



This work is licensed under a [Creative Commons Attribution-NonCommercial-NoDerivatives 4.0 International License](https://creativecommons.org/licenses/by-nc-nd/4.0/).



# Ice Prediction Workshop 2

## ONERA's simulations using IGLOO3D

A. Veilleux, E. Radenac, Q. Duchayne

June 23, 2023 – Vienna, Austria

# Outline

---

1. Simulation Process
2. Aerodynamics & Trajectory Outputs
3. Ice shapes
4. Conclusions

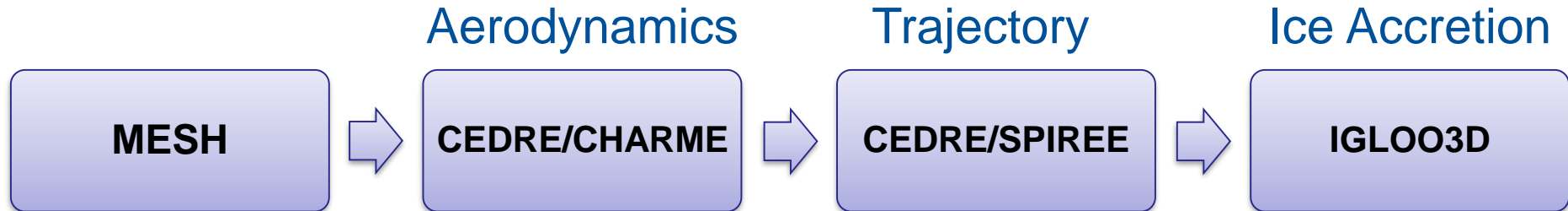
# Outline

---

1. **Simulation Process**
2. Aerodynamics & Trajectory Outputs
3. Ice shapes
4. Conclusions

# Simulation Process

## Computational Method



## Mesh

- Cases 1.X (Midspan) and 2.X (Inboard)
  - Structured mesh with gap from the IPW2
- Cases 3.X (RG15)
  - Structured mesh tunnel from the IPW2

# Simulation Process

## Aerodynamics – CEDRE/CHARME

- Navier-Stokes equations solver
- RANS turbulence model: k- $\omega$  SST model, Boussinesq closing
- 2<sup>nd</sup> order of accuracy in space
- Heat Transfert Coefficient (HTC) on rough-wall

$$h_{tc} = \Phi_w / (T_w - T_r)$$

→ Equivalent sand grain roughness height:  $k_s = c/1000$

- Boundary conditions

→ Airfoil: imposed temperature  $T_{wall} = T_r + 10$  where

$$T_r = T_e \left( 1 + Pr^{1/3} \frac{\gamma - 1}{2} M_e^2 \right)$$

- → Walls: slip conditions

# Simulation Process

---

## Trajectory – CEDRE/SPIREE

- Eulerian droplet-trajectory solver
- 2nd order of accuracy in space
- Particle distribution: provided droplet size distributions
- Full deposition
- Schiller and Naumann model for the droplet drag

## Ice Accretion – IGLOO3D/MESSINGER3D

- Messinger balance for ice accretion
- Ice density given by model of Makkonen and Stallabras or constant
- Predictor computations (1-step, no re-meshing)

# Outline

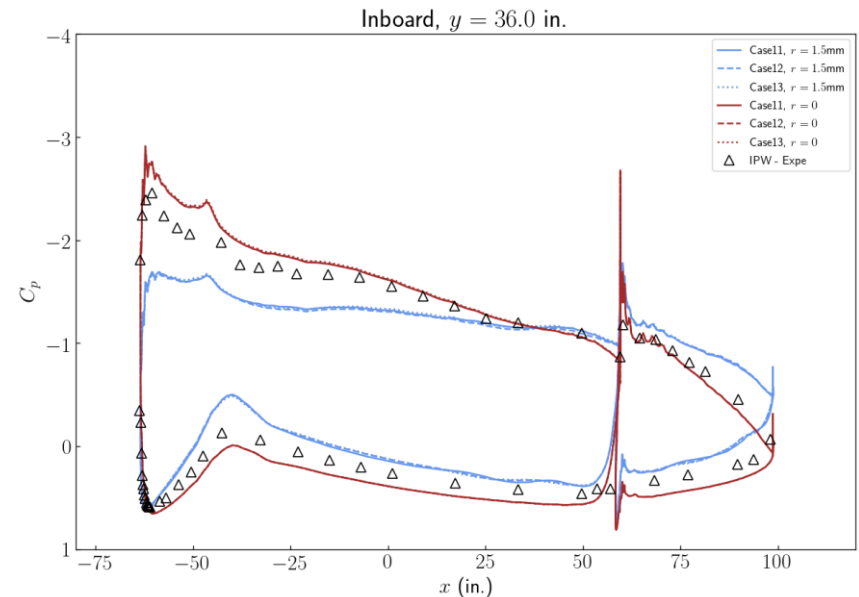
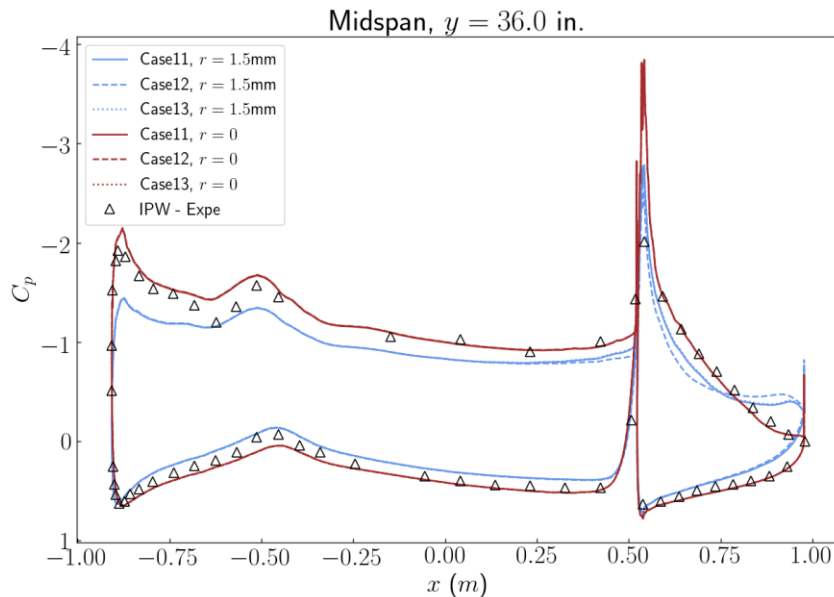
---

