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Ice Protection Workshop 2

Guy Fortin
Advanced Aerodynamics

2023-06-23

BOMBARDIER

CRM-65 MidSpan

DRAGON ICE SUITE

Flow: Reynolds Averaged Navier Stokes Solver (RANS)
k-w Turbulence Model

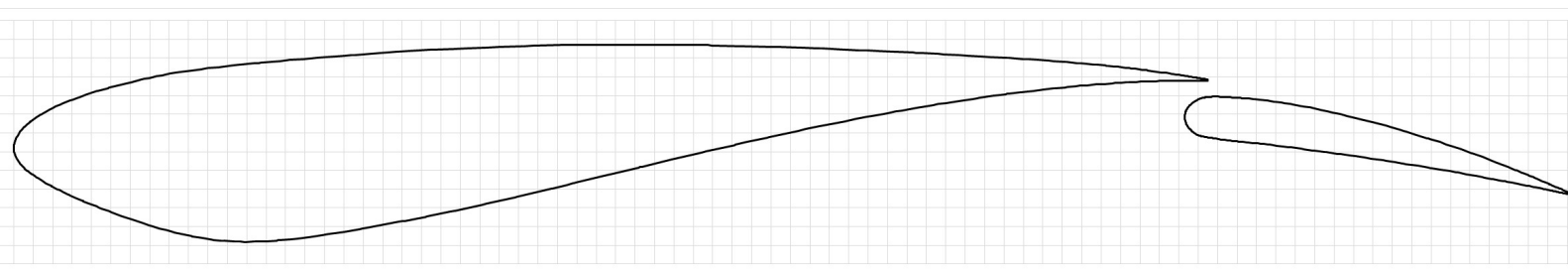
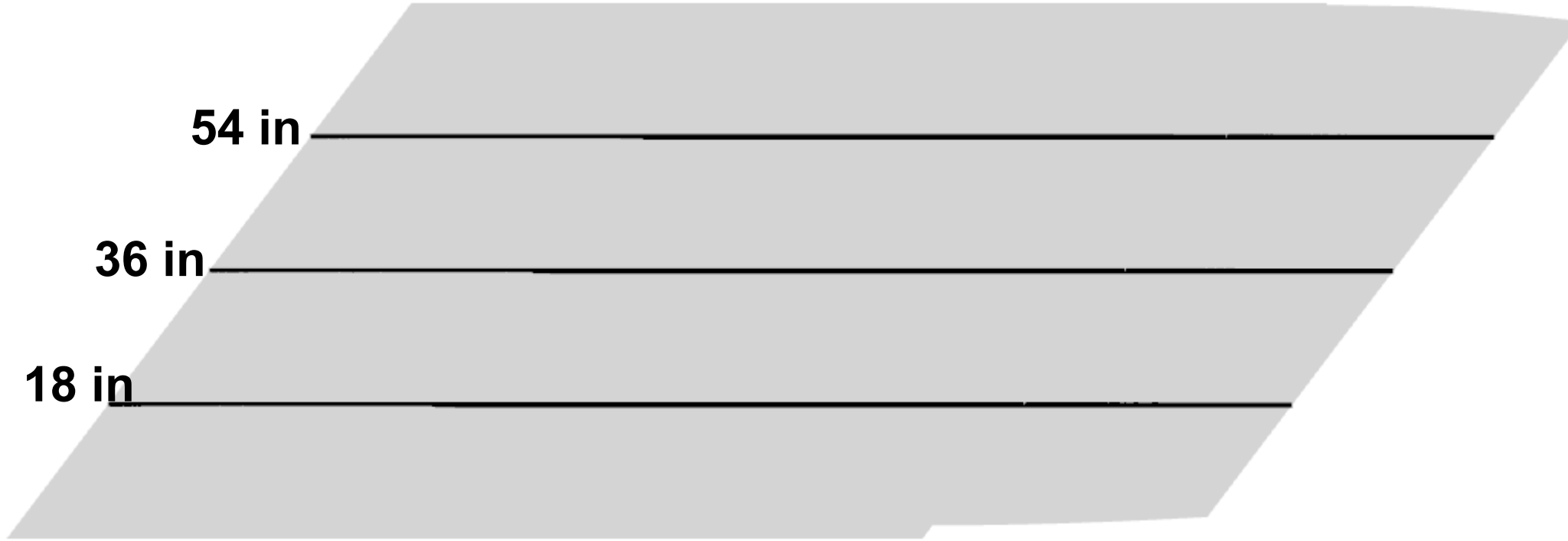
Heat Transfer Coefficient by Convection: Newton's law of cooling and Fourier's law
Semi-Empiric Equivalent Sand Grain Roughness Correlation for 1 layer ice shape prediction

Drop (Collection Efficiency): Eulerian Solver

Thermo (Mass and Heat Transfers): Iterative Messinger Solver
Multi-stagnation point
Runback is based on wall shears stress

Geometry: Lagrangian Node Displacement Method

CRM-65 InBoard

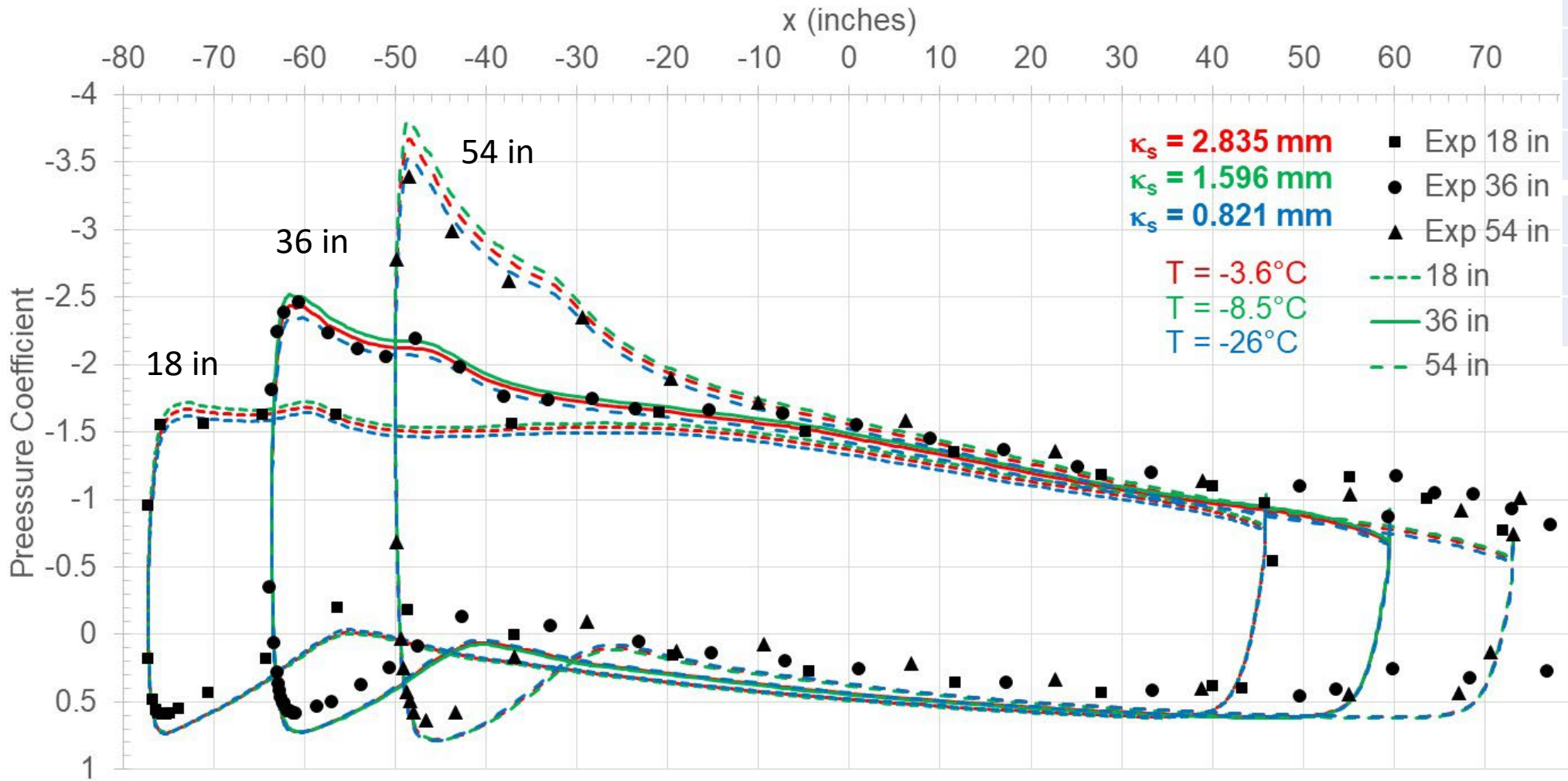


AoA	3.7	deg
TAS	66.9	m/s
MVD	25	μm
LWC	1	g/m^3
time	29	min
SAT	-3.6	$^{\circ}\text{C}$
SAT	-8.5	$^{\circ}\text{C}$
SAT	-26	$^{\circ}\text{C}$

NASA IRT	Droplet
Volume	Diameter
0.05	7.3
0.1	9.9
0.2	13.7
0.3	24.9
0.2	44.9
0.1	74.9
0.05	127.6

