

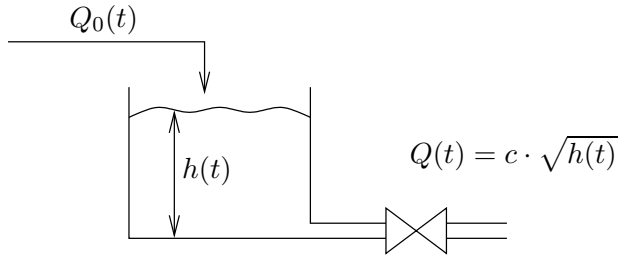
TKP4140 Process control — Midterm Exam

12. October 2017

Student number: SOLUTION

- Write your student number on **every** page in the indicated space.
- Write your student answers on the enclosed pages.
- Use the last two pages for details if you have too little space.
- Do not separate the enclosed pages.

1. (30 points) Consider a tank with one inflow and one outflow, as given in Figure 1. Assume constant density, $\rho = \text{const.}$



Parameters:

$$A = 10\text{m}^2$$

$$c = 10 \frac{\text{m}^3}{\text{min}\sqrt{\text{m}}}$$

$$Q_0^* = 10 \frac{\text{m}^3}{\text{min}} \text{ (nominal value)}$$

Figure 1: Tank system with volume $V = Ah$

- (a) (7 points) Formulate the dynamic mass balance and write it in the form $\frac{dh}{dt} = \dots$

The dynamic mass balance is:

$$\begin{aligned} \frac{dm}{dt} &= m_{in} - m_{out} \\ \frac{d(\rho V)}{dt} &= \rho(Q_0(t) - Q(t)) \\ \frac{d(\rho Ah)}{dt} &= \rho(Q_0(t) - Q(t)) \\ \rho \frac{dAh}{dt} &= \rho(Q_0(t) - Q(t)) \\ \frac{dAh}{dt} &= (Q_0(t) - Q(t)) \text{ after dividing by constant } \rho \\ \frac{dh}{dt} &= \frac{1}{A}(Q_0(t) - Q(t)) \\ \frac{dh}{dt} &= \frac{1}{A}(Q_0(t) - c\sqrt{h(t)}) \end{aligned}$$

- (b) (3 points) What are the steady state values of $h(t)$ and $Q(t)$?

At steady state we have

$$0 = \frac{1}{A}(Q_0(t) - c\sqrt{h(t)}).$$

So

$$Q_0^* = c\sqrt{h(t)},$$

and

$$h^* = \left(\frac{Q_0^*}{c}\right)^2 = 1\text{m}$$

and

$$Q^* = Q_0^* = 10 \frac{\text{m}^3}{\text{min}}$$

- (c) (6 points) Linearize the model and introduce deviation variables.

The model is

$$\frac{dh}{dt} = f(h, Q_0)$$

where

$$f(h, Q_0) = \frac{1}{A}(Q_0(t) - c\sqrt{h(t)})$$

We linearize around the stationary point. The deviation variables are:

$$\Delta h = h - h^* \quad \Delta Q_0 = Q - Q_0$$

The linearized model takes the form

$$\frac{d\Delta h}{dt} = \mathcal{A}\Delta h + \mathcal{B}\Delta Q_0.$$

The constants \mathcal{A} and \mathcal{B} are found as

$$\begin{aligned} \mathcal{A} &= \left. \frac{\partial f}{\partial h} \right|_* \\ &= \frac{-c}{2A\sqrt{h_0}} = -\frac{1}{2\text{min}} \end{aligned}$$

$$\begin{aligned} \mathcal{B} &= \left. \frac{\partial f}{\partial Q} \right|_* \\ &= \frac{1}{A} = \frac{1}{10\text{m}^2} \end{aligned}$$

Omitting the units, the linearized model is

$$\frac{d\Delta h}{dt} = -0.5\Delta h + 0.1\Delta Q_0.$$

- (d) (6 points) Take the Laplace transform and derive the transfer function
- $g(s)$
- :

$$h(s) = g(s)Q_0(s)$$

Taking the Laplace transform of the linearized model, we have

$$sh(s) = -0.5h(s) + 0.1Q_0(s).$$

Solving for $h(s)$

$$\begin{aligned} h(s) &= \frac{0.1}{s + 0.5}Q_0(s) \\ &= \frac{0.2}{2s + 1}Q_0(s), \end{aligned}$$

and comparing $h(s) = g(s)Q_0(s)$ with the above gives the transfer function $g(s)$ as

$$g(s) = \frac{0.2}{2s + 1}$$

This is a first order transfer function of form

$$g(s) = \frac{k}{\tau s + 1}$$

- (e) (2 points) What is the value of the steady state gain and the time constant in $g(s)$?