1. Simulation Process
- 2. Aerodynamics & Trajectory Outputs**
3. Ice shapes
4. Conclusions



# Aerodynamics & Trajectory Outputs

## Impact of the wall roughness on the pressure coefficient



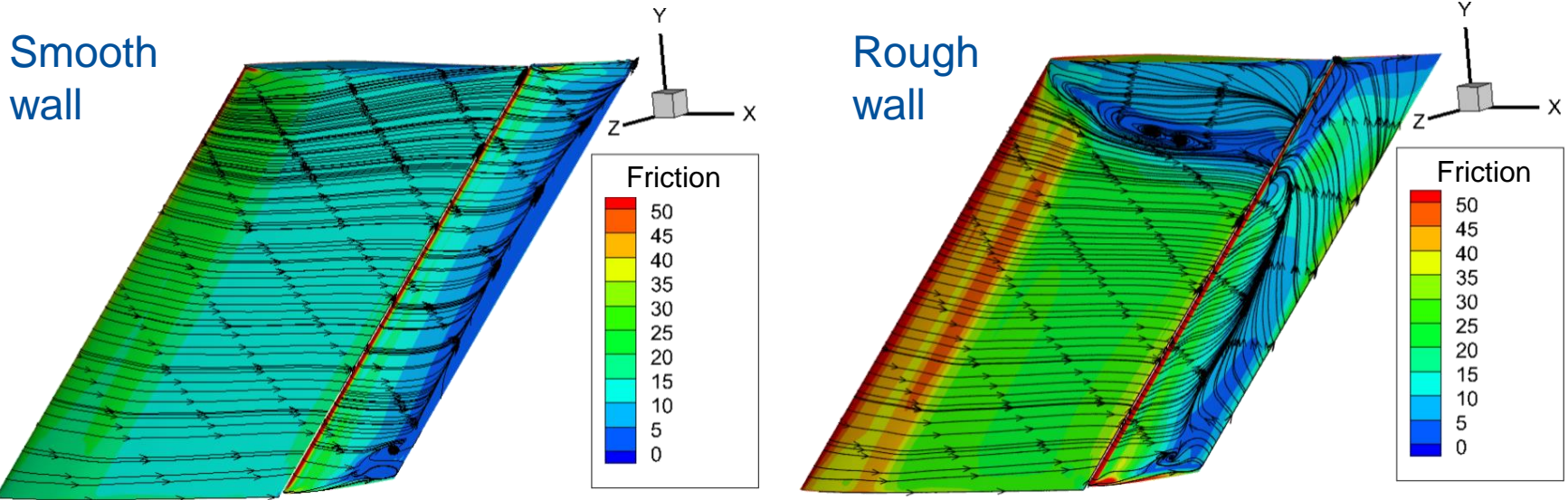
For both the Midspan and the Inboard:

- The pressure coefficient obtained on a smooth wall are in good agreements with the experiments
- Considering a rough-wall leads to a poorer  $C_p$

→ Why is that ?

# Aerodynamics & Trajectory Outputs

## Impact of the wall roughness – Midspan



→ The whole flow structure is modified

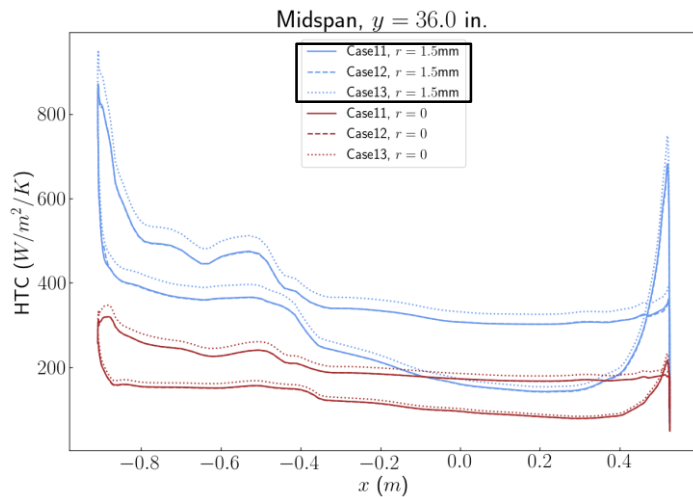
→ The rough-wall model is a priori not the (only) cause of the problem (past simulations with elsA showed no visible effect of the rough-wall model, cf E. Radenac presentation at SAE 2023).

# Aerodynamics & Trajectory Outputs

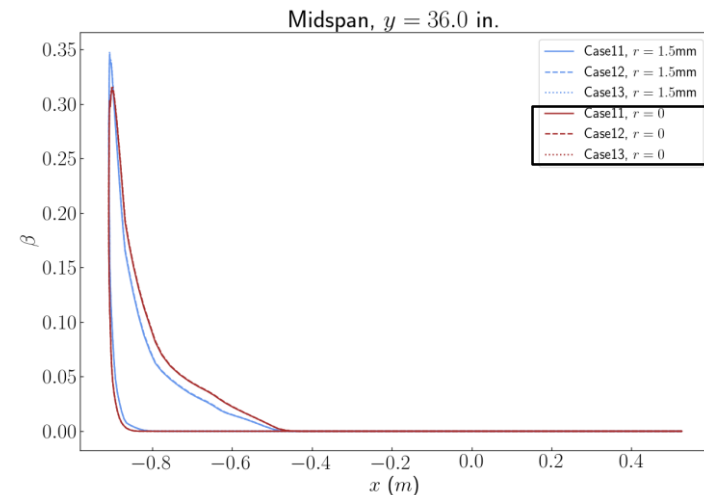
## Impact of the wall roughness – Cases 1.X (MIDSPAN)

→ Choice is made to adopt an ‘hybrid’ approach

- Heat Transfer Coefficient is extracted from the rough wall simulation
- The smooth wall simulation is imposed as the aerodynamics field for the trajectory simulation



- A higher HTC is obtained considering a rough airfoil (as expected)

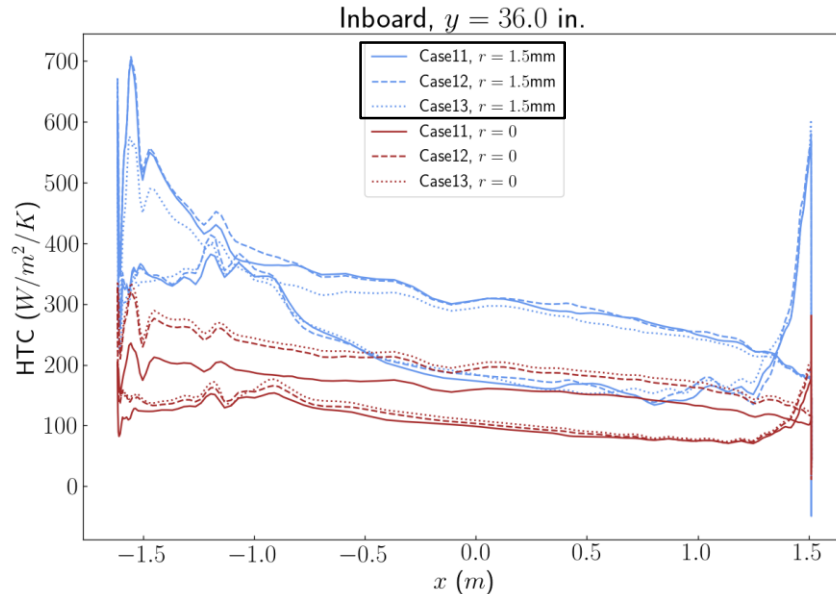


Smooth airfoil leads to

- a higher  $\beta$  on the lower surface
- a smaller one on the upper surface and at the attachment line