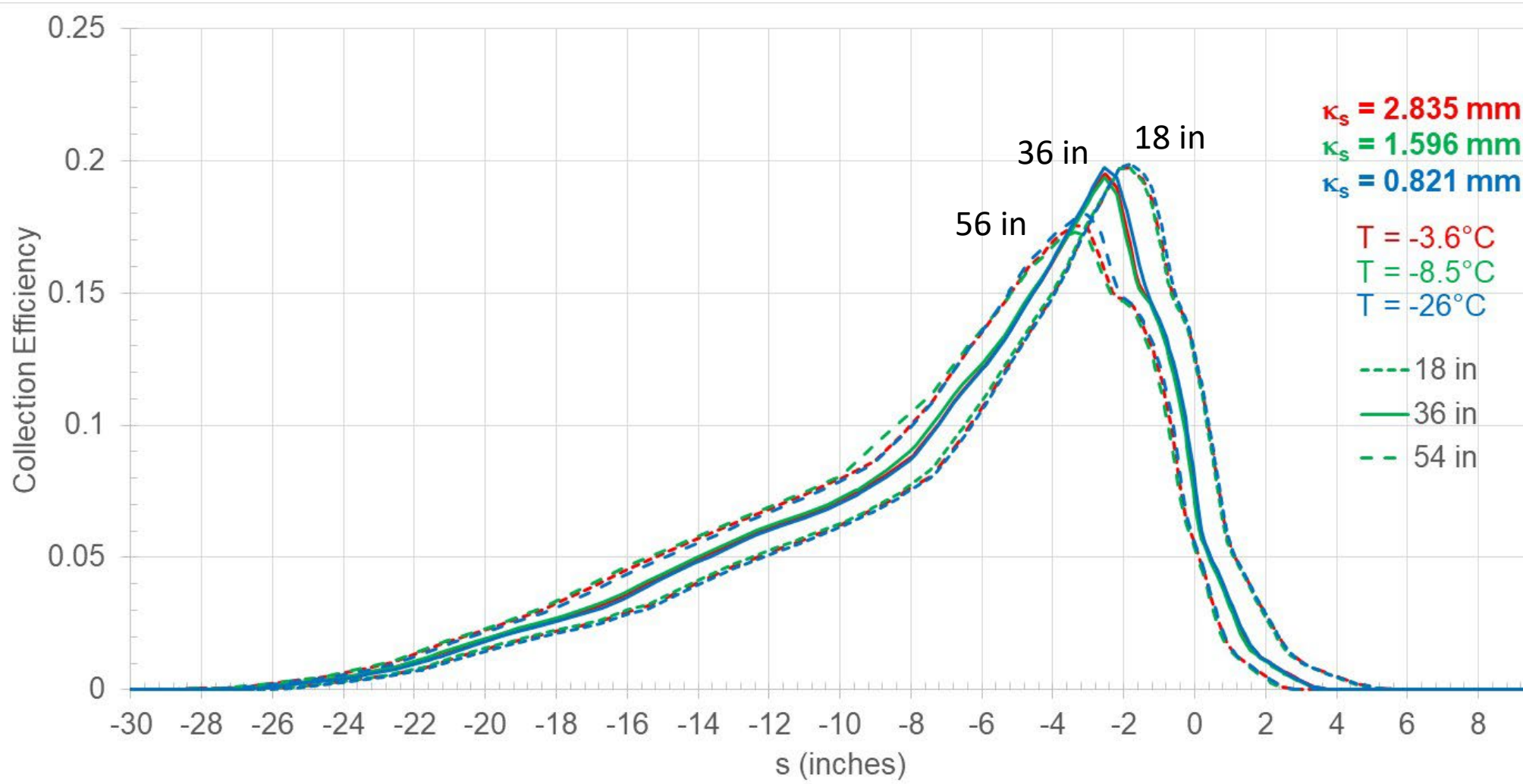
CRM-65 InBoard

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BOMBARDIER

CRM-65 InBoard

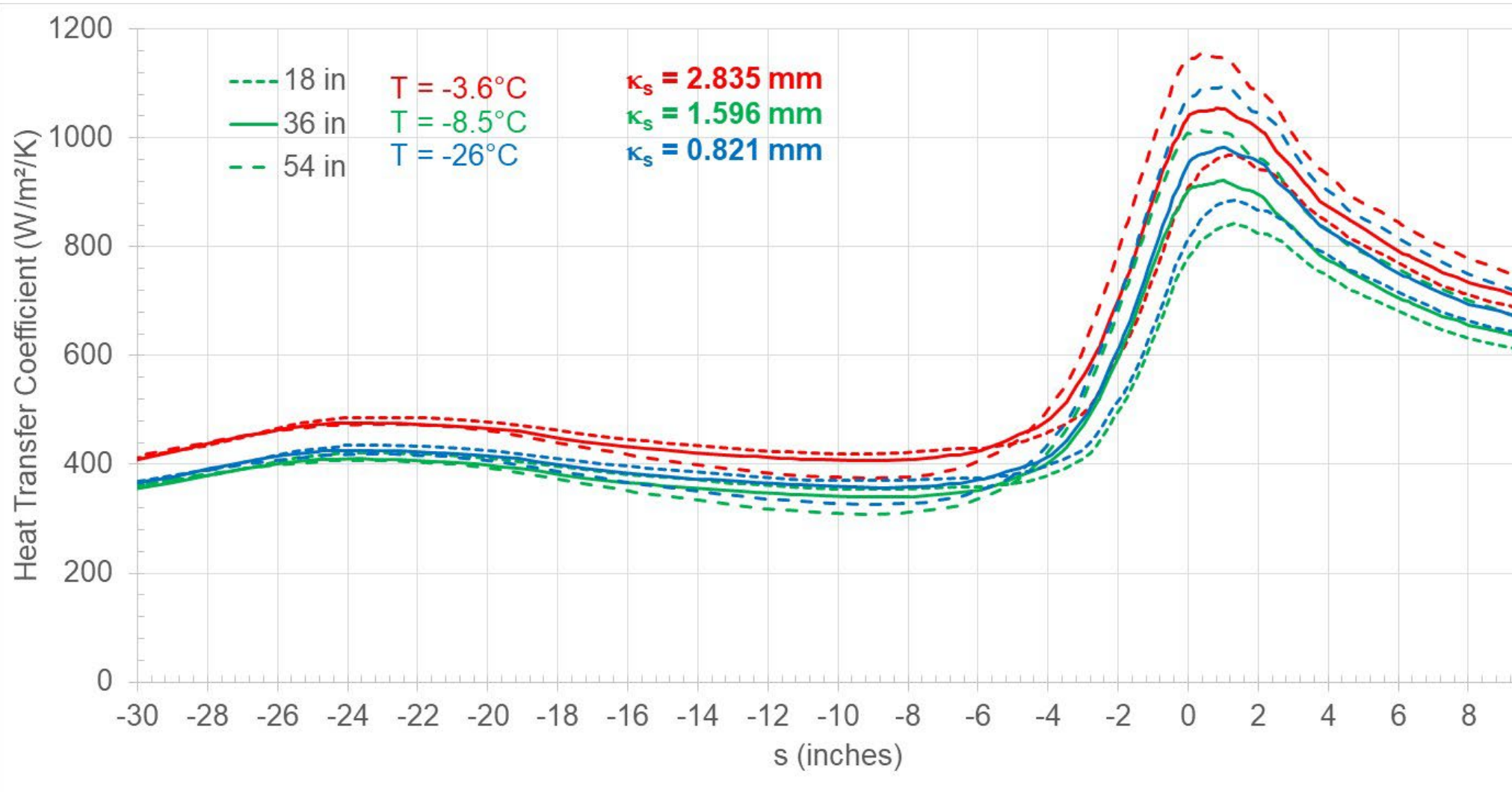


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CRM-65 InBoard

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0.1	74.9	
0.05	127.6	



CRM-65 InBoard

—18 —36 —54 —Clean

• TH2404 • TH2411

SAT = -3.6°C
 $\kappa_s = 2.835 \text{ mm}$
 $\rho_{\text{ice}} = 917 \text{ kg/m}^3$

---18 (917) ---36 (917) ---54 (917)

• TH2404 • TH2411

SAT = -8.5°C
 $\kappa_s = 1.596 \text{ mm}$
 $\rho_{\text{ice}} = 917 \text{ kg/m}^3$

SAT = -26°C
 $\kappa_s = 0.821 \text{ mm}$
 $\rho_{\text{ice}} = 917 \text{ kg/m}^3$

• TH2412 • TH2415

Experimental
Ice
Shape

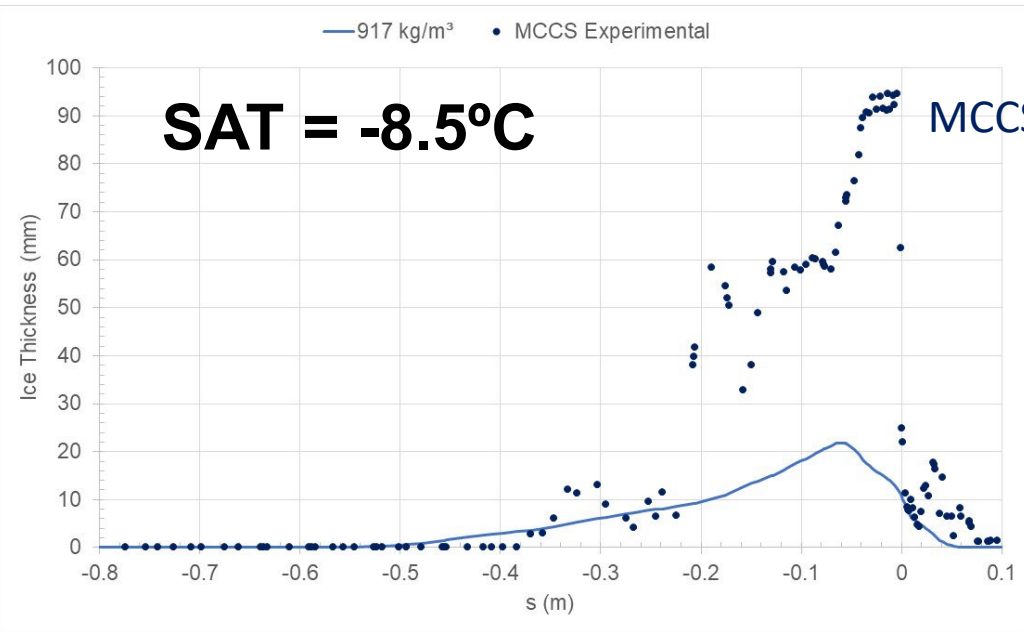
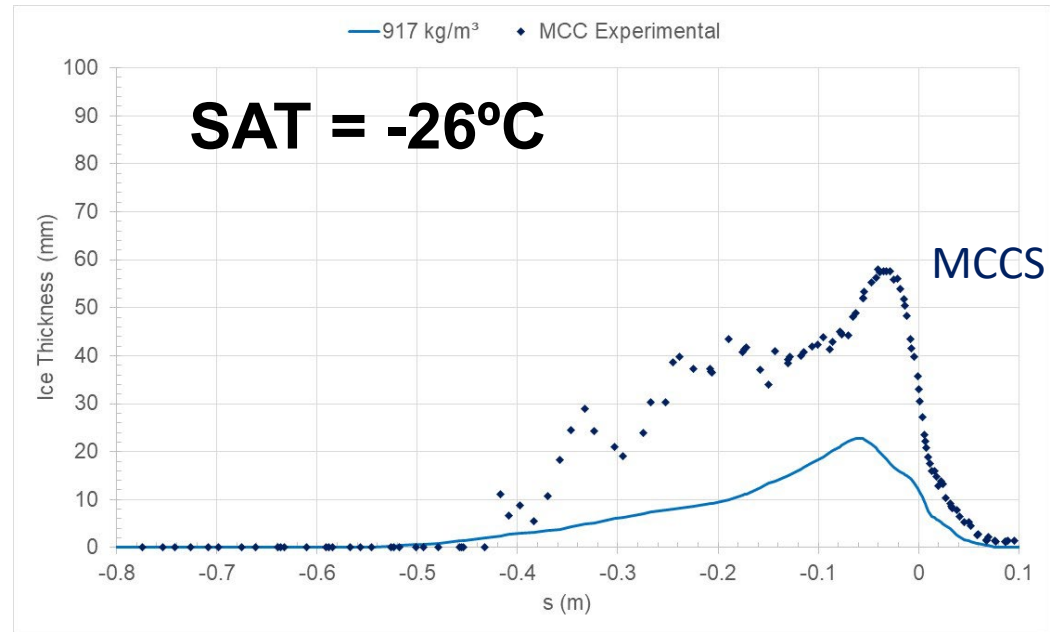
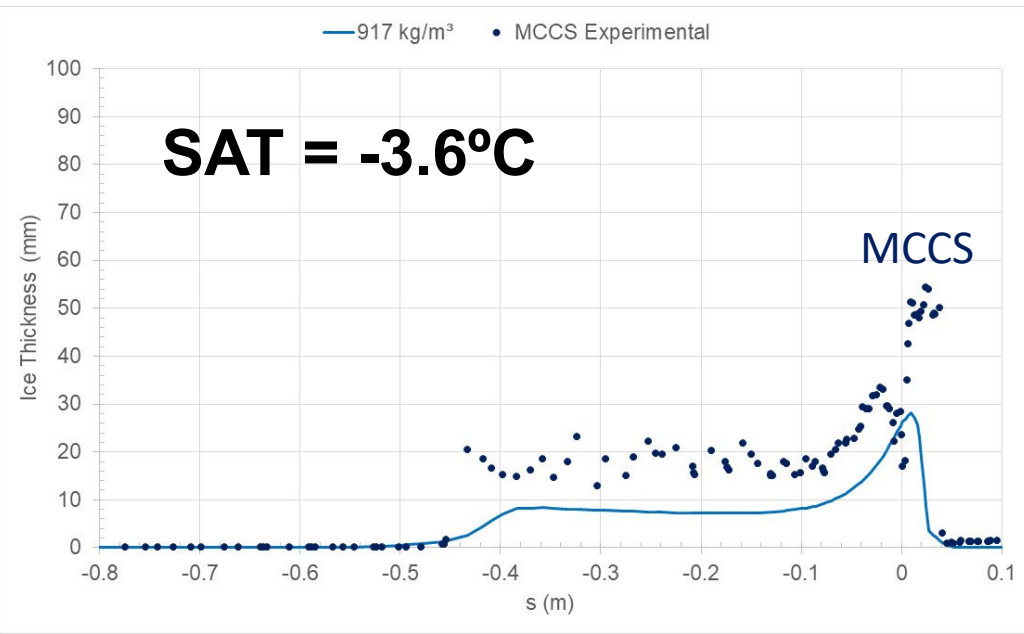
=

Maximum
Combined
Cross
Section

CRM-65 InBoard

SAT (°)	Surface (m ²) Exp	Ice Mass (kg/m) Exp	Ice Density kg/m ³
-3.6	0.013851	4.920	355
-8.5	0.019920	8.220	413
-26.0	0.019404	7.900	407

Hingewise cut



BOMBARDIER

CRM-65 InBoard

—18 —36 —54 —Clean

• TH2404 • TH2411

SAT = -3.6°C
 $\kappa_s = 2.835$ mm
 $\rho_{ice} = 355$ kg/m³

---18 (917) ---36 (917) ---54 (917)