The gain is $k = 0.2$ and the time constant $\tau = 2$.

- (f) (4 points) Fill in the corresponding transfer functions in the block diagram from Figure 2.

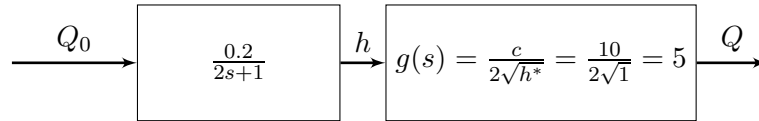


Figure 2: Block Diagram Tank System

- (g) (2 points) Does the block diagram from Figure 2 correspond to an open loop or a closed loop system?

Open loop system.

2. (10 points) Given the first-order transfer function

$$g(s) = \frac{2e^{-7s}}{5s + 1} \quad (1)$$

and $y(s) = g(s)u(s)$.

Consider a step change in the input:

$$u(t) = \begin{cases} 0 & \text{for } t < 3 \\ 5 & \text{for } t \geq 3 \end{cases} \quad (2)$$

Use the template in Fig.3 to sketch $u(t)$ and the resulting $y(t)$. Indicate the time constant, delay, and steady state value in your sketch.

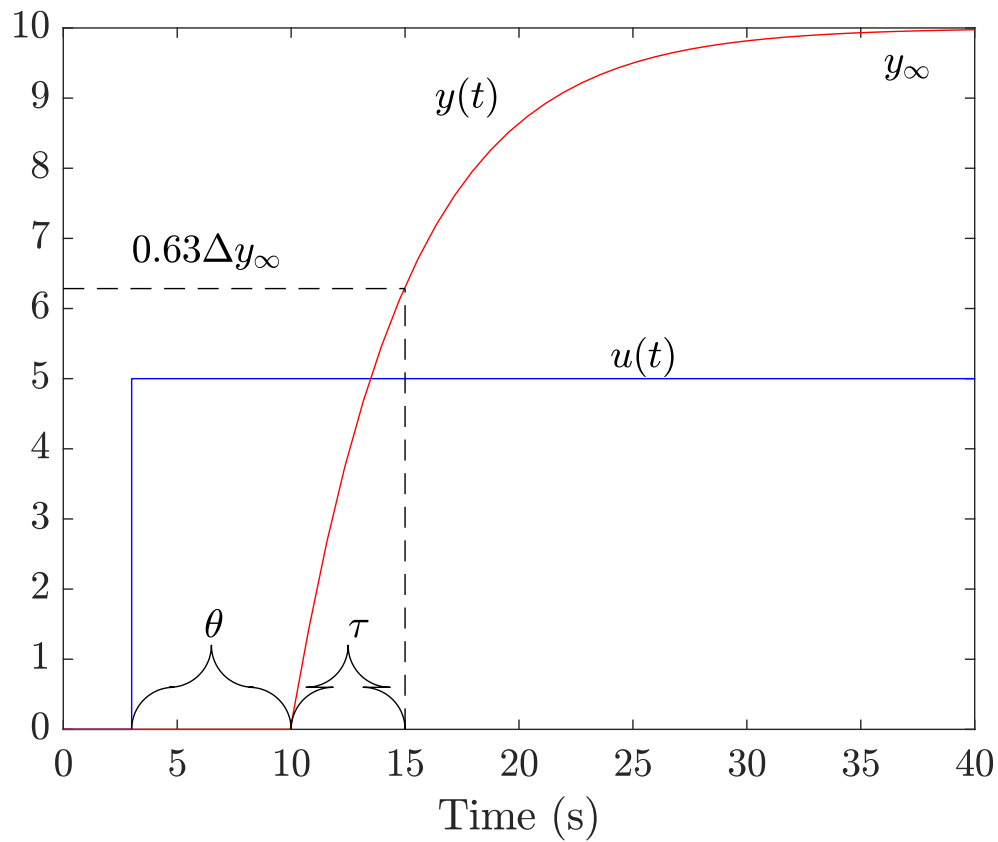


Figure 3: Step Response

3. (20 points) Consider the system in Figure 4.