# Aerodynamics & Trajectory Outputs

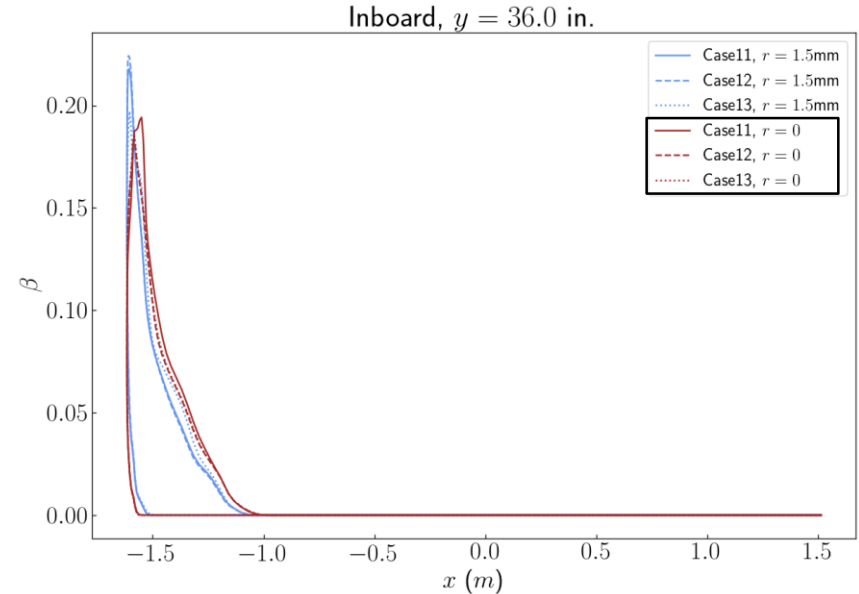
## HTC and collection efficiency – Cases 2.X (INBOARD)



A higher HTC is obtained:

- Considering rough airfoil

Given the discrepancy between cases, results on the inboard seem to be more dependant on the icing conditions

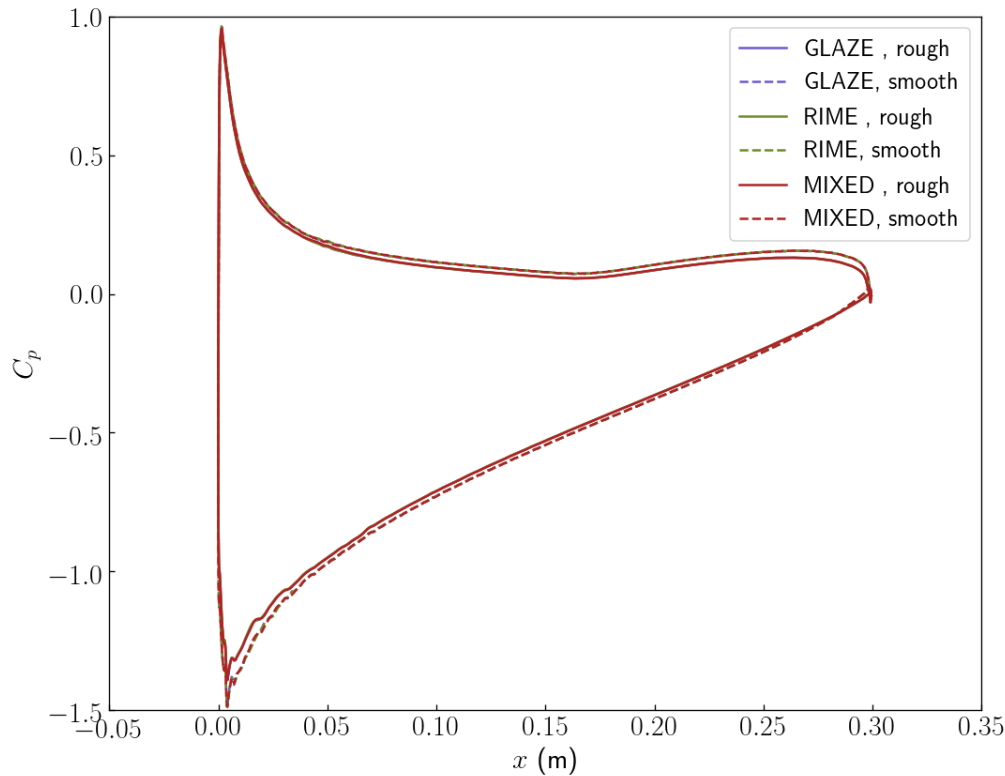


Smooth airfoil leads to

- a higher  $\beta$  on the lower surface
- a smaller one on the upper surface and at the attachment line

# Aerodynamics & Trajectory Outputs

## Impact of the wall roughness – Cases 3.X (RG15)

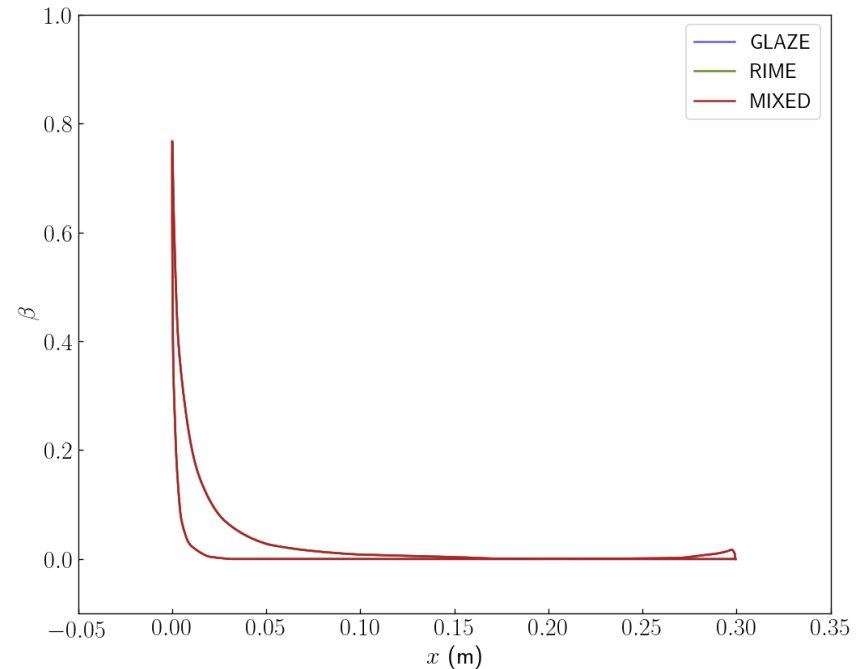
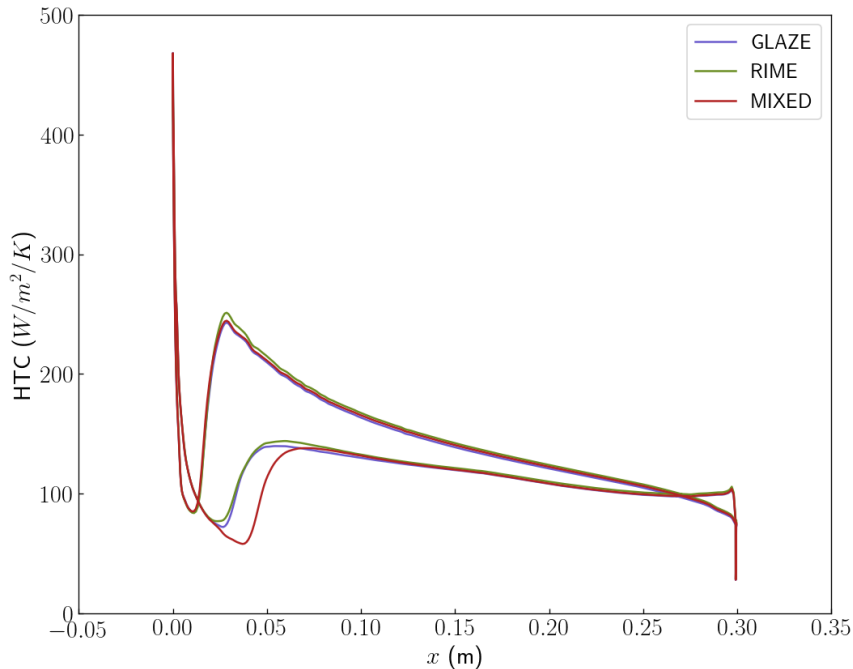