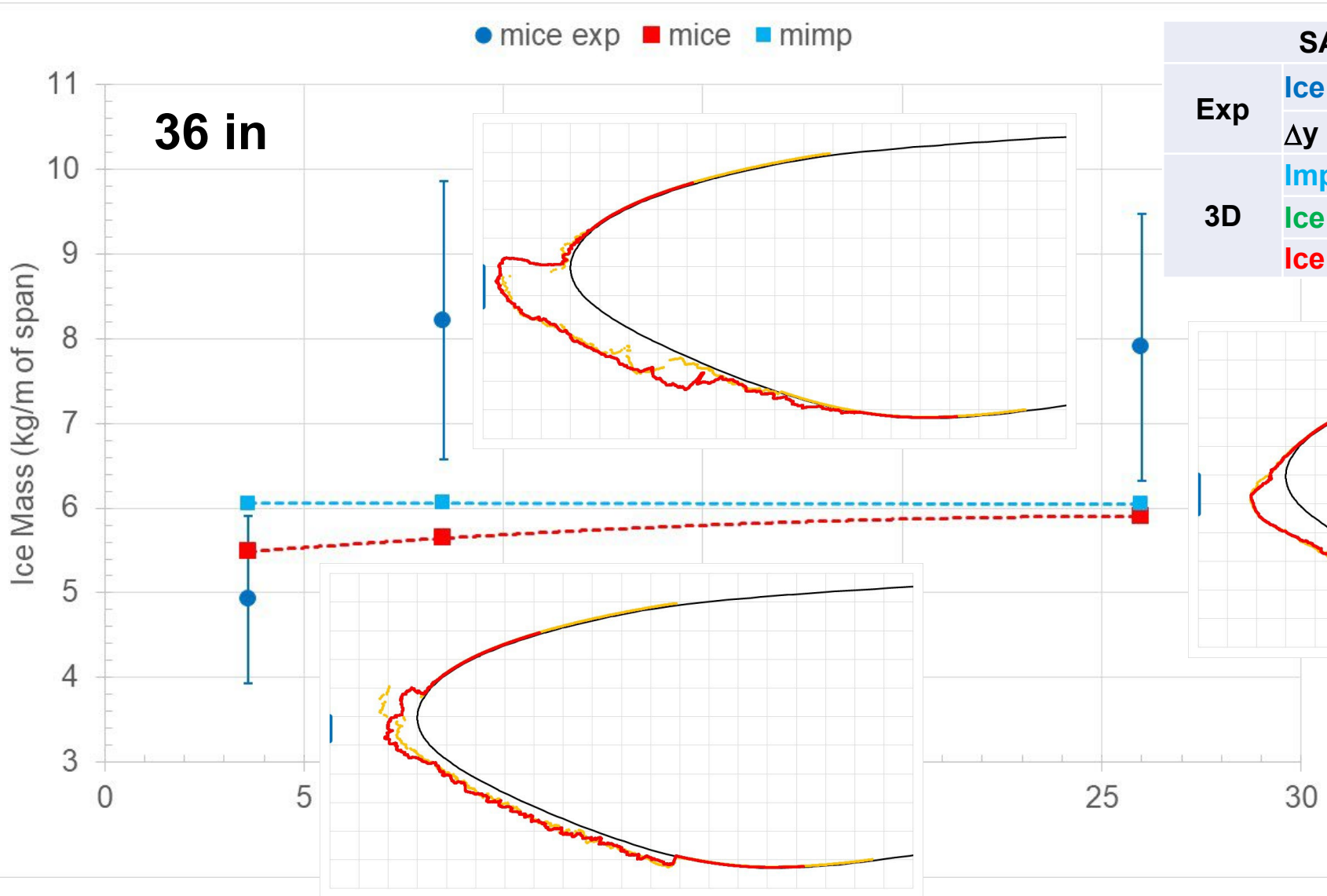
• TH2404 • TH2411

SAT = -8.5°C
 $\kappa_s = 1.596$ mm
 $\rho_{ice} = 413$ kg/m³

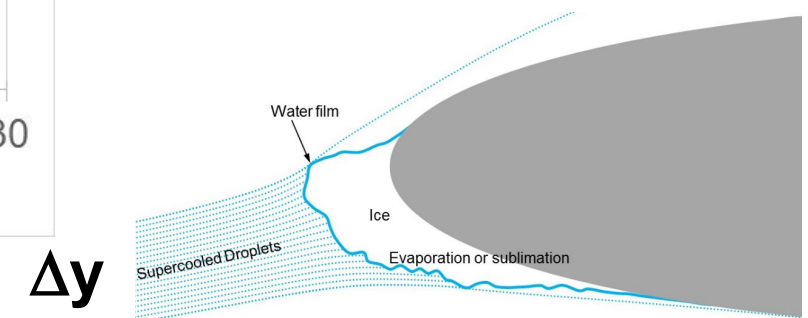
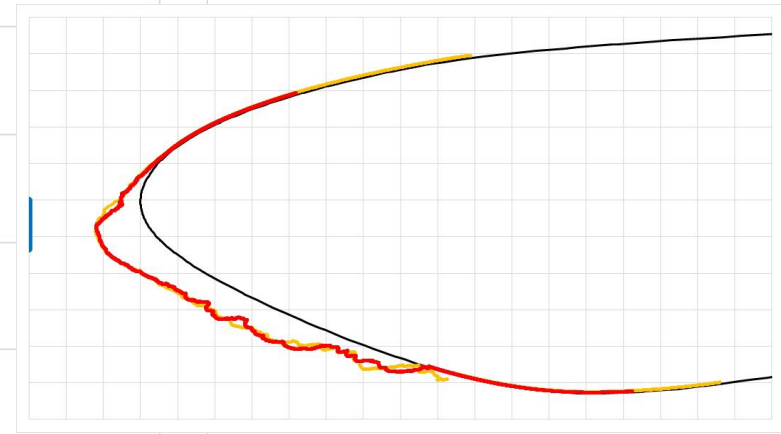
SAT = -26°C
 $\kappa_s = 0.821$ mm
 $\rho_{ice} = 407$ kg/m³

• TH2412 • TH2415

CRM-65 InBoard



SAT		-3.6	-8.5	-26	°C
Exp	Ice Mass	4.920	8.220	7.900	kg/m
	Δy	1.664	2.780	2.672	inches
3D	Impingement	6.050	6.067	6.044	kg/m
	Ice Thermo	5.485	5.645	5.905	kg/m
	Ice Thickness	5.229	5.492	5.687	kg/m

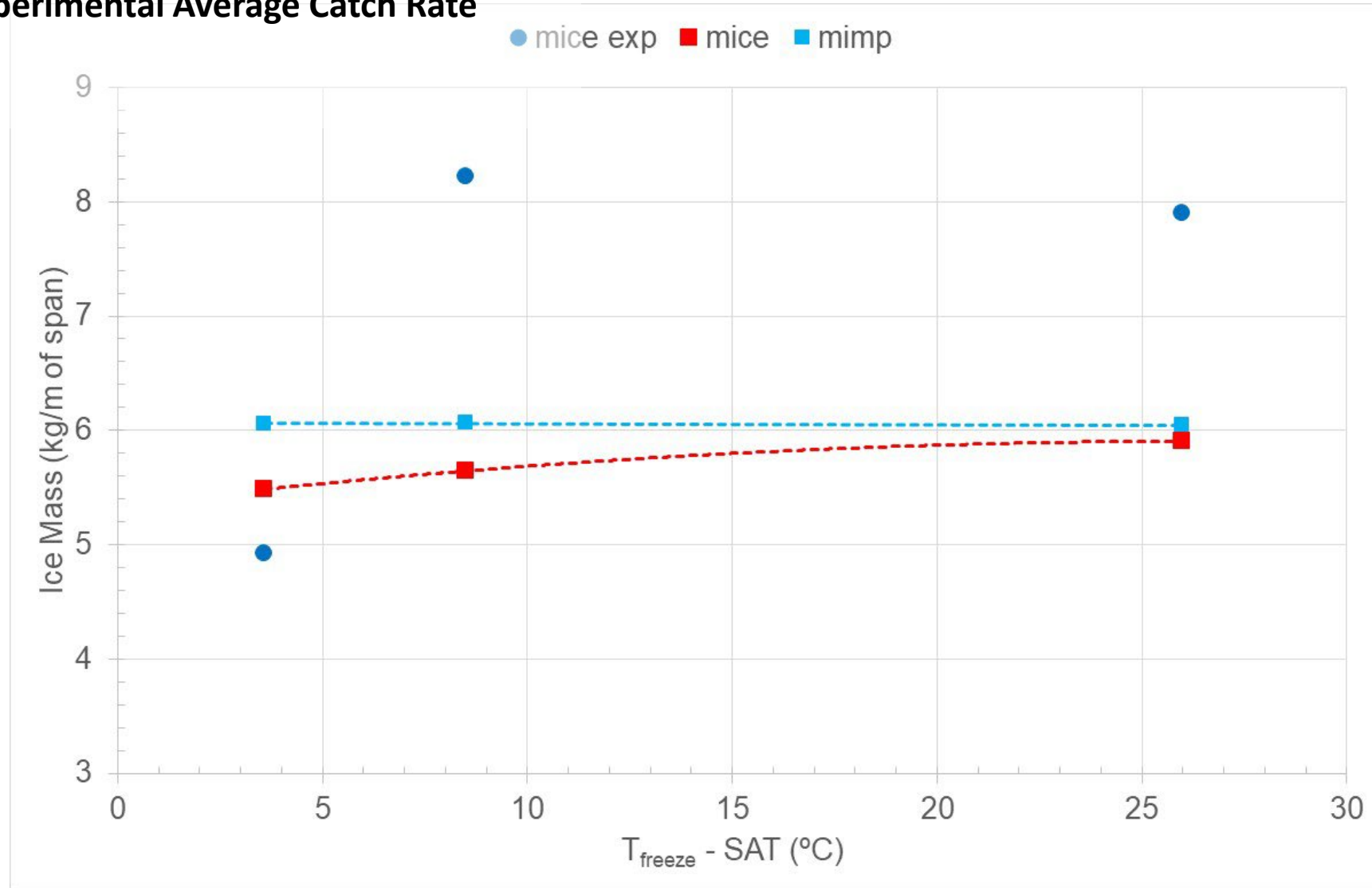


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CRM-65 MidSpan

Observation: Ice Mass

Numerical Clean Catch Rate versus Experimental Average Catch Rate



BOMBARDIER

CRM-65 MidSpan

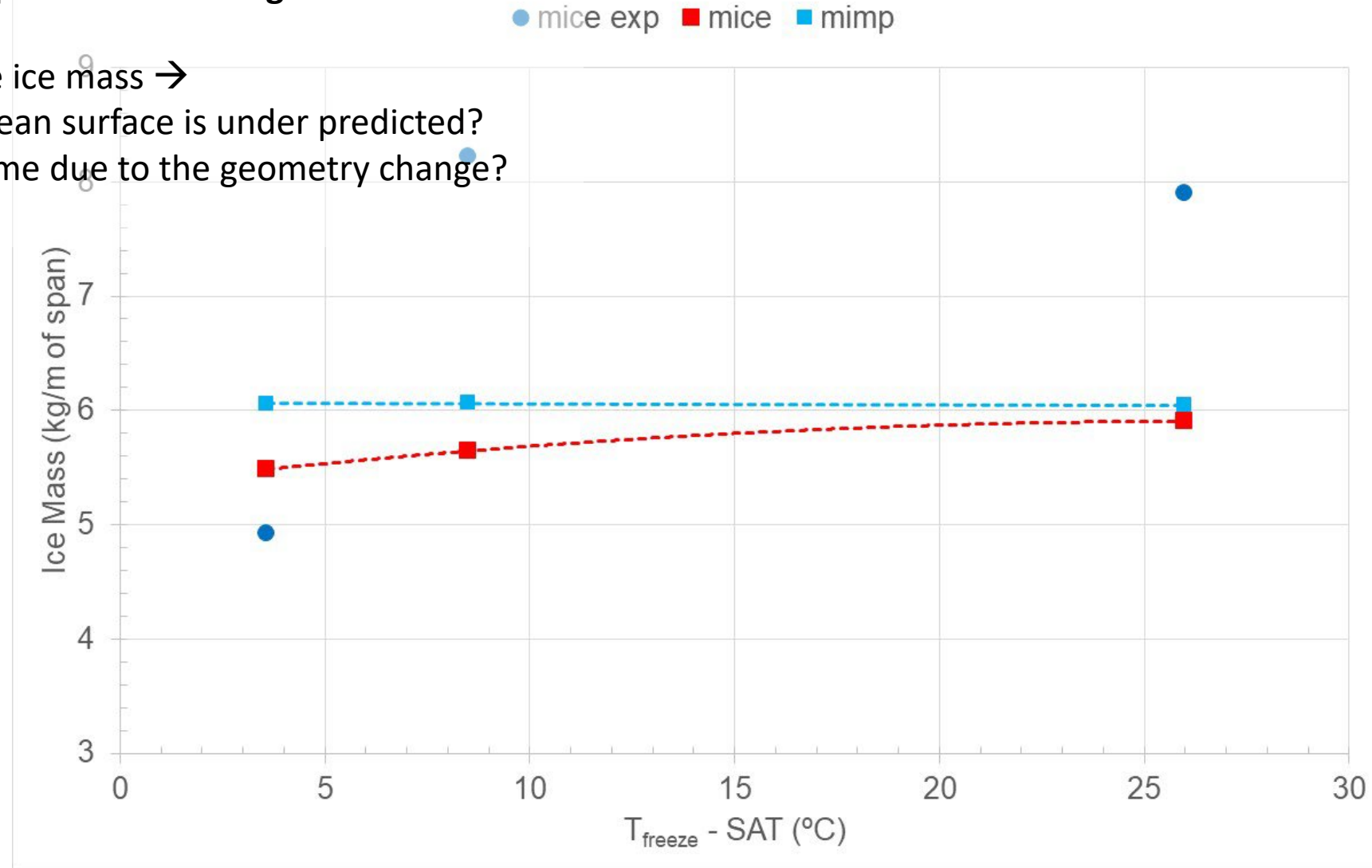
Observation: Ice Mass

Numerical Clean Catch Rate versus Experimental Average Catch Rate

Cold Case (-26°C): Under predicted the ice mass →

Do the numerical catch rate for clean surface is under predicted?