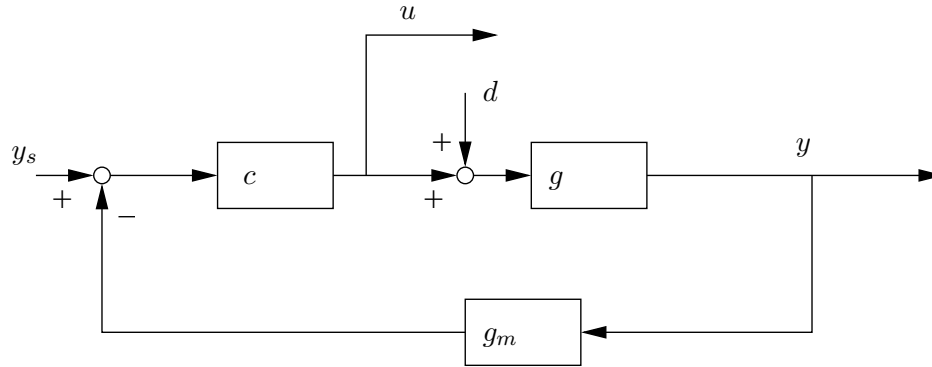


Figure 4: Block diagram

- (a) (4 points) Find the closed loop transfer function $T(s)$ from $y_s(s)$ to $y(s)$. Use symbols $(c(s), g(s), g_m(s))$.

$$T(s) = \frac{\text{"direct"}}{1 + \text{"closed loop"}}$$

$$= \frac{gc}{1 + g_m gc}$$

- (b) (4 points) Find the closed loop transfer function $Q(s)$ from $y_s(s)$ to $u(s)$. Use symbols $(c(s), g(s), g_m(s))$.

$$Q(s) = \frac{c}{1 + g_m gc}$$

- (c) (5 points) Find $T(s)$ when: $g(s) = \frac{3}{5s+1}$ $g_m(s) = \frac{-s+1}{s+1}$ $c(s) = 1$

$$T(s) = \frac{\frac{3}{5s+1} \cdot 1}{1 + \frac{-s+1}{s+1} \cdot \frac{3}{5s+1} \cdot 1} = \frac{3(s+1)}{5s^2 + 3s + 4} = \frac{3}{4} \frac{s+1}{\frac{5}{4}s^2 + \frac{3}{4}s + 1}$$

- (d) (3 points) What is the steady state gain when there is a unit step in y_s ?

The steady-state gain is $T(0) = \frac{3}{4} = 0.75$

- (e) (2 points) Calculate the damping factor and the time constant of $T(s)$.
Hint: the denominator in the second order transfer function is $\tau^2 s^2 + 2\tau\zeta s + 1$.

$$\zeta = \frac{3}{2 \cdot 4\tau} = 0.335 \qquad \tau = \sqrt{\frac{5}{4}} = 1.118$$

- (f) (2 points) Does the system oscillate?

Yes, the system oscillates because $|\zeta| < 1$. This happens because the controller gain is a bit too large.

4. (20 points) Given

$$g_1 = \frac{2.5}{(6s + 1)}$$

$$g_2 = \frac{2.5(s + 0.8)}{(6s + 1)^2}$$

$$g_3 = \frac{2.5}{(9s^2 + 3s + 1)}$$

$$g_4 = \frac{2(-4s + 1)}{(6s + 1)^2}$$

$$g_5 = \frac{2e^{-4s}}{(6s + 1)^2}$$

$$g_6 = \frac{2.5}{(6s + 1)^2}$$

Fill in the missing values in Table 1. In the case that the results in the table do not give a unique answer, comment on your choice.

Hints:

Initial slope of response to unit step input: $\lim_{t \rightarrow 0} y'(t) = \lim_{s \rightarrow \infty} sg(s)$