- All conditions lead to the very same pressure coefficient
- Small difference are observed between the rough and smooth pressure coefficients but they remain very close and the flow structure is not modified

→ For the RG15 simulations, both the aerodynamics and trajectory simulations are carried out considering a rough airfoil

# Aerodynamics & Trajectory Outputs

## HTC and collection efficiency



- Same HTC is obtained for the three test case conditions except on the upper surface where the mixed condition leads to a slightly lower HTC
- No influence of the test case conditions on the collection efficiency

# Outline

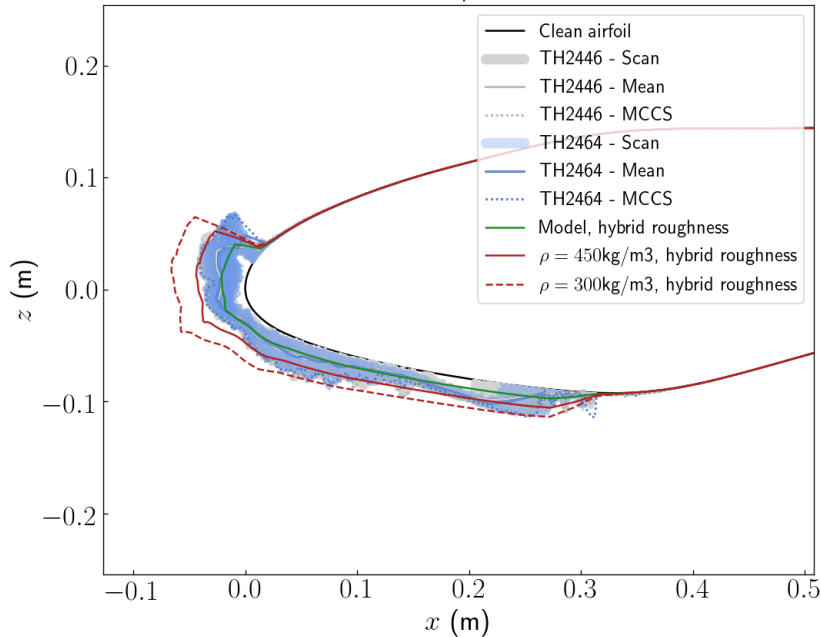
---

1. Simulation Process
2. Aerodynamics & Trajectory Outputs
- 3. Ice shapes**
4. Conclusions

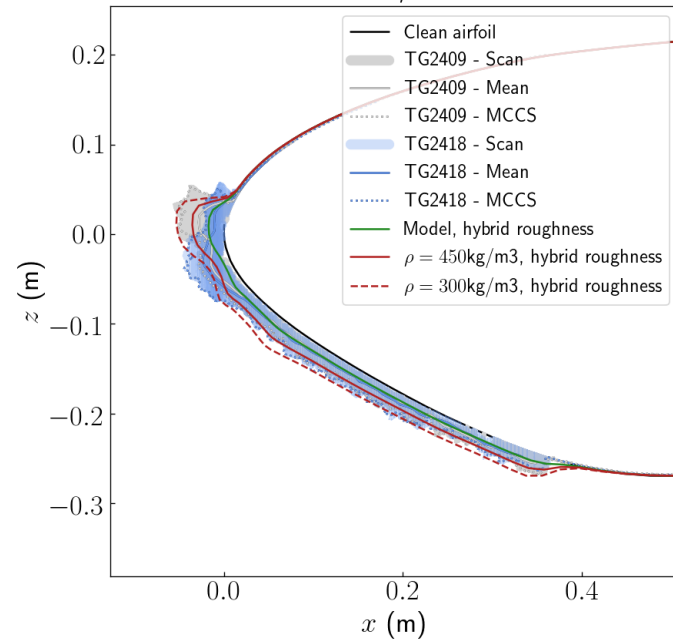
# Ice shapes

## Warmer cases

MIDSPAN, CASE11



INBOARD, CASE21



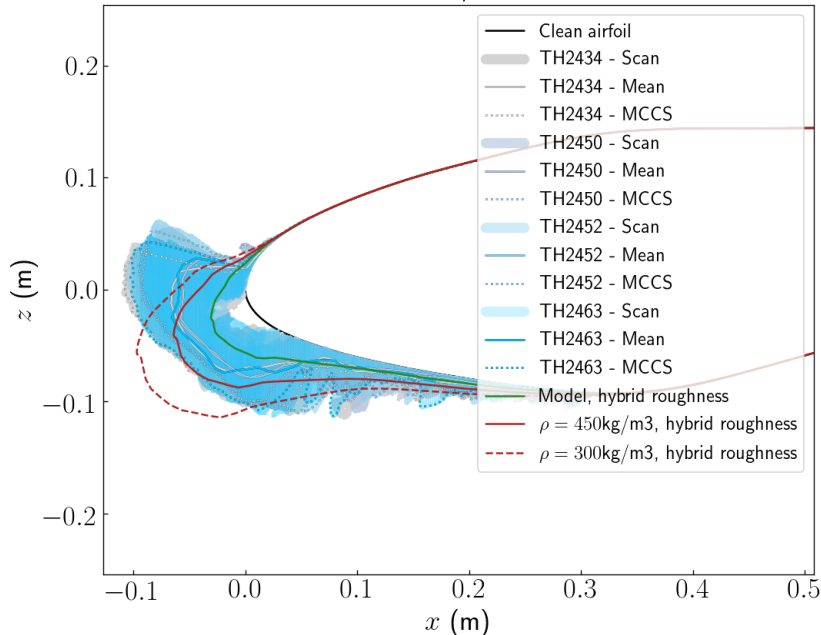
- Proper levels, shapes and ice limits
- MCCA is best predicted for a fixed density
- Mean shape is best predicted with the Makkonen and Stallabras model (MS model) for the ice density