Do the catch rate increase with time due to the geometry change?



CRM-65 MidSpan

Observation: Ice Mass

Numerical Clean Catch Rate versus Experimental Average Catch Rate

Cold Case (-26°C): Under predicted the ice mass →

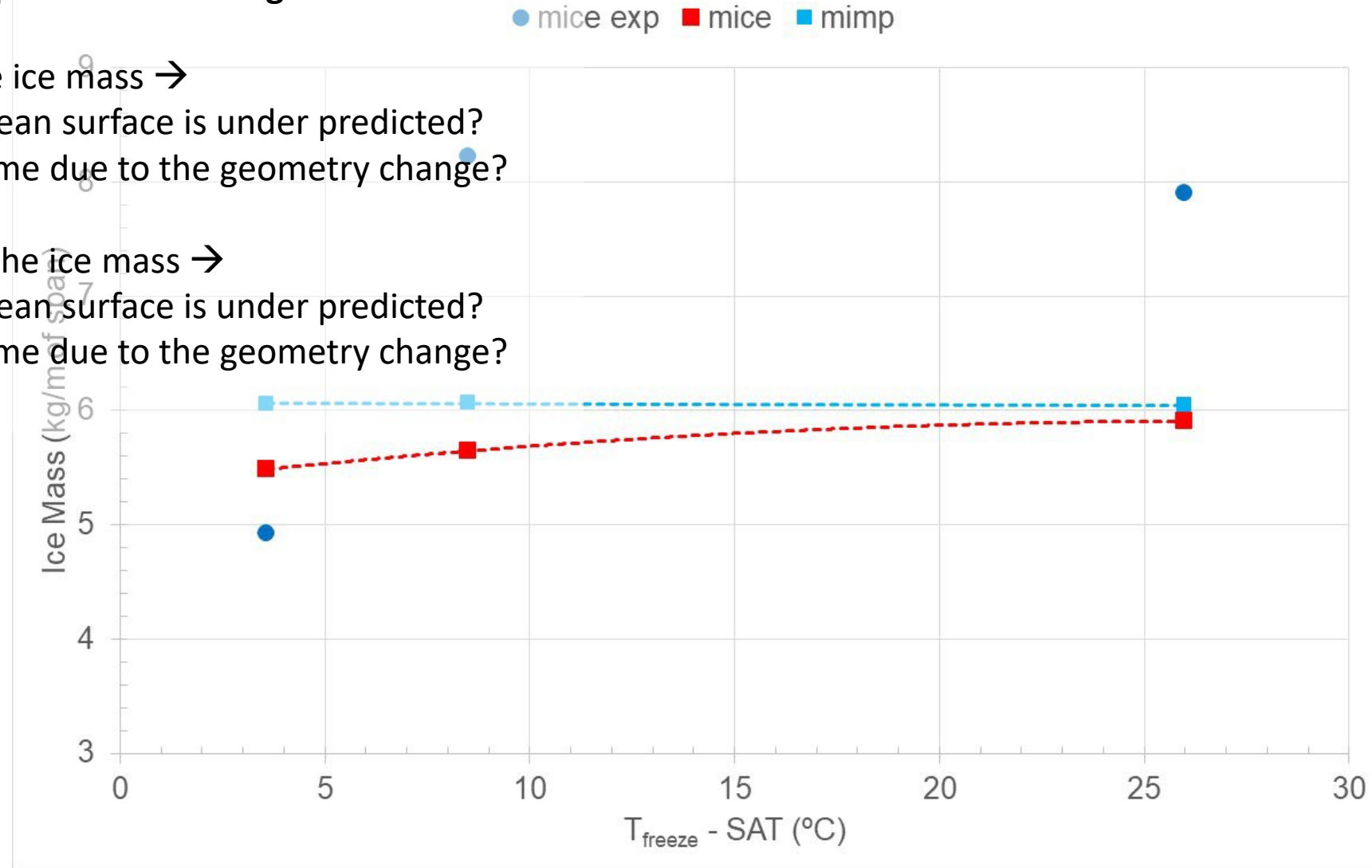
Do the numerical catch rate for clean surface is under predicted?

Do the catch rate increase with time due to the geometry change?

Mixed Case (-8.5°C): Under predicted the ice mass →

Do the numerical catch rate for clean surface is under predicted?

Do the catch rate increase with time due to the geometry change?



CRM-65 MidSpan

Observation: Ice Mass

Numerical Clean Catch Rate versus Experimental Average Catch Rate

● mice exp ■ mice ■ mimp

Cold Case (-26°C): Under predicted the ice mass →

Do the numerical catch rate for clean surface is under predicted?

Do the catch rate increase with time due to the geometry change?

Mixed Case (-8.5°C): Under predicted the ice mass →

Do the numerical catch rate for clean surface is under predicted?

Do the catch rate increase with time due to the geometry change?

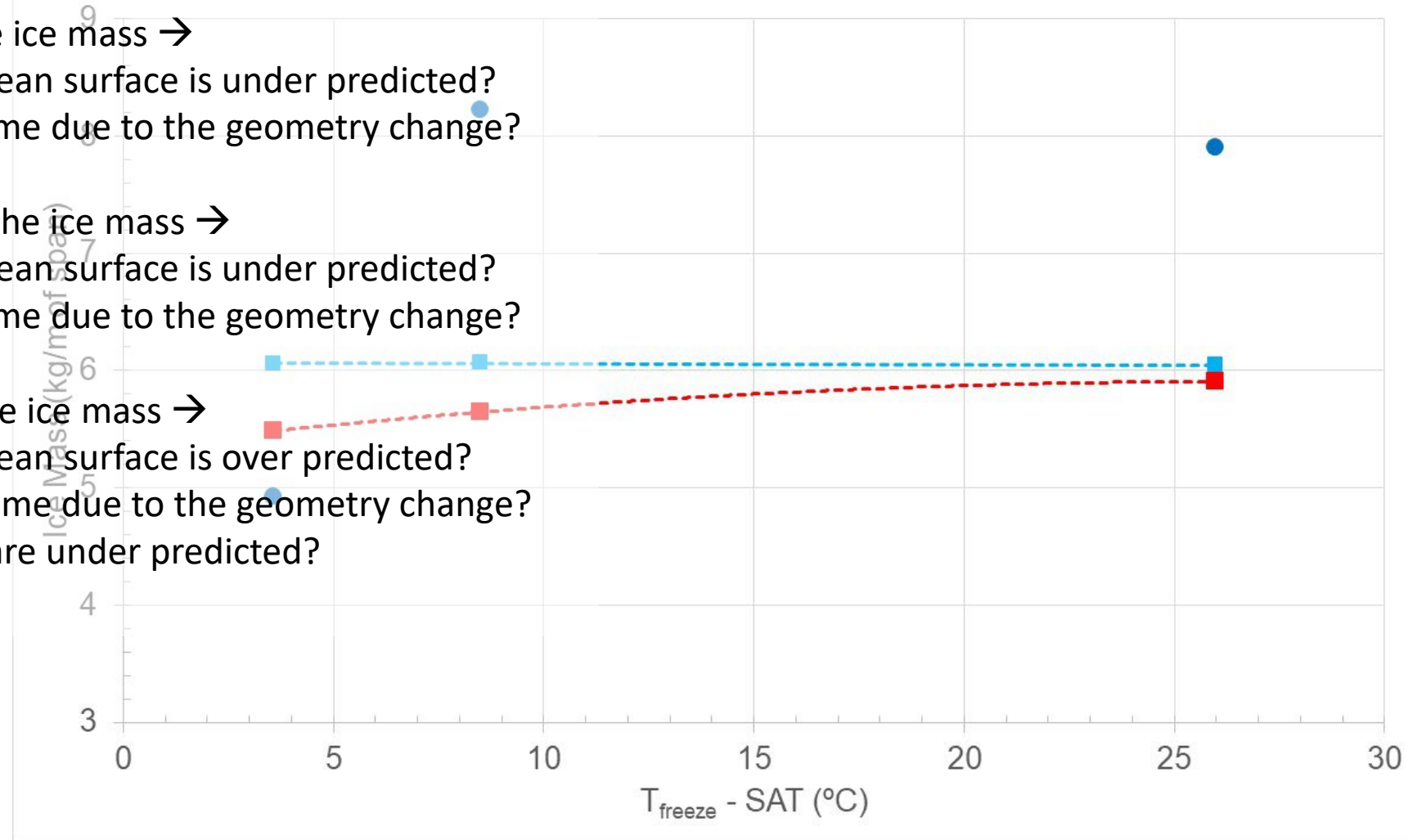
Mixed Case (-3.6°C): Over predicted the ice mass →

Do the numerical catch rate for clean surface is over predicted?

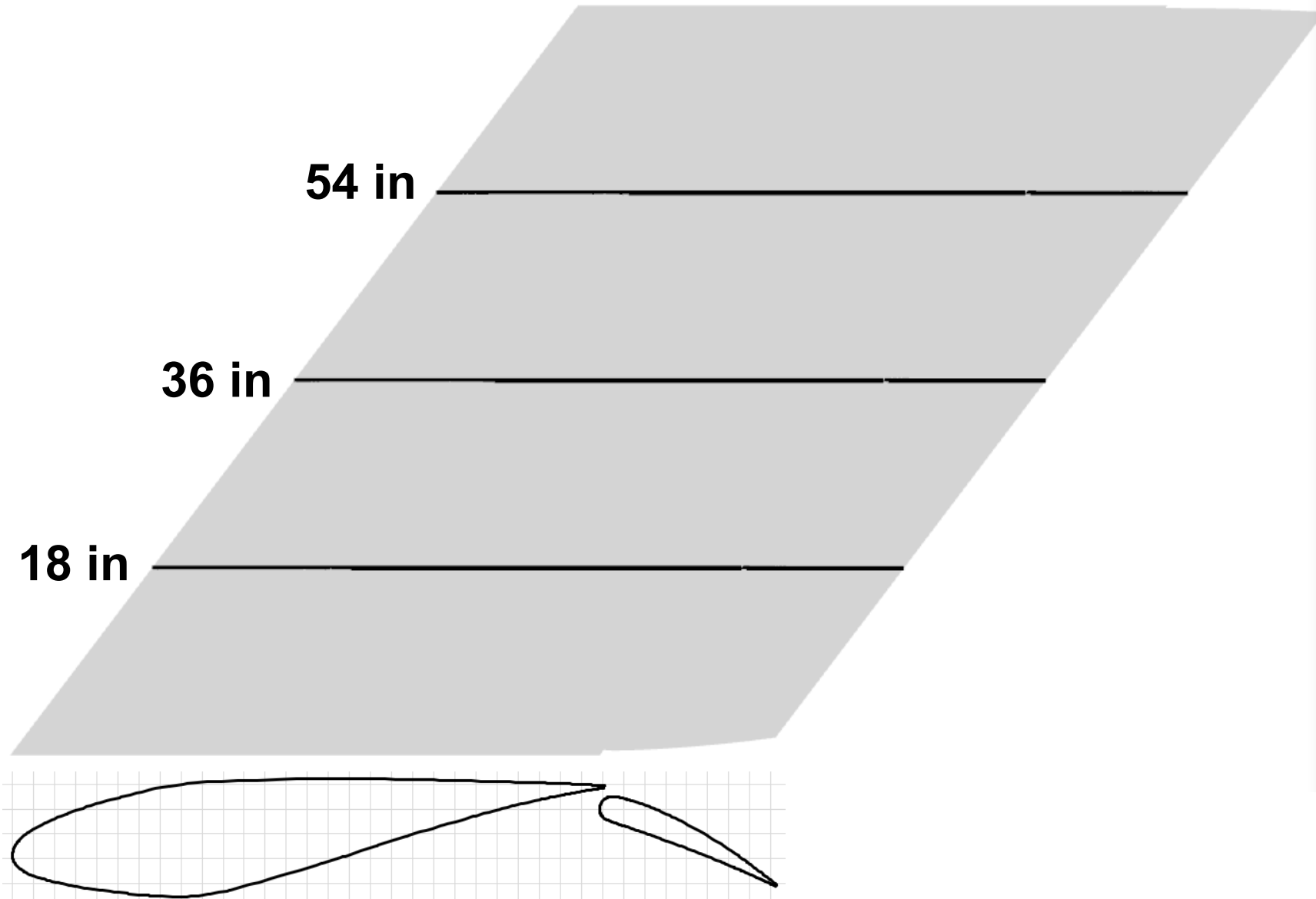
Do the catch rate decrease with time due to the geometry change?