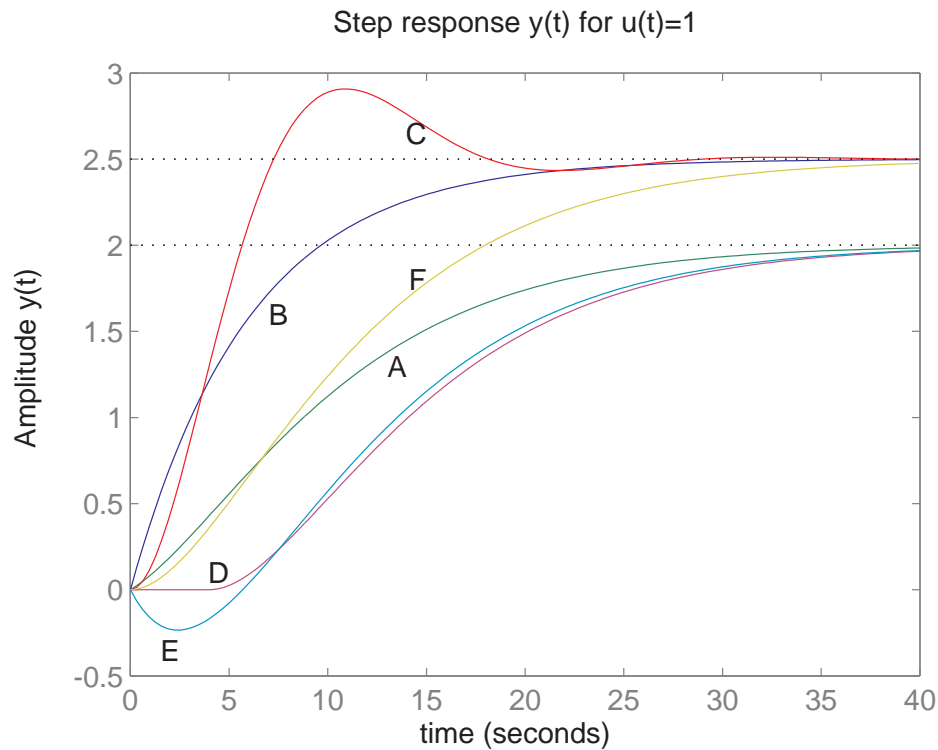


Figure 5: Step responses

Table 1: Problem 4; SS: steady state; TF: transfer function

TF	Poles	Zeros	SS gain	Initial gain	Initial slope	Conclusion
g_1	$s = -0.17$	-	2.5	0	0.41	B
g_2	$s_1 = -0.17$ $s_2 = -0.17$	-0.8	2	0	0.07	A
g_3	$-0.17 \pm 0.29i$	-	2.5	0	0	C
g_4	$s_1 = -0.17$ $s_2 = -0.17$	0.25	2	0	-0.22	E
g_5	$s_1 = -0.17$ $s_2 = -0.17$	-	2	0	0	D
g_6	$s_1 = -0.17$ $s_2 = -0.17$	-	2.5	0	0	F

5. (20 points) (a) SIMC tuning rules.

i. (3 points) Write the SIMC PI tuning rules for a first-order plus delay process.

$$g(s) = \frac{ke^{-\theta s}}{\tau s + 1}$$

$$K_c = \frac{1}{k} \frac{\tau_1}{\tau_c + \theta} \quad \tau_I = \min(\tau_1, 4(\tau_c + \theta))$$

ii. (3 points) Write the SIMC tuning rules for cascade PID for a second-order plus delay process.

$$g(s) = \frac{ke^{-\theta s}}{(\tau s + 1)(\tau_2 + 1)}$$

$$K_c = \frac{1}{k} \frac{\tau_1}{\tau_c + \theta} \quad \tau_I = \min(\tau_1, 4(\tau_c + \theta)) \quad \tau_D = \tau_2$$

(b) By modelling and linearization, you have derived the following process transfer function

$$g(s) = \frac{3(-1.5s + 1)e^{-0.5s}}{(25s + 1)(3s + 1)(0.8s + 1)} \quad (3)$$

i. (3 points) Write the first-order plus delay approximation $g_1(s)$ using the half rule.

$$\theta = 1.5 + 0.5 + \frac{3}{2} + 0.8 = 4.3$$

$$\tau = 25 + \frac{3}{2} = 26.5$$

$$k = 3$$

$$\begin{aligned} g_1(s) &= \frac{ke^{-\theta s}}{\tau s + 1} \\ &= \frac{3e^{-4.3s}}{26.5s + 1} \end{aligned}$$

ii. (3 points) Write the second-order plus delay approximation $g_2(s)$ using the half rule.

$$\theta = 1.5 + 0.5 + \frac{0.8}{2} = 2.4$$

$$\tau_1 = 25$$

$$\tau_2 = 3 + \frac{0.8}{2} = 3.4$$

$$k = 3$$

$$\begin{aligned} g_2(s) &= \frac{ke^{-\theta s}}{(\tau_1 s + 1)(\tau_2 s + 1)} \\ &= \frac{3e^{-2.4s}}{(25s + 1)(3.4s + 1)} \end{aligned}$$

- iii. (3 points) Based on the approximations of $g_1(s)$ and $g_2(s)$ give the SIMC PI and PID settings. Use the standard choice $\tau_c = \theta$, where θ is the effective delay.