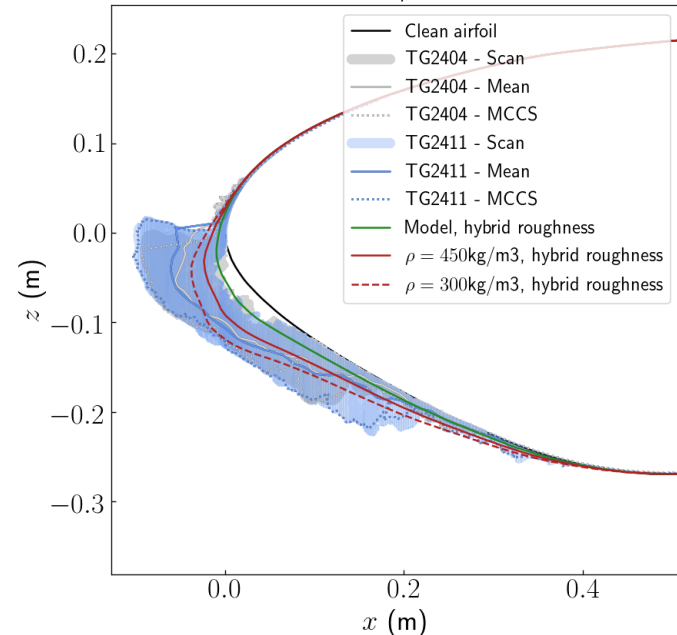
# Ice shapes

## Maximum scallop cases

MIDSPAN, CASE12



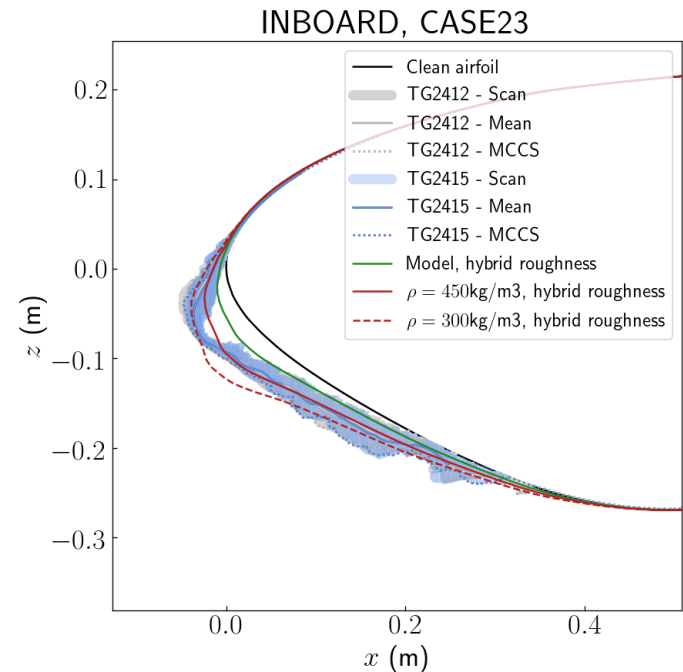
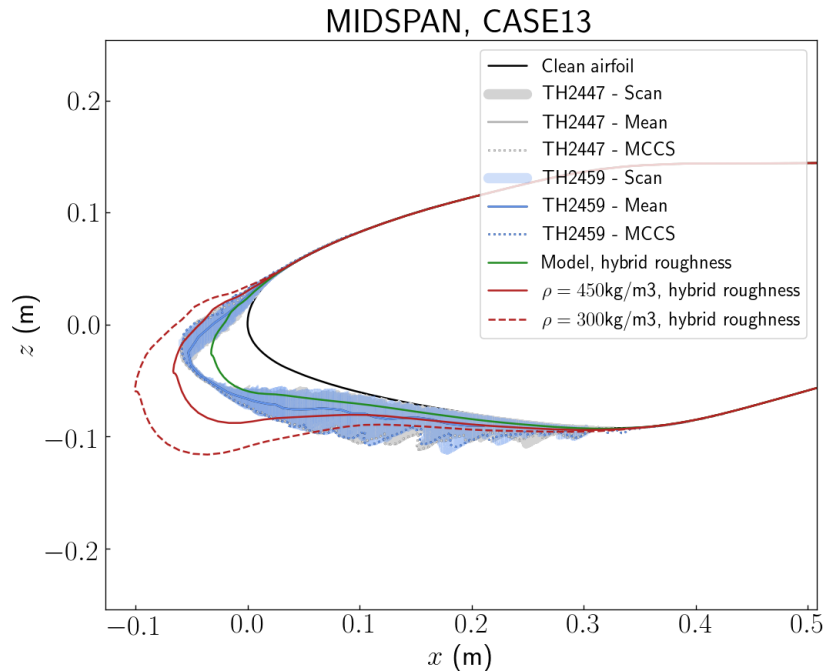
INBOARD, CASE22



- Levels obtained with a fixed density are closer to the (MCCA or mean) experiments than with a modelled density.
- Compared to the MCCA, shapes are not so good...
- Ice limits are rather well predicted
- The ice shape produced with bulk  $\rho_{ice}=450\text{ kg/m}^3$  (resp.  $300\text{ kg/m}^3$ ) is more representative of the mean ice shape for the midspan (resp. the inboard).

# Ice shapes

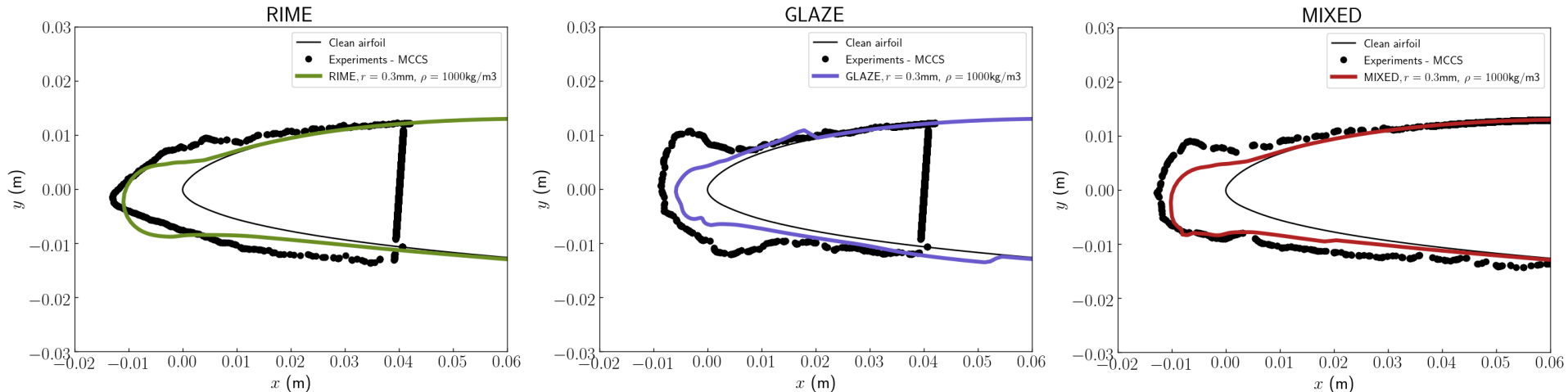
## Rime cases



- Ice limits are rather good
- For the midspan, the shape and level obtained when modelling the density are okay at the attachment line but lower elsewhere
- The ice shape obtained with a fixed ice density of 300 kg/m<sup>3</sup> for the inboard is better.