Do evaporation and sublimation are under predicted?

Do water shedding occurs



CRM-65 MidSpan



AoA	3.7	deg
TAS	66.9	m/s
MVD	25	μm
LWC	1	g/m ³
time	29	min

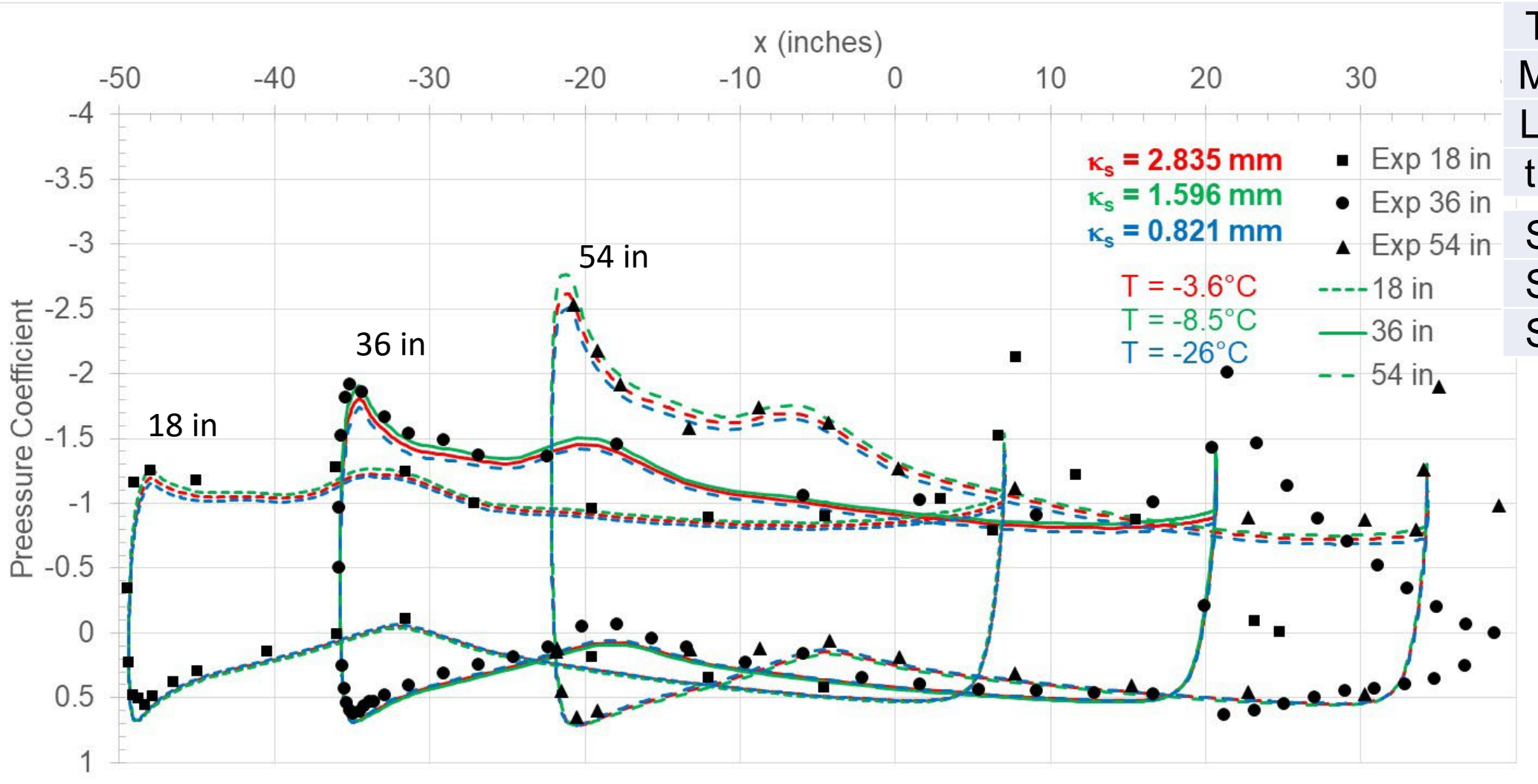
SAT	-3.6	°C
SAT	-8.5	°C
SAT	-26	°C

NASA IRT Volume	Droplet Diameter
0.05	7.3
0.1	9.9
0.2	13.7
0.3	24.9
0.2	44.9
0.1	74.9
0.05	127.6

BOMBARDIER

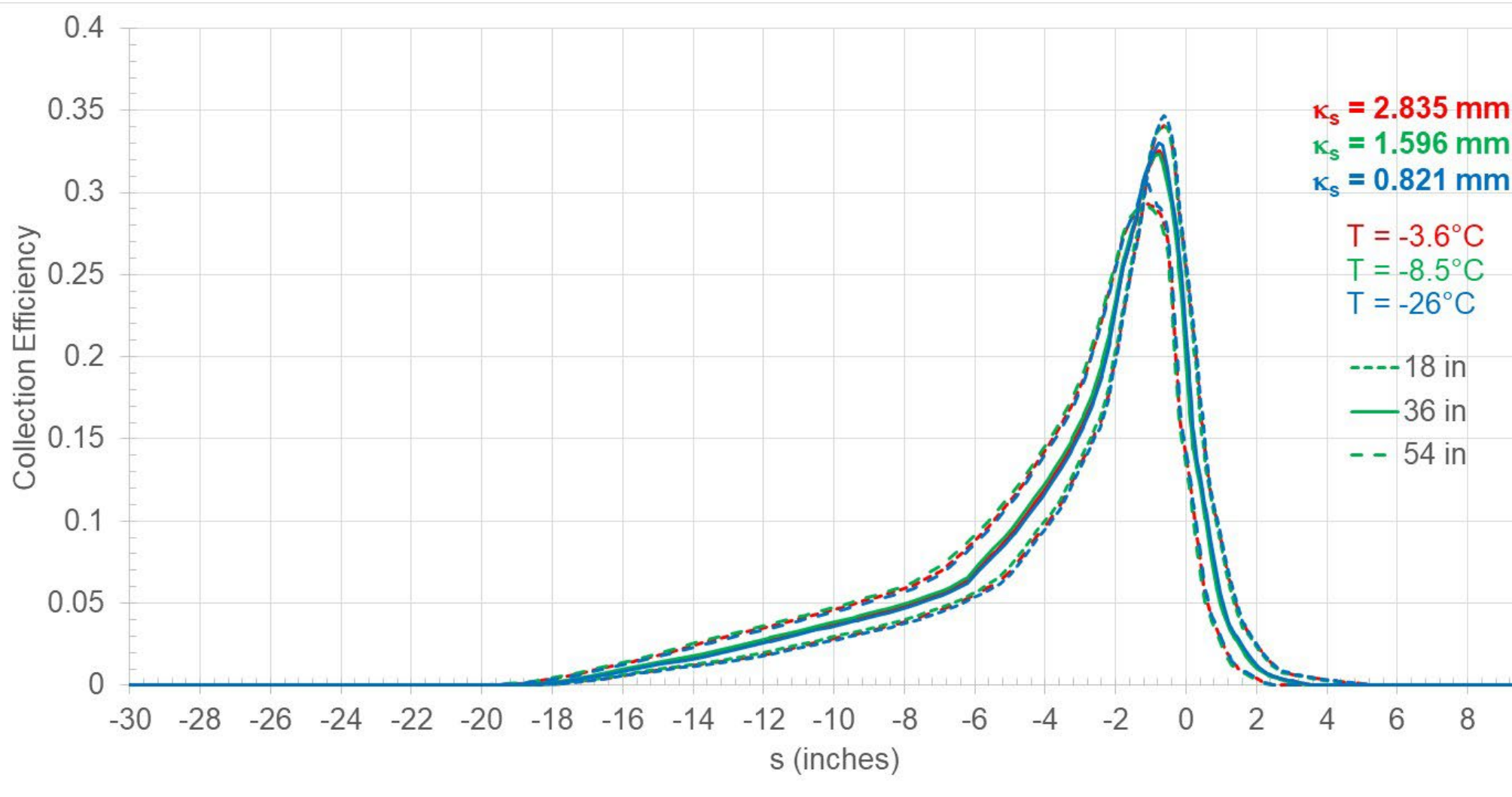
CRM-65 MidSPan

AoA	3.7	deg
TAS	66.9	m/s
MVD	25	μm
LWC	1	g/m^3
time	29	min
SAT	-3.6	$^{\circ}\text{C}$
SAT	-8.5	$^{\circ}\text{C}$
SAT	-26	$^{\circ}\text{C}$



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CRM-65 InBoard

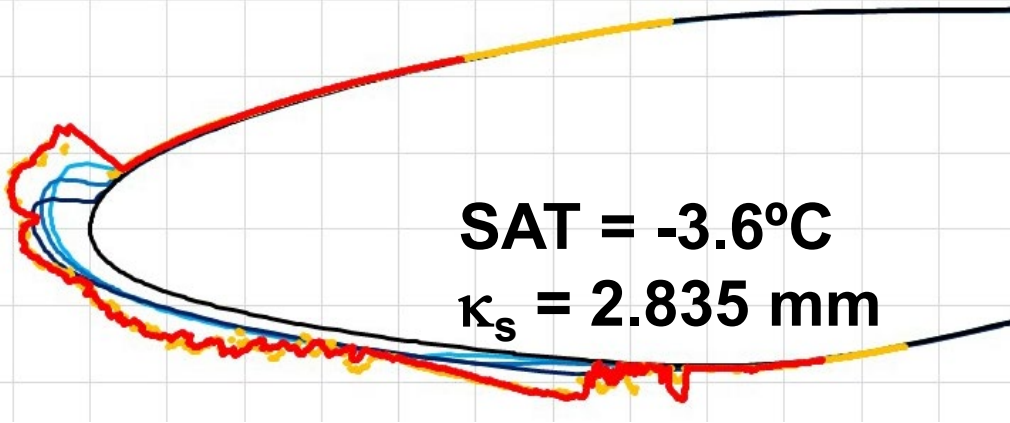


AoA	3.7	deg
TAS	66.9	m/s
MVD	25	μm
LWC	1	g/m ³
time	29	min
SAT	-3.6	°C
SAT	-8.5	°C
SAT	-26	°C

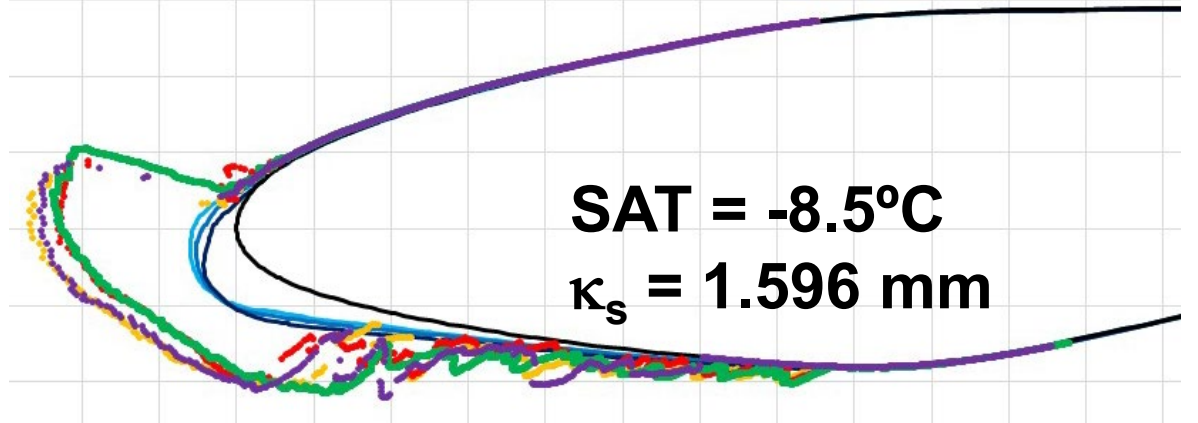
NASA IRT Volume	Droplet Diameter
0.05	7.3
0.1	9.9
0.2	13.7
0.3	24.9
0.2	44.9
0.1	74.9
0.05	127.6