PI settings:

$$K_c = \frac{1}{3} \cdot \frac{26.5}{2 \cdot 4.3} = 1.03$$

$$\tau_i = \min(26.5, 4 \cdot 2 \cdot 4.3) = 26.5$$

PID settings:

$$K_c = \frac{1}{3} \cdot \frac{26.5}{2 \cdot 4.3} = 1.74$$

$$\tau_i = \min(25, 4 \cdot 2 \cdot 2.4) = 19.2$$

$$\tau_2 = 3.4$$

- iv. (3 points) Would you recommend a PI or a PID controller? Explain briefly.

PID-controller is recommended for g_2 because $\tau_2 > \theta$. Figure 6 shows the closed loop responses for both PI and PID controllers, when a unit step is given in the input u at $t = 10$ s (u acts as a disturbance in this case). It can be observed that the input usage is higher for the PID controller. However, the change in the output is smaller for the PI controller.

- (c) (3 points) What would the SIMC PI tunings be for the system in Problem 3 (given Figure 4 with the transfer function from 3(c))?

In practice, every measurement has a time delay. Therefore, to design the controller, one has to consider the transfer function from the input (u) to the measured output (y_m), which is:

$$gg_m = \frac{3}{5s + 1} \cdot \frac{-s + 1}{s + 1}$$

Applying the half rule gives:

$$gg_m \approx \frac{3e^{-1.5s}}{5.5s + 1}$$

Applying the SIMC PI rules, and assuming $\tau_c = \theta$:

$$K_c = \frac{1}{3} \cdot \frac{5.5}{2 \cdot 1.5} = 0.61$$

$$\tau_i = \min(5.5, 4 \cdot 2 \cdot 1.5) = 5.5$$

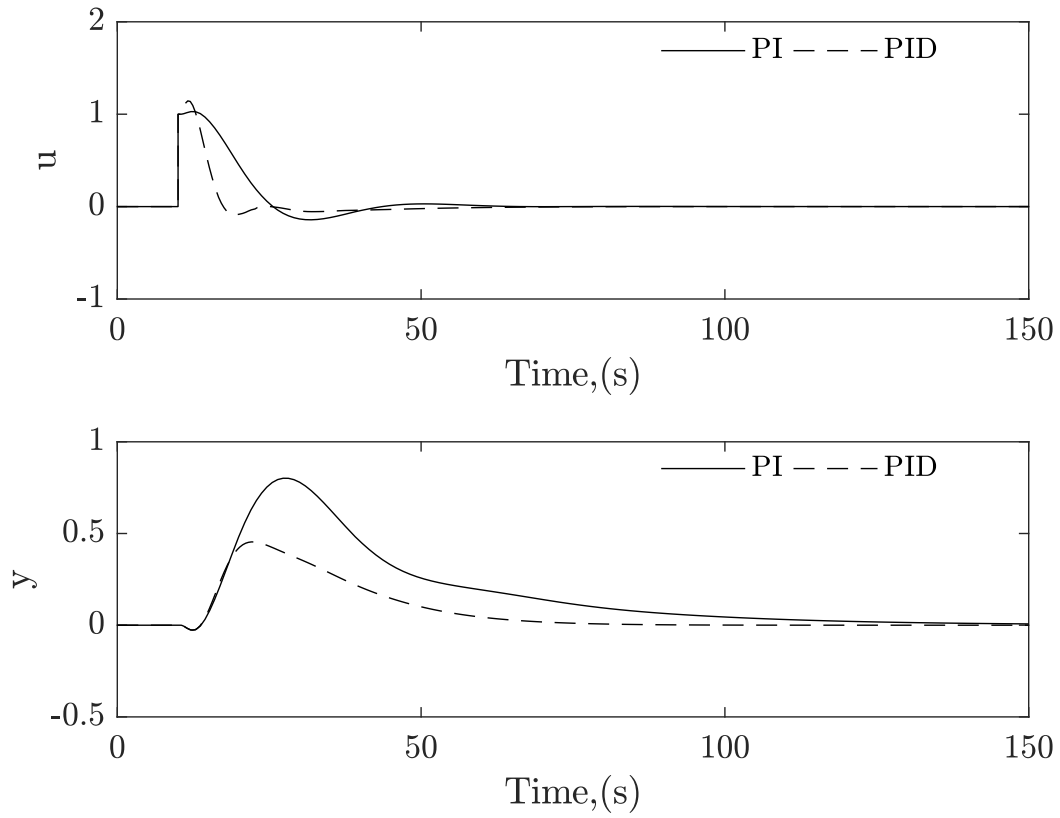


Figure 6: Closed loop response for PI and PID controllers for a unit step in u at $t = 10$ s