# Ice shapes

## RG15 (3.1, 3.2, 3.3)



All ice shapes were obtained using a modelled density

- Rime: the ice thickness level at the leading edge matches the experiment but the conical shape is not captured
- Glaze: shape and levels are not well represented
- Mixed: levels and shapes are rather good

→ Comparison with results from IGLOO2D must be conducted in the future

# Outline

---

1. Simulation Process
2. Aerodynamics & Trajectory Outputs
3. Ice shapes
- 4. Conclusions**

# Conclusion

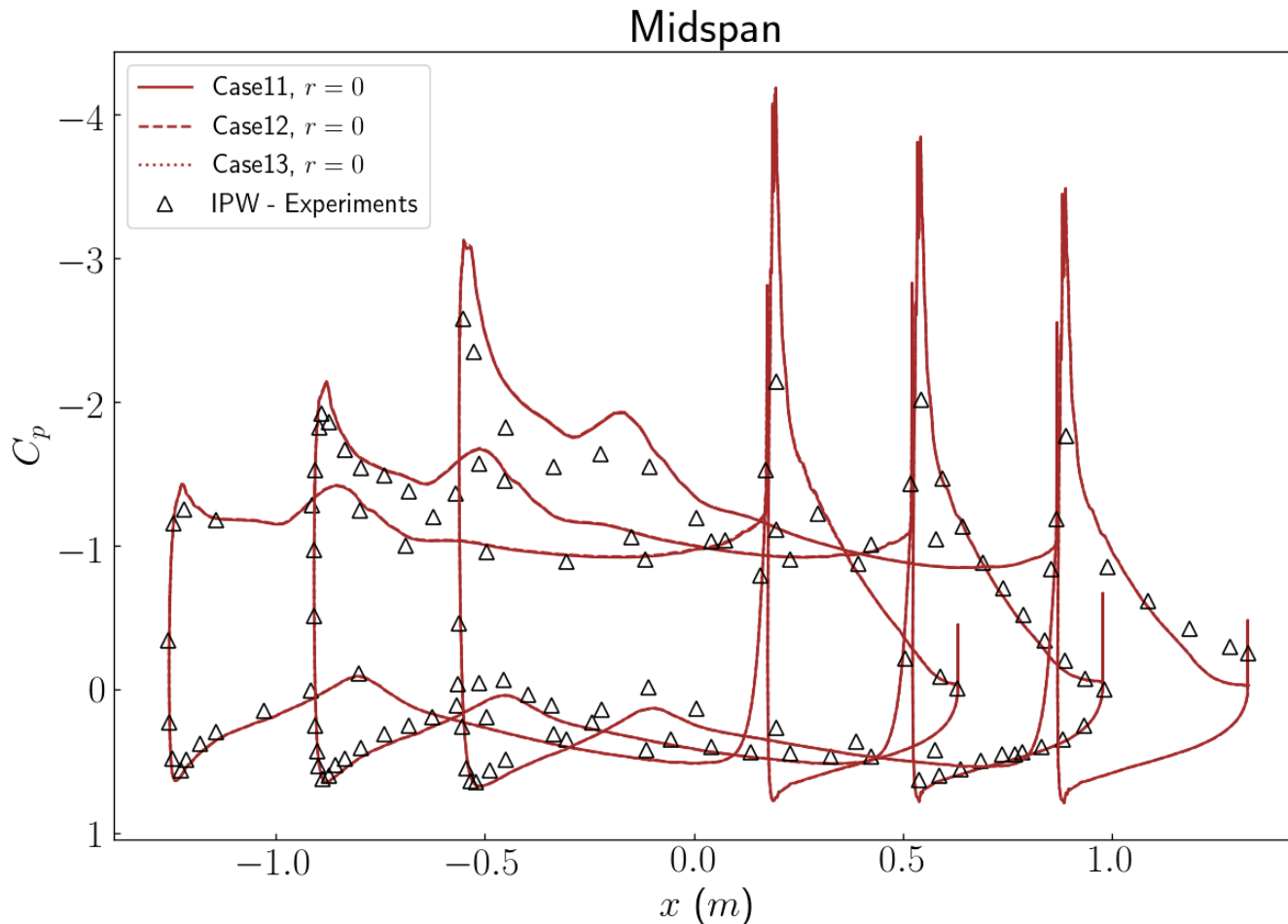
---

- IGLOO3D was run on all the cases of the IPW2 database.
- Only 1-step simulations were conducted.
- The impact of the ice density modelling was studied. Depending on the conditions, the MS model or the use of a constant ice density can be more representative of the mean or the MCCS, as detailed in the presentation.
- The next step would be to run multi-step simulations

Thank you for your attention! Any questions?