CRM-65 MidSpan

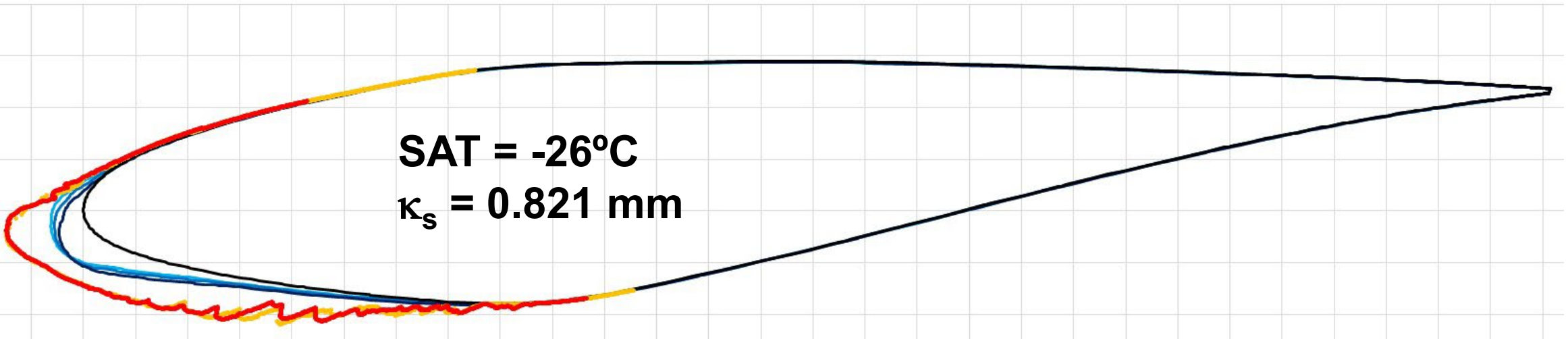
• TH2446 • TH2464 —18 —36 —54 —Clean



• TH2447 • TH2459 • TH2452 • TH2463 —18 —36 —54 —Clean



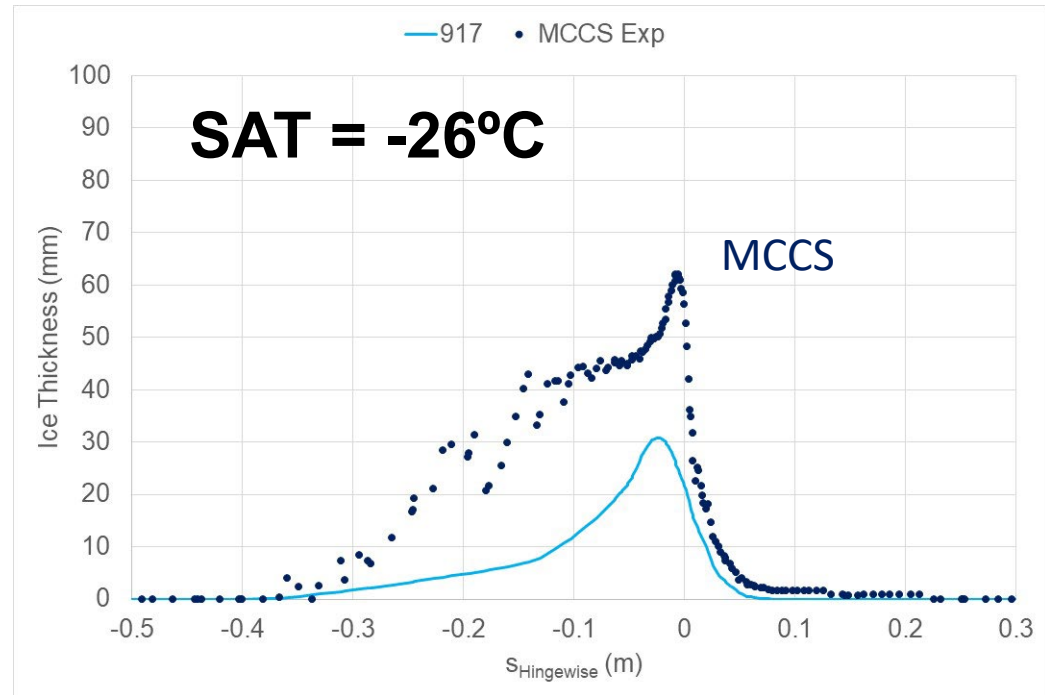
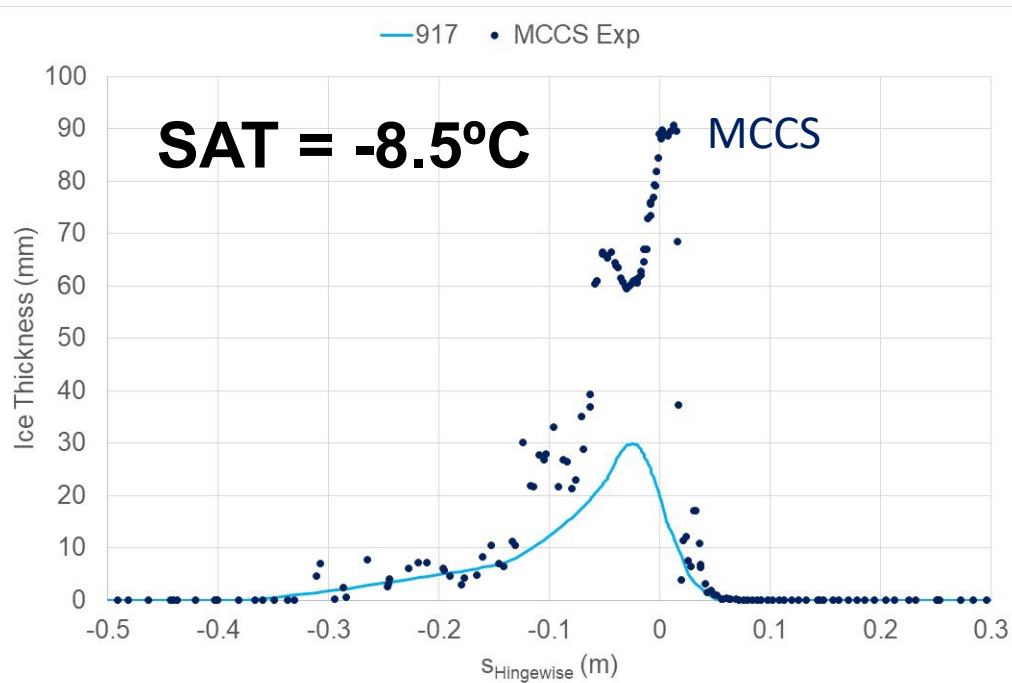
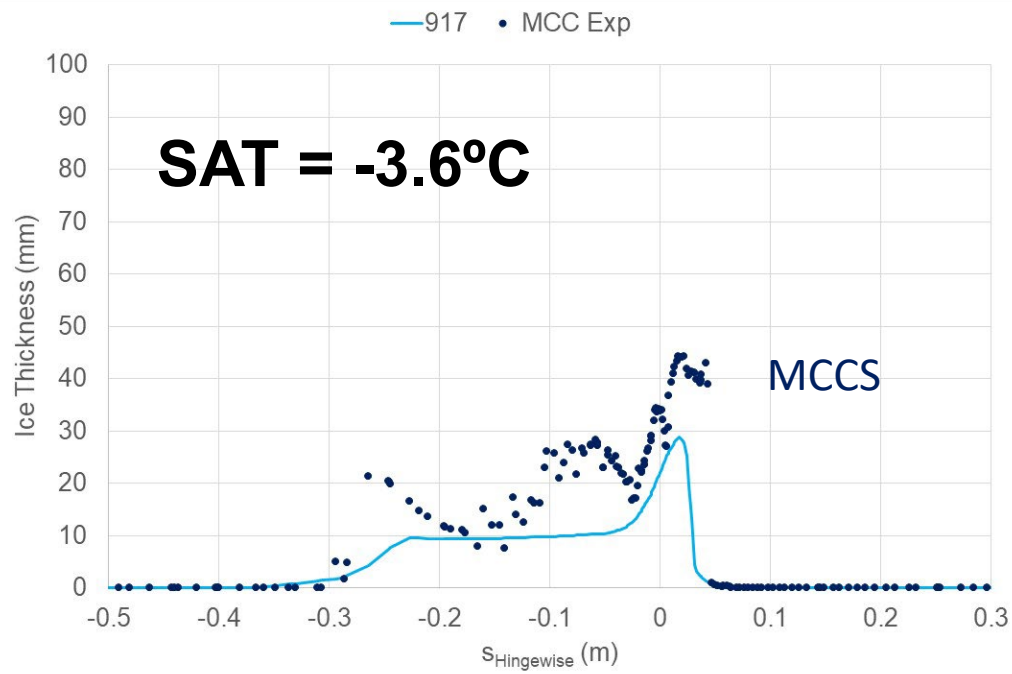
• TH2447 • TH2459 —18 —36 —54 —Clean



CRM-65 MidSpan

SAT (°)	Surface (m ²) Exp	Ice Mass (kg/m) Exp	Ice Density kg/m ³
-3.6	0.011466	4.170	364
-8.5	0.013216	6.420	486
-26.0	0.014025	6.500	463

Hingewise cut



BOMBARDIER

CRM-65 MidSpan

—18 —36 —54 —Clean

• TH2446 • TH2464

SAT = -3.6°C
 $\kappa_s = 2.835 \text{ mm}$
 $\rho_{ice} = 364 \text{ kg/m}^3$

-----18 (917) -----36 (917) -----54 (917)

• TH2447 • TH2459 • TH2452 • TH2463

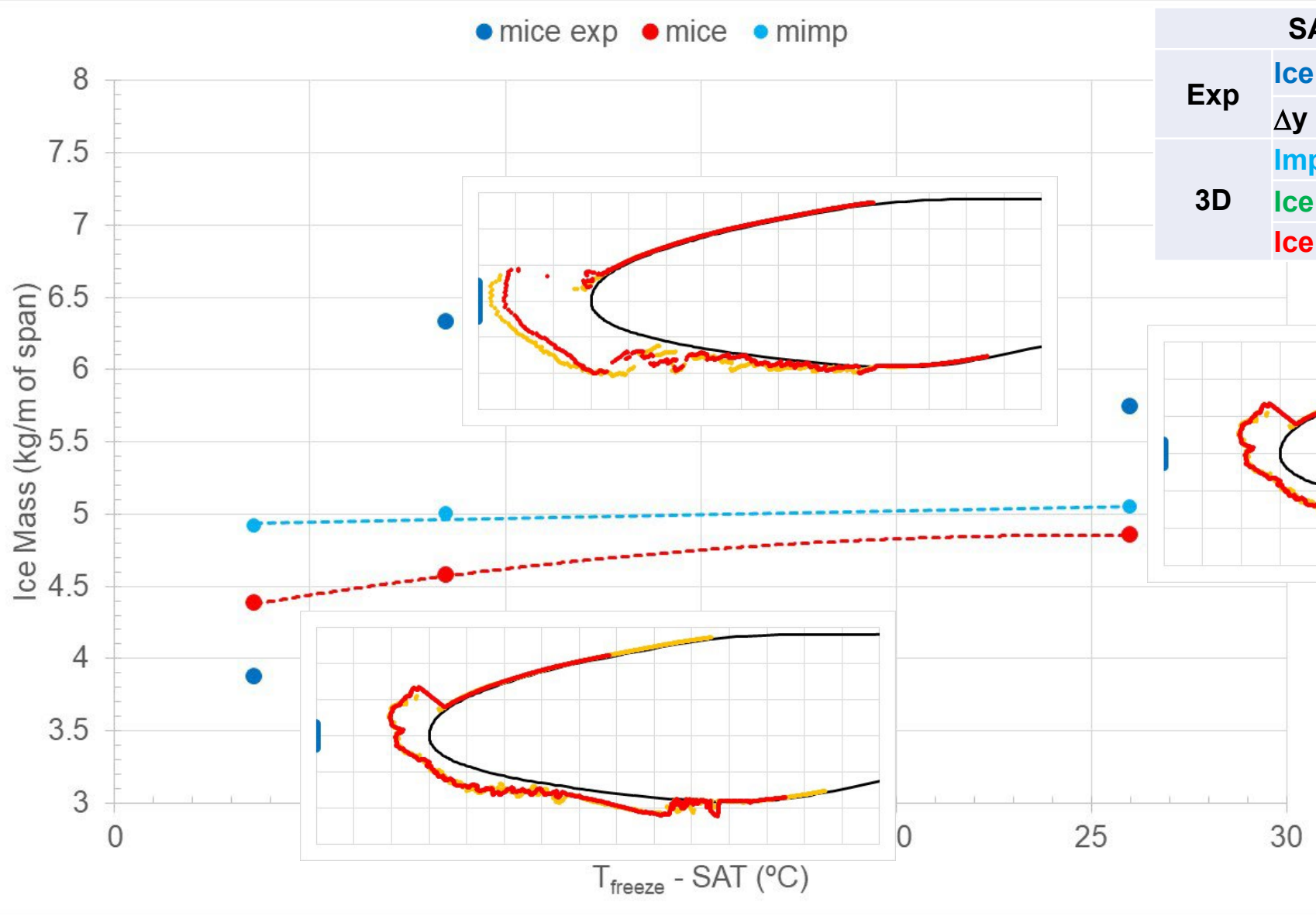
SAT = -8.5°C
 $\kappa_s = 1.596 \text{ mm}$
 $\rho_{ice} = 486 \text{ kg/m}^3$

