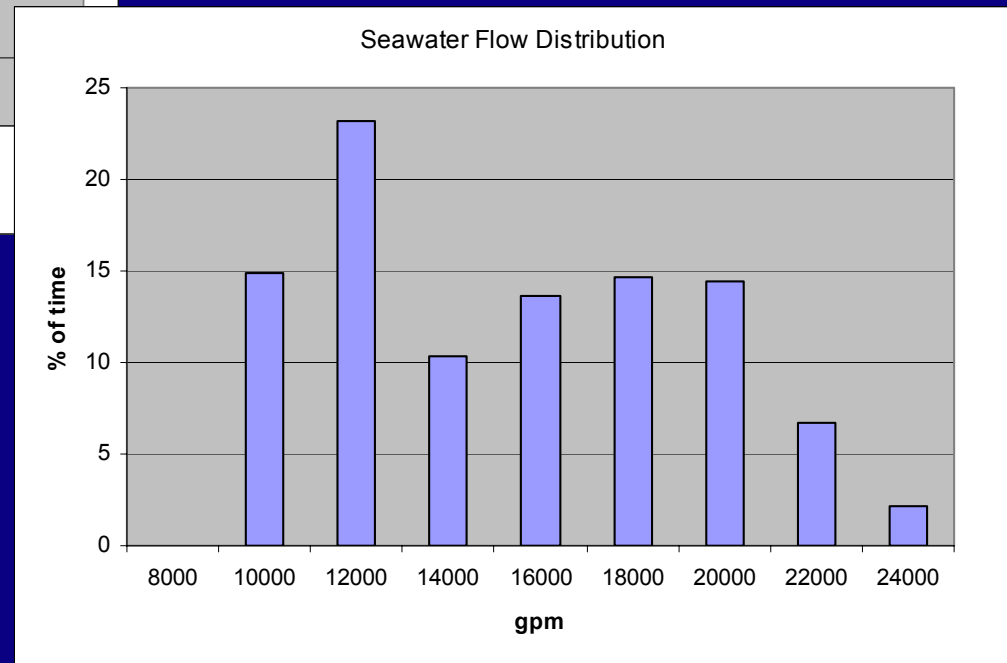
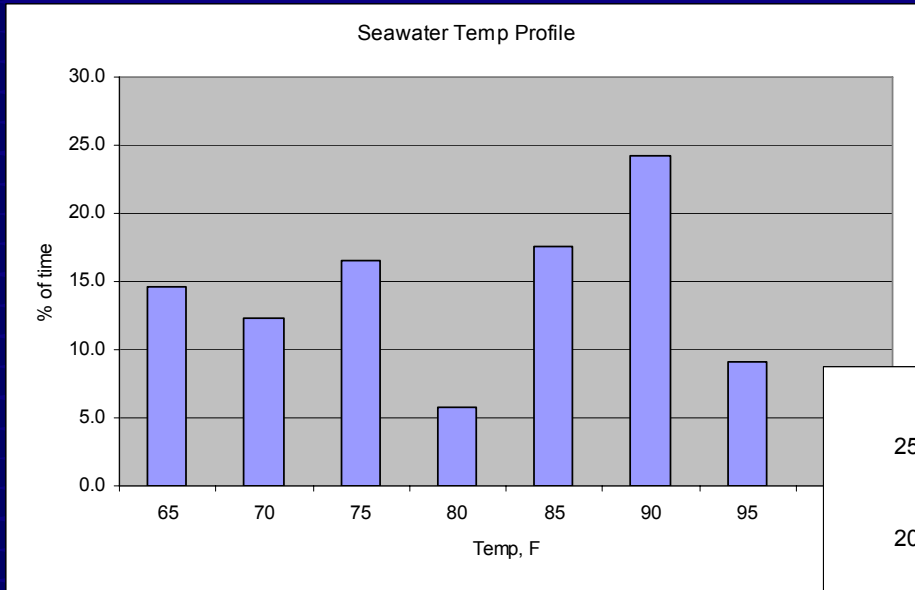
Estd Op Cost Savings – CDU