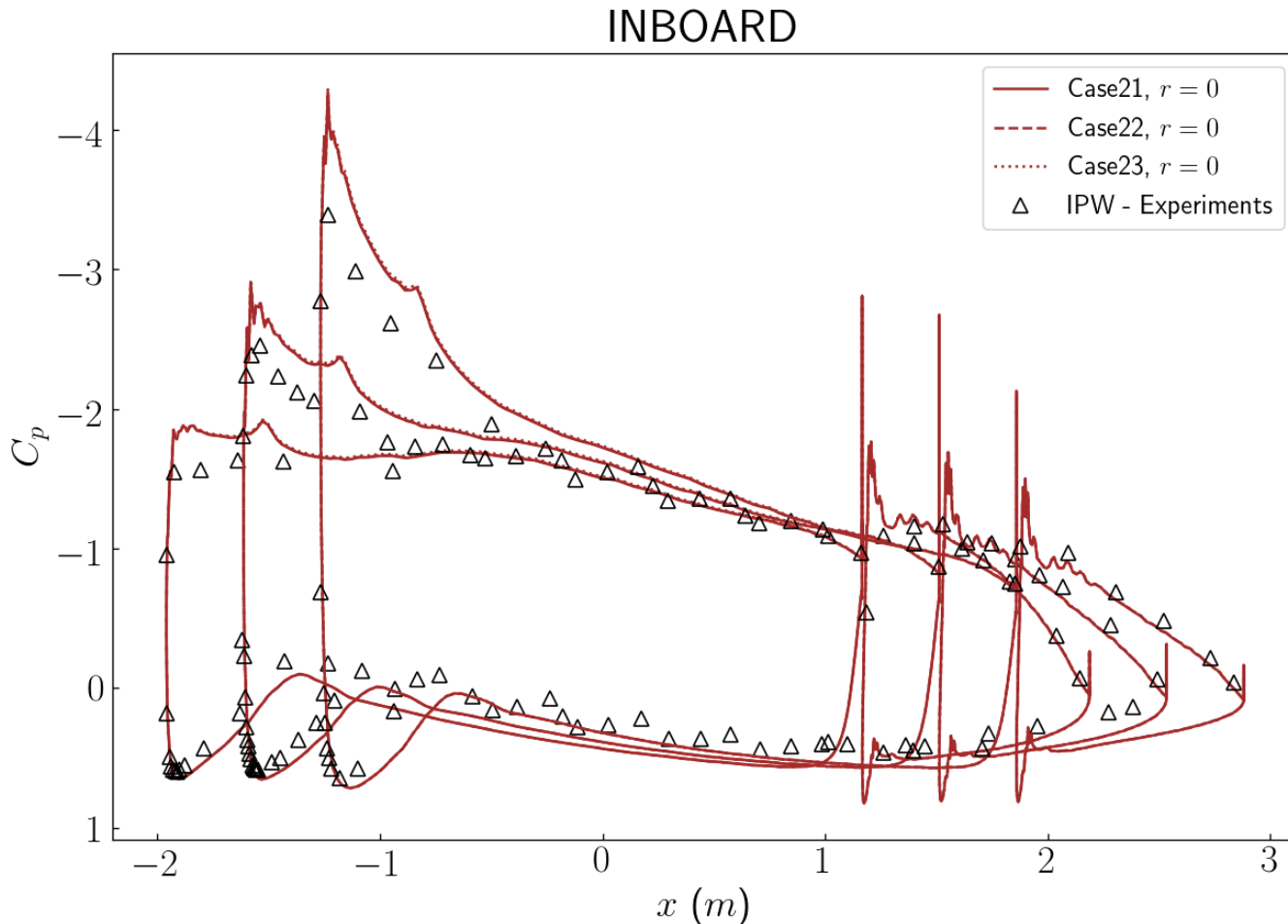
# Aerodynamics – Pressure Coefficient

## Comparison with experimental data – Cases 1.X (MIDSPAN)



# Aerodynamics – Pressure Coefficient

## Comparison with experimental data – Cases 2.X (INBOARD)



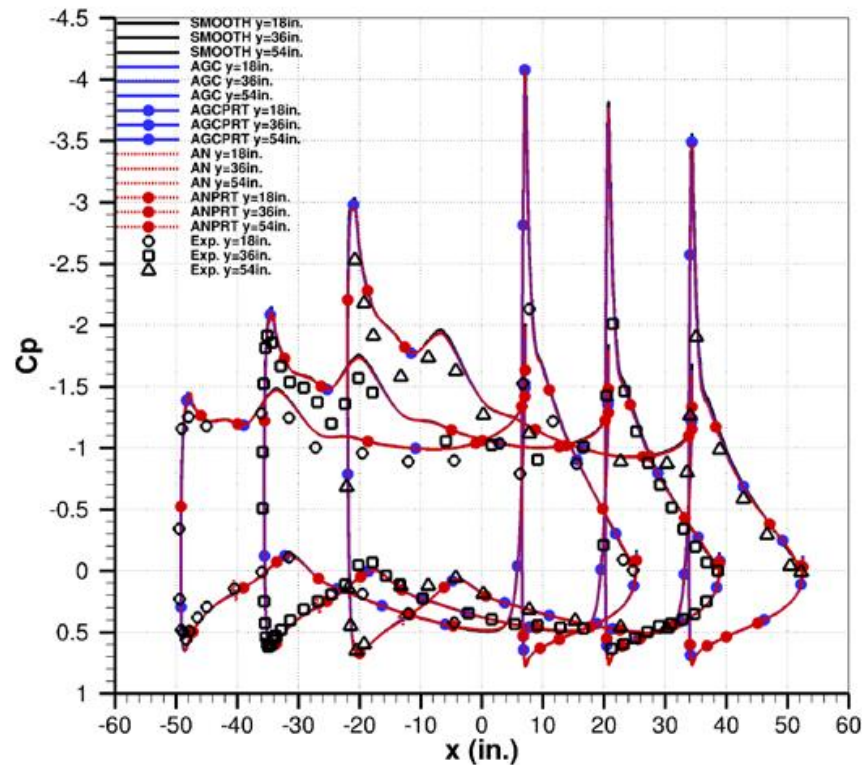
# Presentation of the simulations

## Numerical strategy for the CRM65 database

- Effects of our rough-wall modelling on the simulations: rough-wall vs. smooth-wall
  - The rough-wall model is a priori not the cause of the problem

Past simulations with elsA on the Midspan geometry:

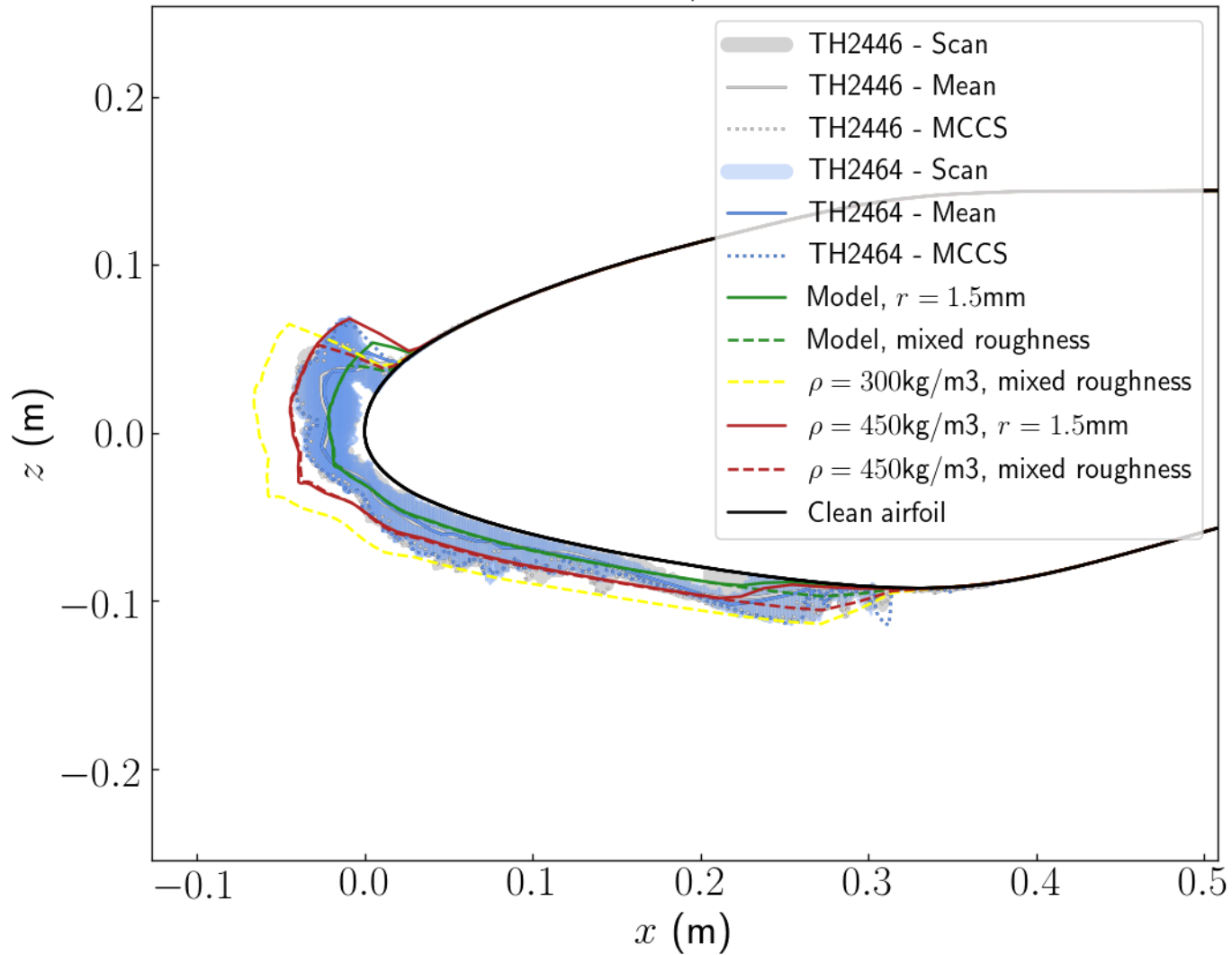
No visible effect of the rough-wall model