• TH2447 • TH2459

SAT = -26°C
 $\kappa_s = 0.821 \text{ mm}$
 $\rho_{ice} = 463 \text{ kg/m}^3$

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CRM-65 MidSpan



SAT		-3.6	-8.5	-26	°C
Exp	Ice Mass	3.873	6.420	5.743	kg/m
	Δy	1.310	2.141	1.942	inches
3D	Impingment	4.915	4.999	5.049	kg/m
	Ice Thermo	4.379	4.572	4.853	kg/m
	Ice Thickness	4.163	4.420	4.248	kg/m



CRM-65

Conclusion: 3D Ice Shape Simulation

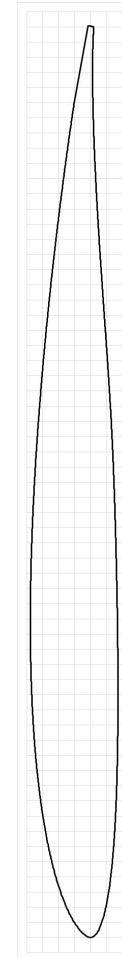
1 layer ice simulation

- Need an equivalent ice density to match the Maximum Combined Cross Section
- If evaporation is under estimated that is due to Test Section Relative Humidity or to the evaporation model
- Artificial Ice Density based on MCCS volume to match ice shape

Multi-Layer Simulation

- Need Catch Rate or Collection Efficiency on
 - clean surface
 - intermediary iced surface
- Need Ice mass
 - few minute after ice accretion start
 - at intermediary time
 - at final time
- Local Ice Roughness Coefficient
- Local Ice Density

RG-15



AoA	4	deg
TAS	25	m/s
MVD	23	μm
LWC	0.44	g/m^3
time	20	min

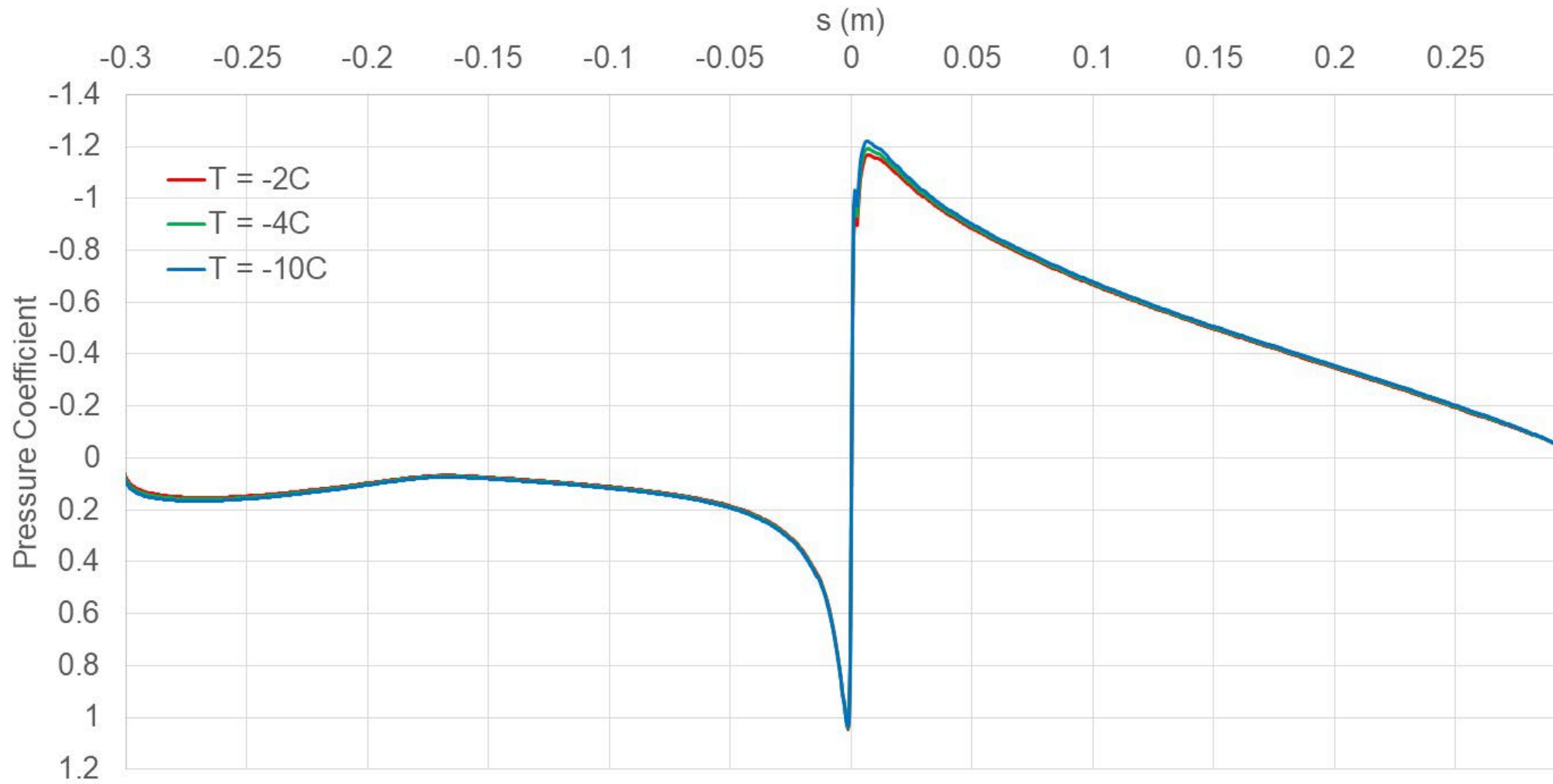
SAT	-2	$^{\circ}\text{C}$
SAT	-4	$^{\circ}\text{C}$
SAT	-10	$^{\circ}\text{C}$

VTT Icing Wind Tunnel	
Volume	Diameter
0.05	6.5
0.1	11.2
0.2	15.7
0.3	22.7
0.2	32.9
0.1	59.5
0.05	96.7

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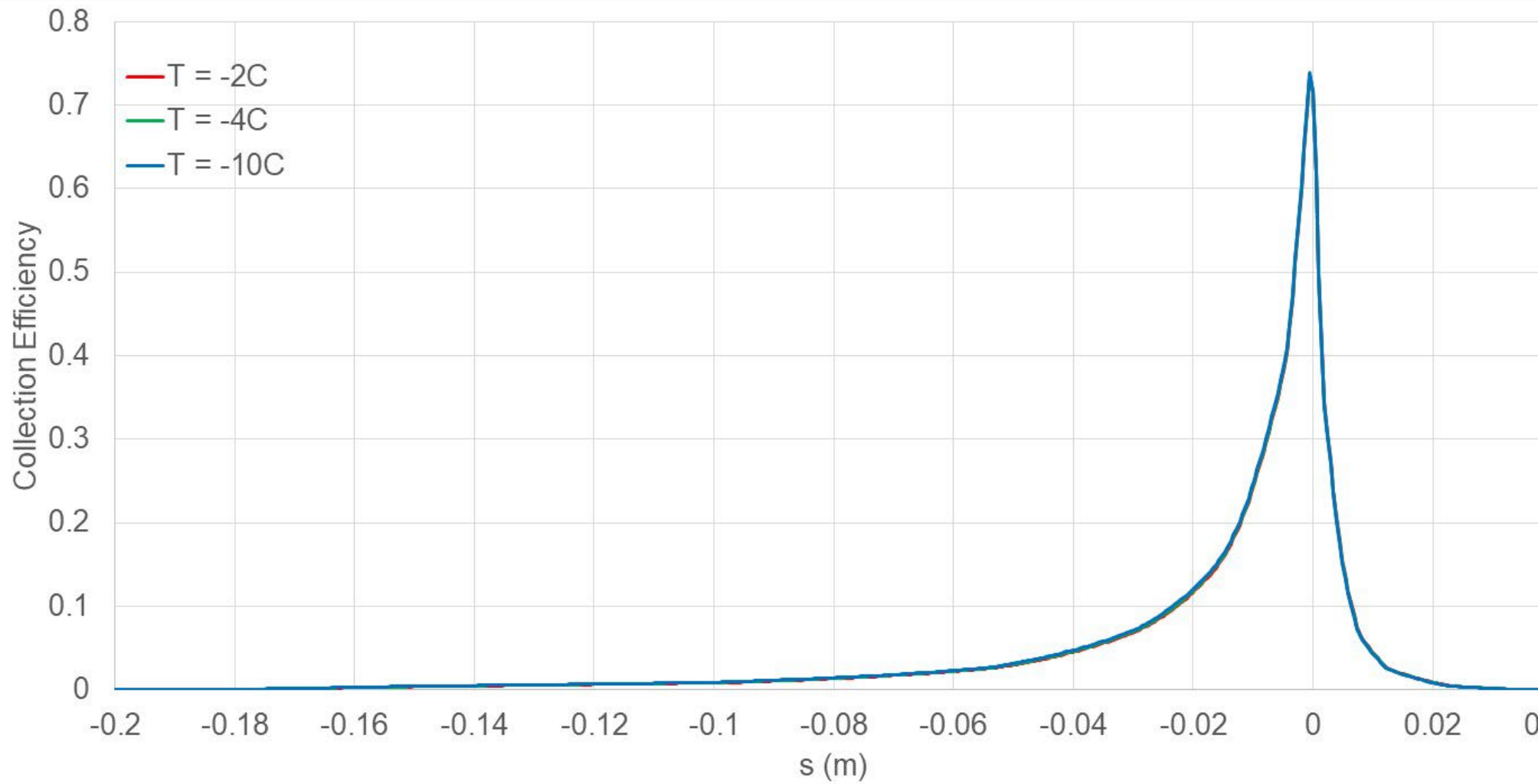
RG-15

AoA	3.7	deg
TAS	66.9	m/s
MVD	25	μm
LWC	1	g/m^3
time	29	min
SAT	-3.6	$^{\circ}\text{C}$
SAT	-8.5	$^{\circ}\text{C}$
SAT	-26	$^{\circ}\text{C}$



BOMBARDIER

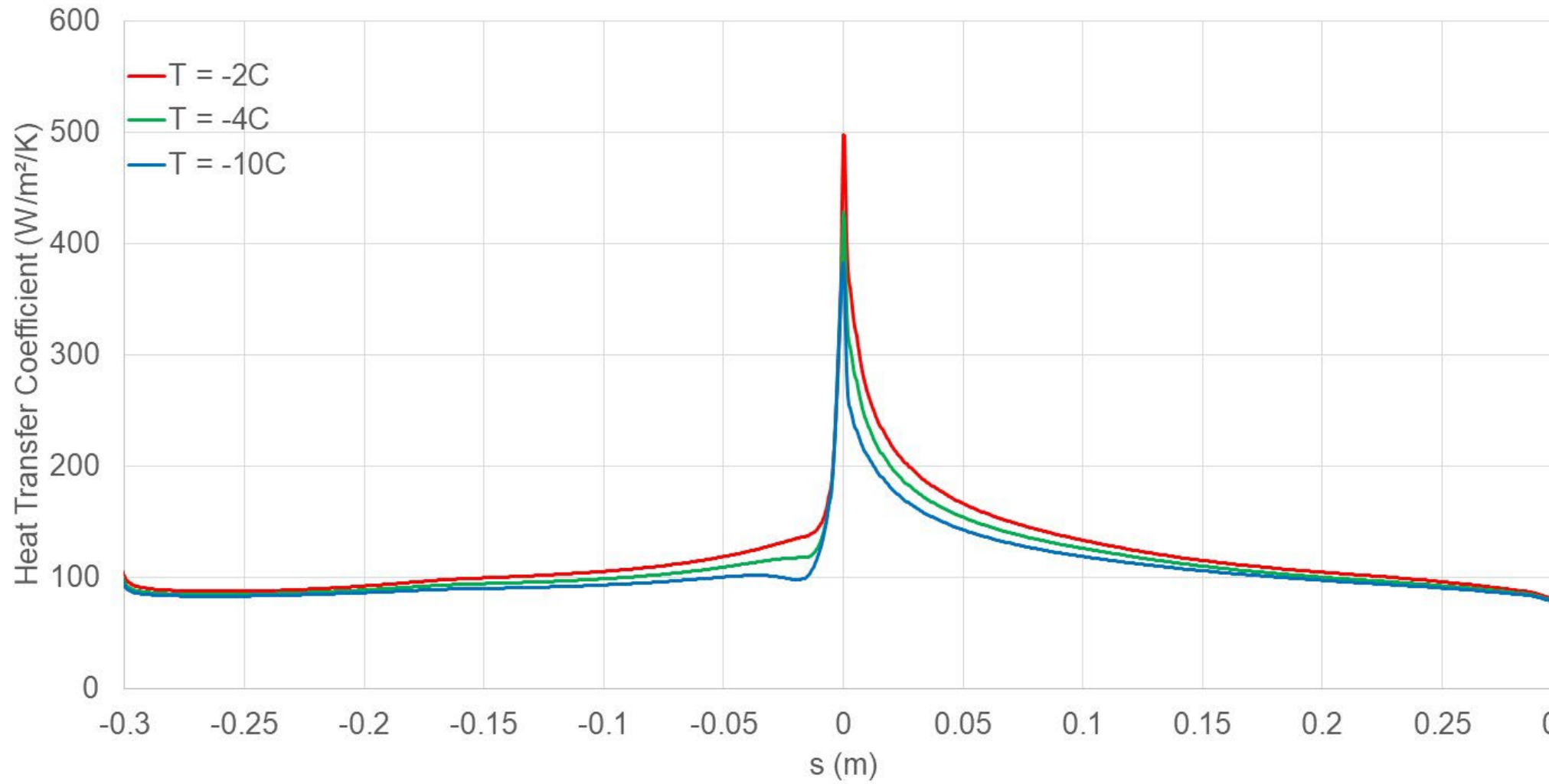
RG-15



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Volume	Diameter	
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0.2	44.9	
0.1	74.9	
0.05	127.6	