| Energy Savings | | | | | | |
|-------------------------------------|---------|---------|----------|------------|------|------------|
| | | MMBtu/h | \$/MMBtu | \$/hr | h/yr | K\$/yr |
| Fuel gas or oil | | 20.1 | 1.25 | 25.1 | 8400 | 211 |
| | psig | Klb/h | \$/Klb | \$/hr | h/yr | K\$/yr |
| HP steam | 625 | 0 | 2.72 | 0 | 8400 | 0 |
| MP steam | 150 | 37.2 | 2.48 | 92.2 | 8400 | 774 |
| LP steam | 50 | 0 | 2.46 | 0 | 8400 | 0 |
| Condensate | 15 | -37.9 | 0.90 | -34.1 | 8400 | -287 |
| | temp, F | MMBtu/h | \$/MMBtu | | | |
| Air cooling | 100 | -112.8 | 0.09 | -10.2 | 8400 | -85 |
| cooling water | 86 | 35.3 | 0.27 | 9.5 | 8400 | 80 |
| freon refig | 20 | 0 | 2.74 | 0 | 8400 | 0 |
| | | kw | \$/kwh | \$/hr | h/yr | K\$/yr |
| Elec power usage Δ | | | 0.0267 | 0 | 8400 | 0 |
| Elec power generation Δ | | 0 | 0.024 | 0 | 8400 | 0 |
| Operation and Maintenance Cost, etc | | | | 3 % of TIC | | 9 K\$/yr |
| Total savings (net) | | | | | | 685 K\$/yr |

37% of New Des

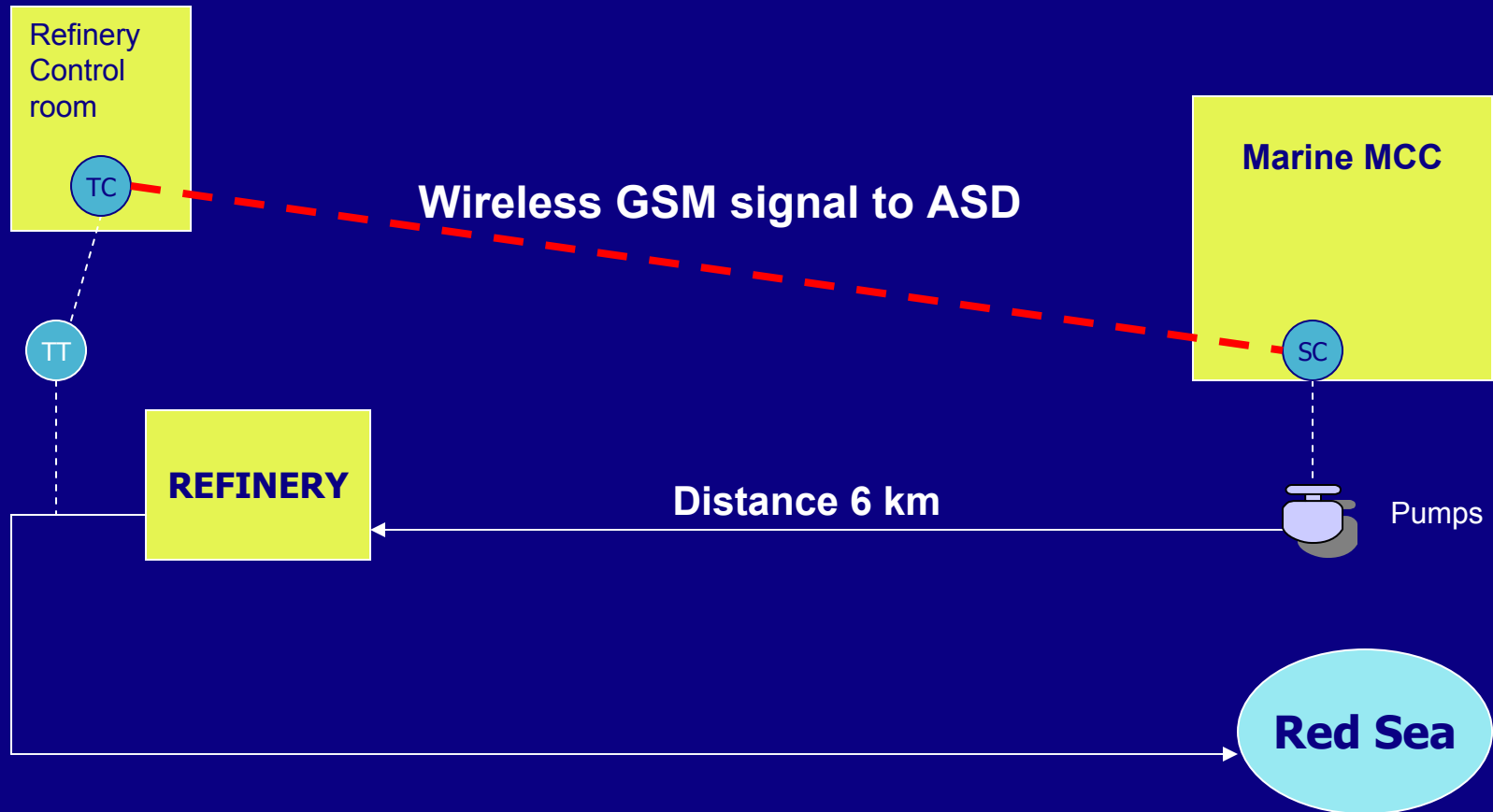
Est. Cap Cost = \$300 K, Simple Payback < 6 months

Power Conservation (ASD for Seawater Circulation Pumps)



ASDs are a good option when there is significant flow or ΔP variation

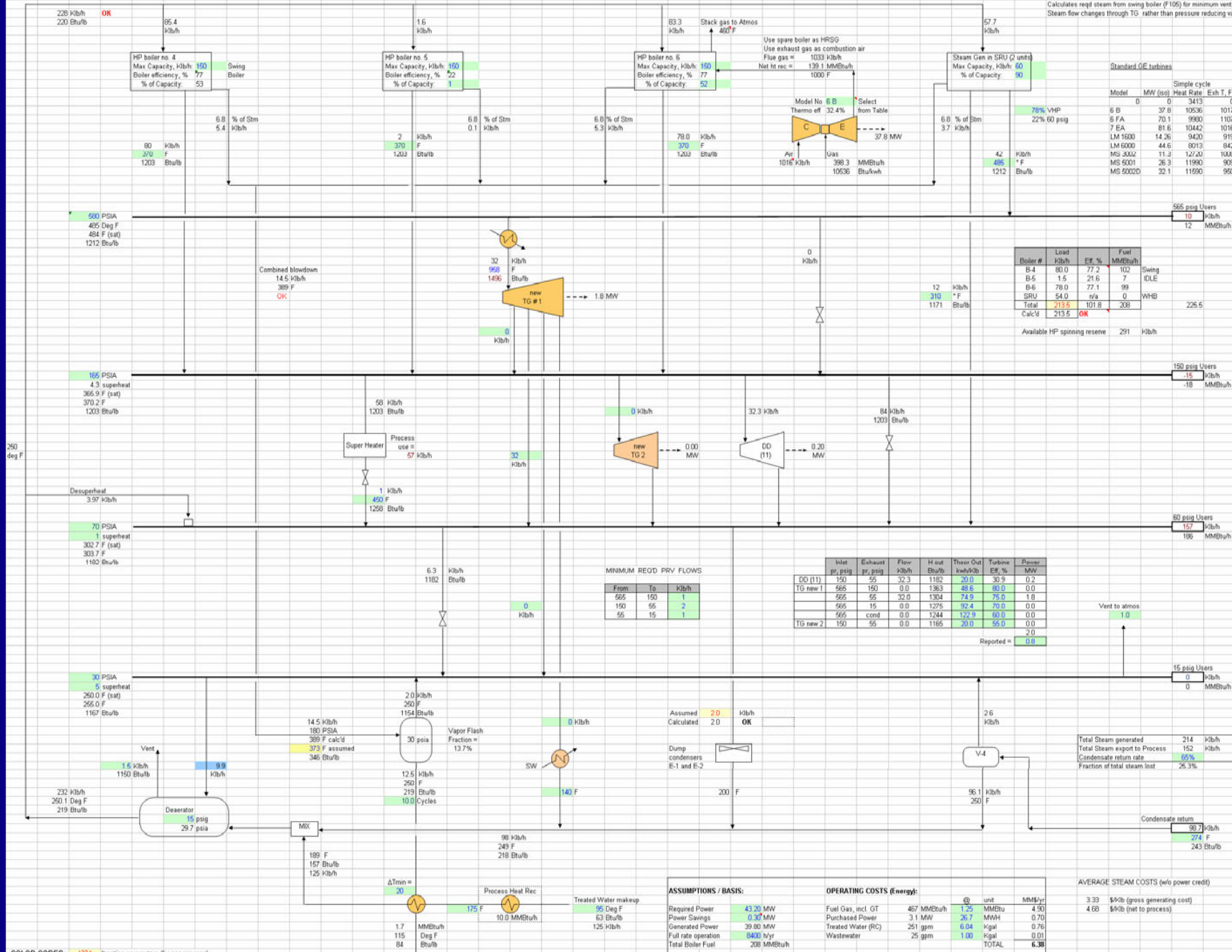
Proposed ASD Retrofit



Savings = \$90K/yr, Cap cost = \$200K

CHP System Optimization

Calculates reqd steam from swing boiler (F105) for minimum vent
Steam flow changes through TG rather than pressure reducing valve



COLOR CODES: 1234 Iteration parameters (for convergence)
1234 Input data to be provided
5678 linked call for other applications

Summary and Status Report

- 35 projects were identified & evaluated
- 6 were accepted by Plant Mgmt
- Savings potential = \$9.7 MM/yr (35%)
for Cap Cost of \$41 MM
- Implemented savings = \$0.5 MM/yr
- Rest delayed for political or legal reasons

Thank You