BOMBARDIER

CRM-65 InBoard



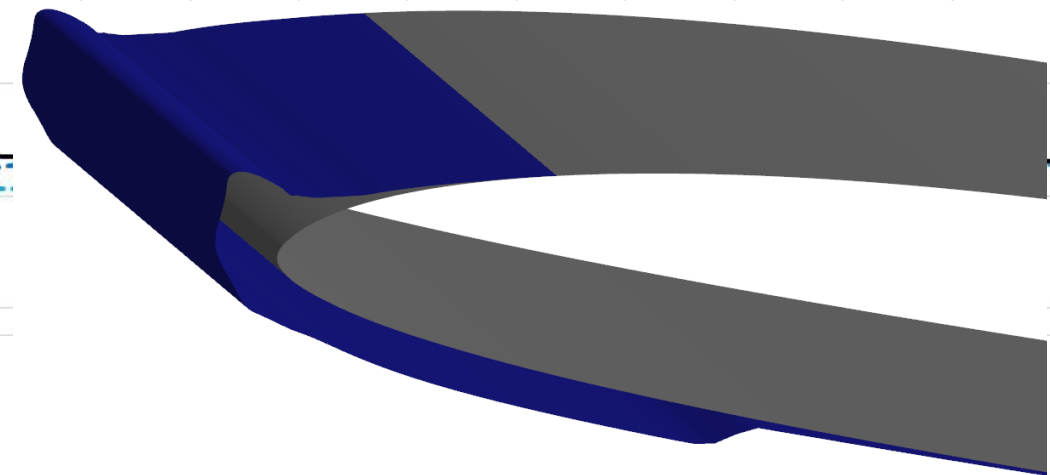
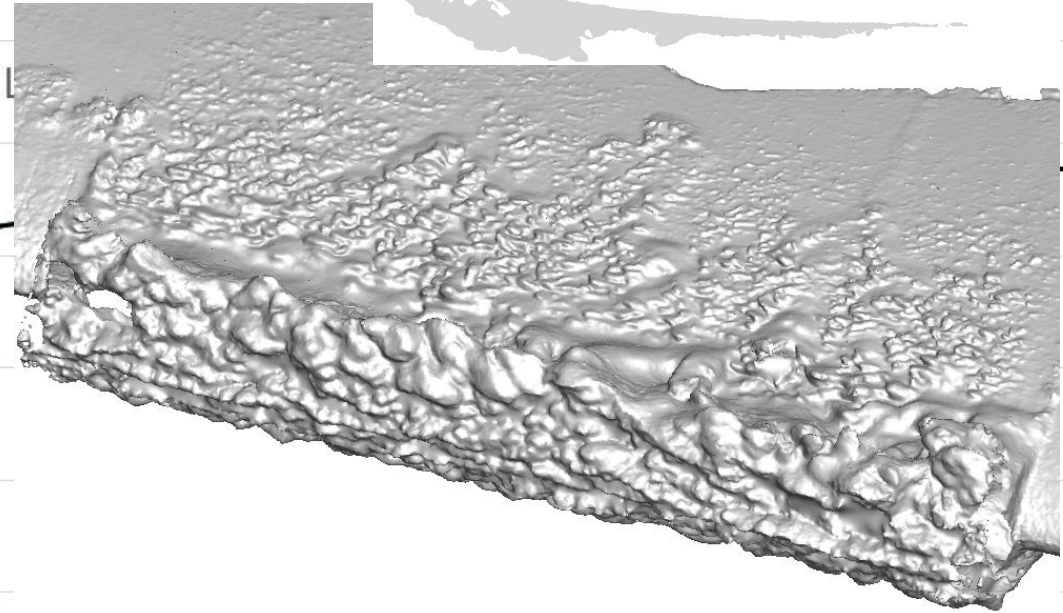
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0.3		24.9
0.2		44.9
0.1		74.9
0.05		127.6

BOMBARDIER

RG-15

--- ks=0.397mm, 10L --- ks=0.397mm, 1L

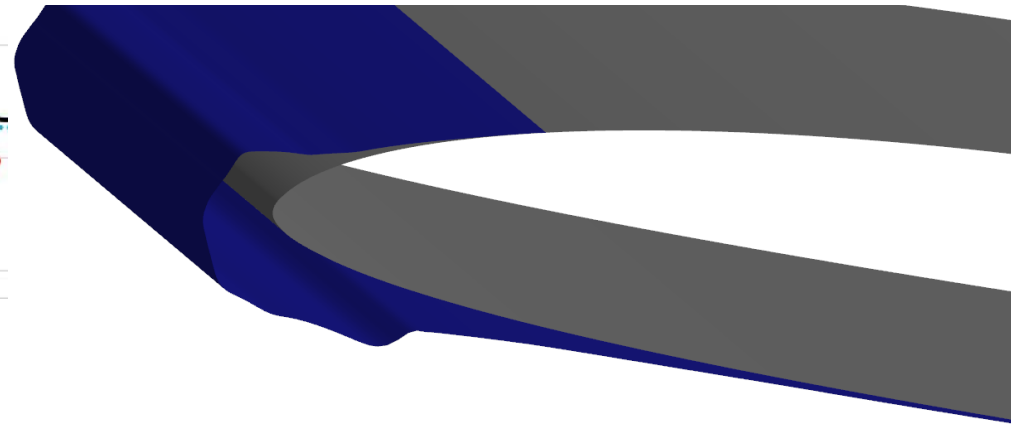
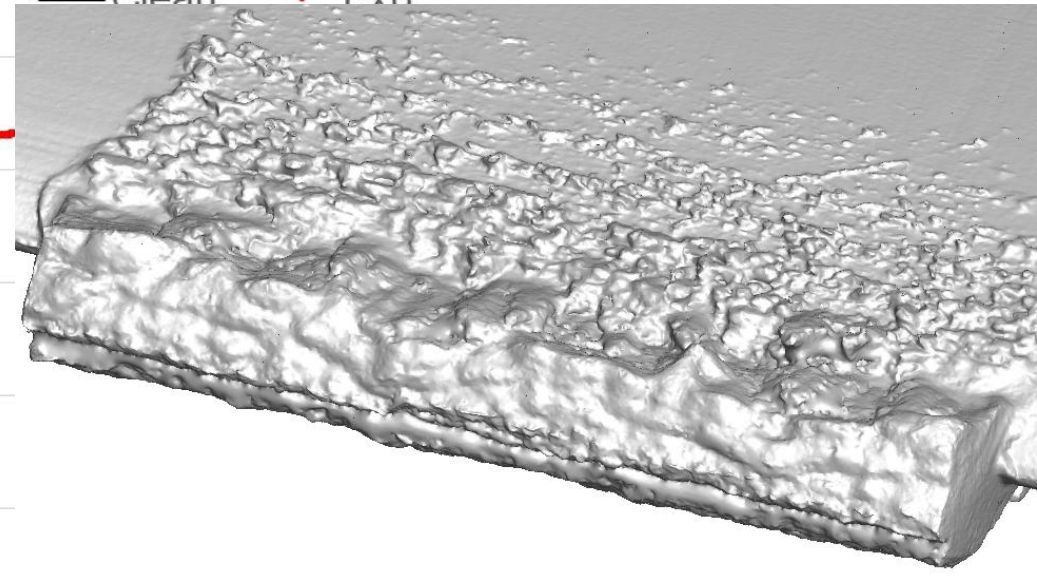
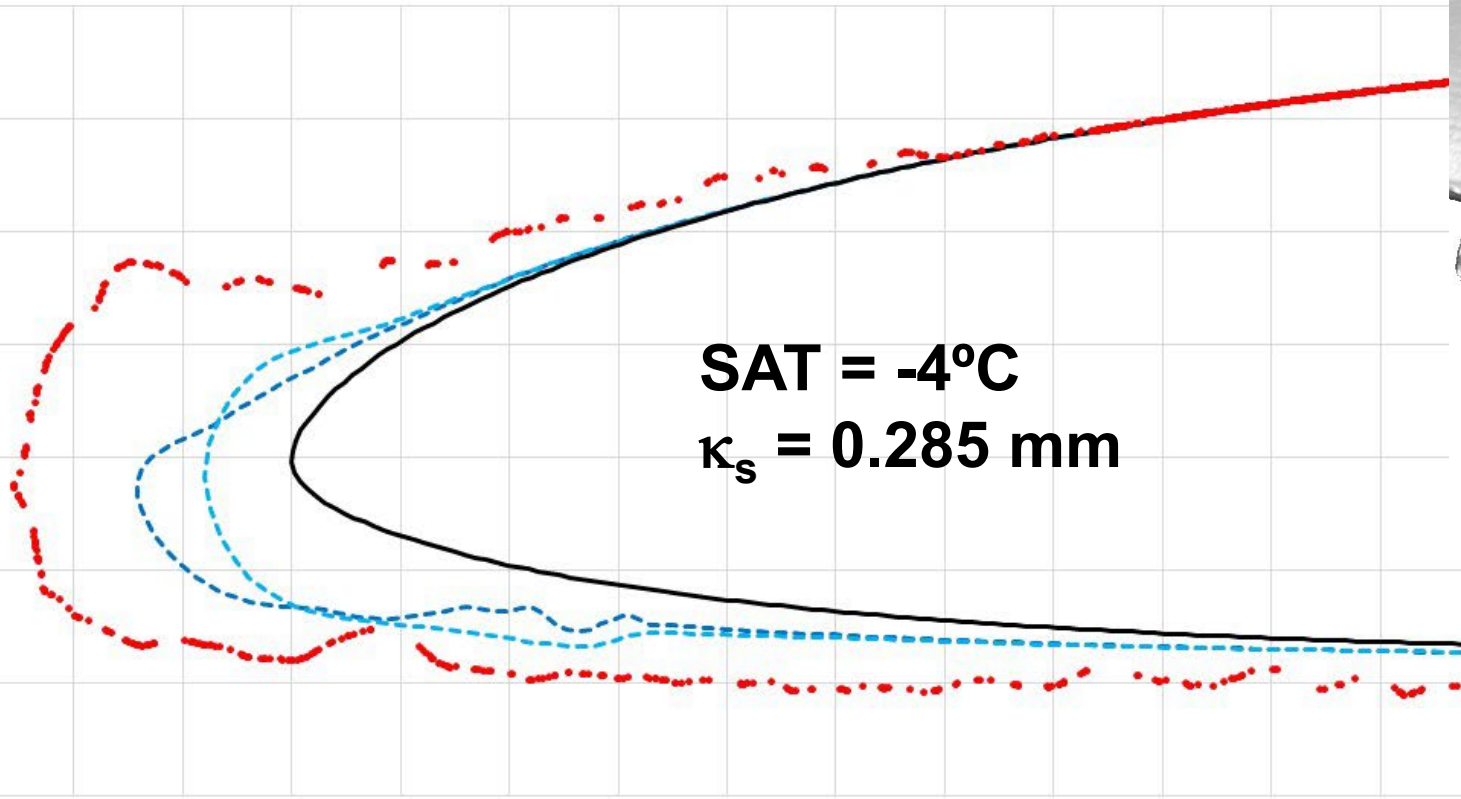
SAT = -2°C
 $\kappa_s = 0.397 \text{ mm}$



BOMBARDIER

RG-15

--- ks=0.285mm, 10L -.- ks=0.285mm, 1L



BOMBARDIER

RG-15

--- ks=0.178mm, 10L --- ks=0.178mm, 1L — Clean — Lap

SAT = -10°C
 $\kappa_s = 0.178 \text{ mm}$