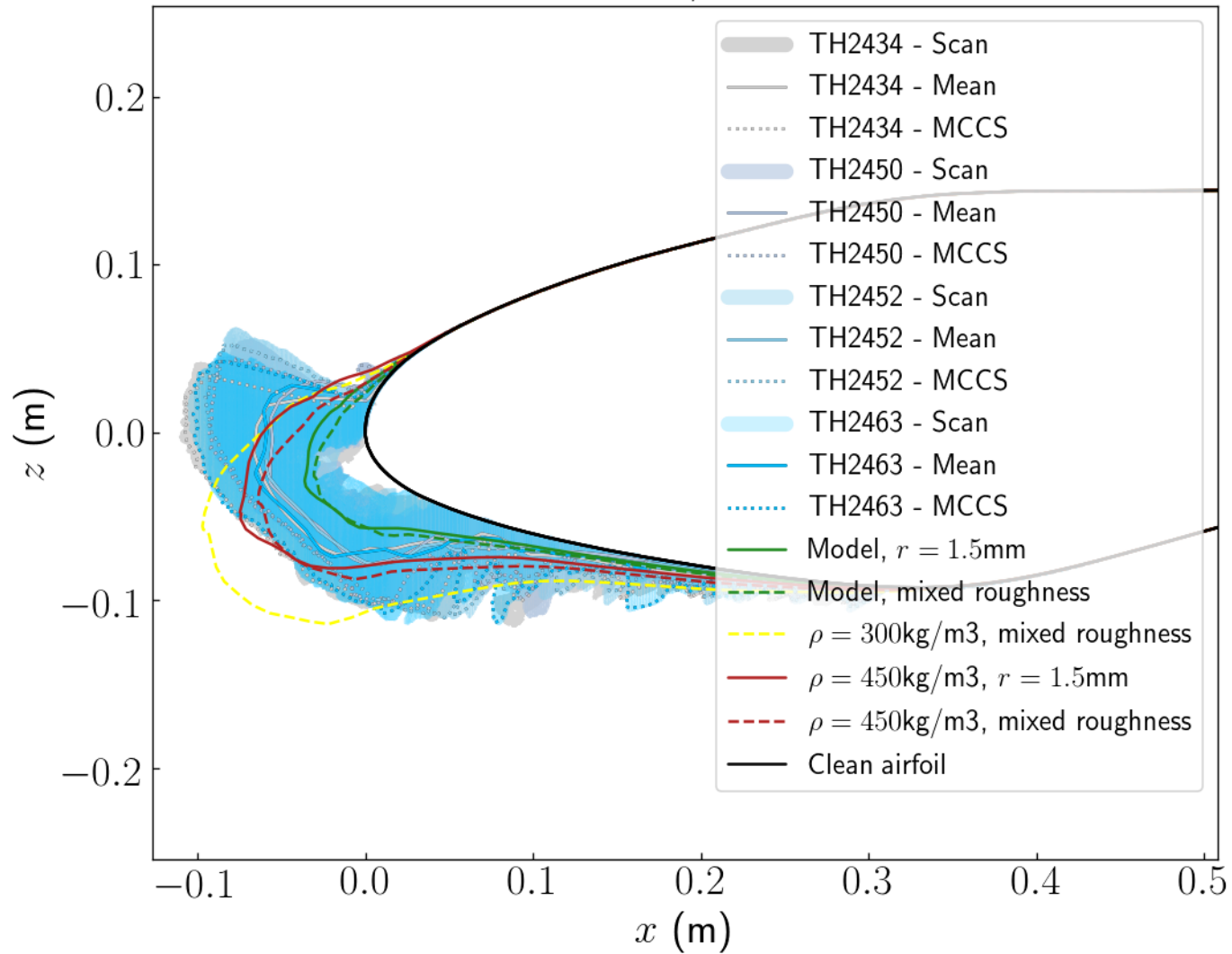
*E. Radenac and H. Gaible and H. Bézard and P. Reulet, IGLOO3D Computations of the Ice Accretion on Swept-Wings of the SUNSET2 Database, International Conference on Icing of Aircraft, Engines, and*



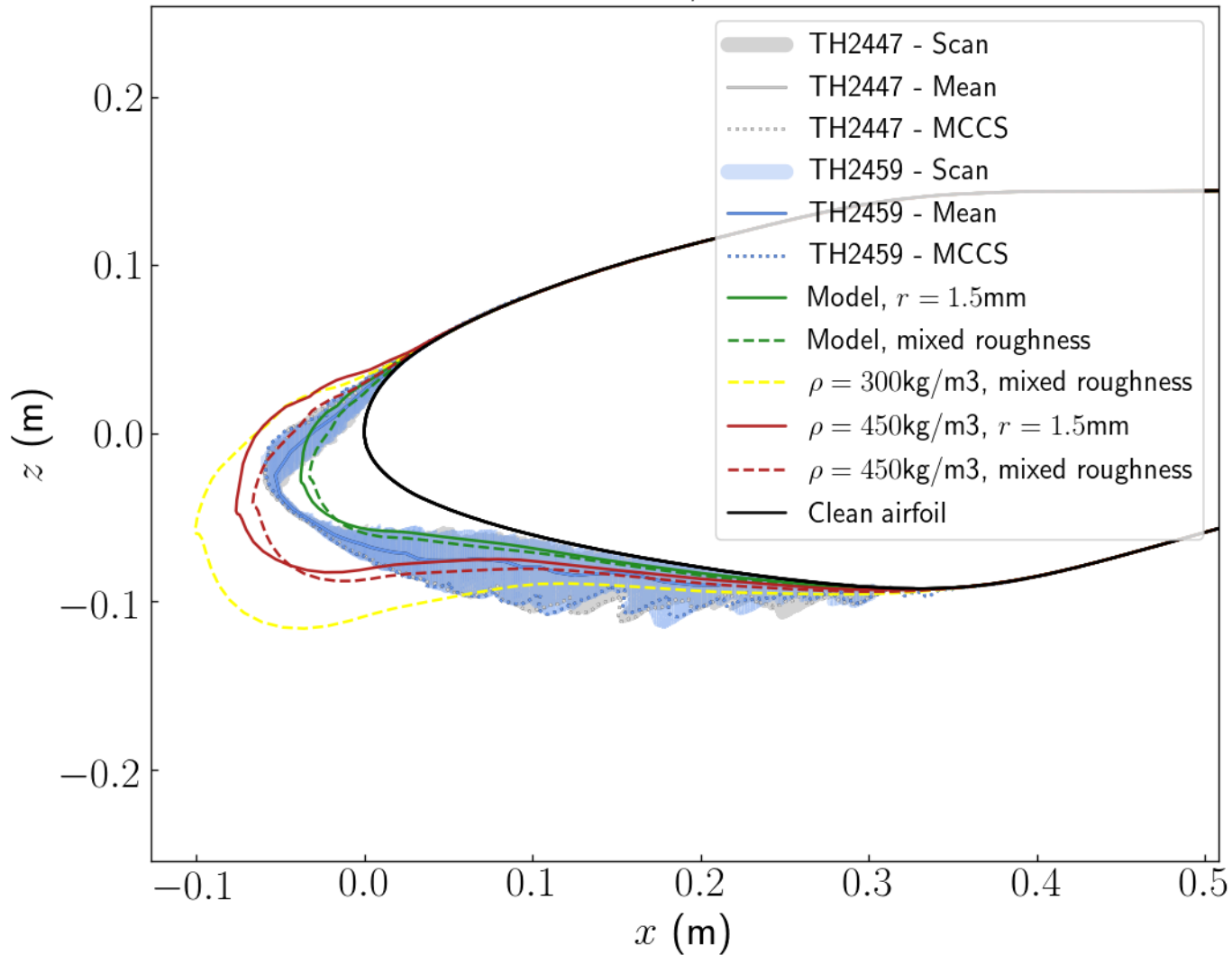
# MIDSPAN, CASE11



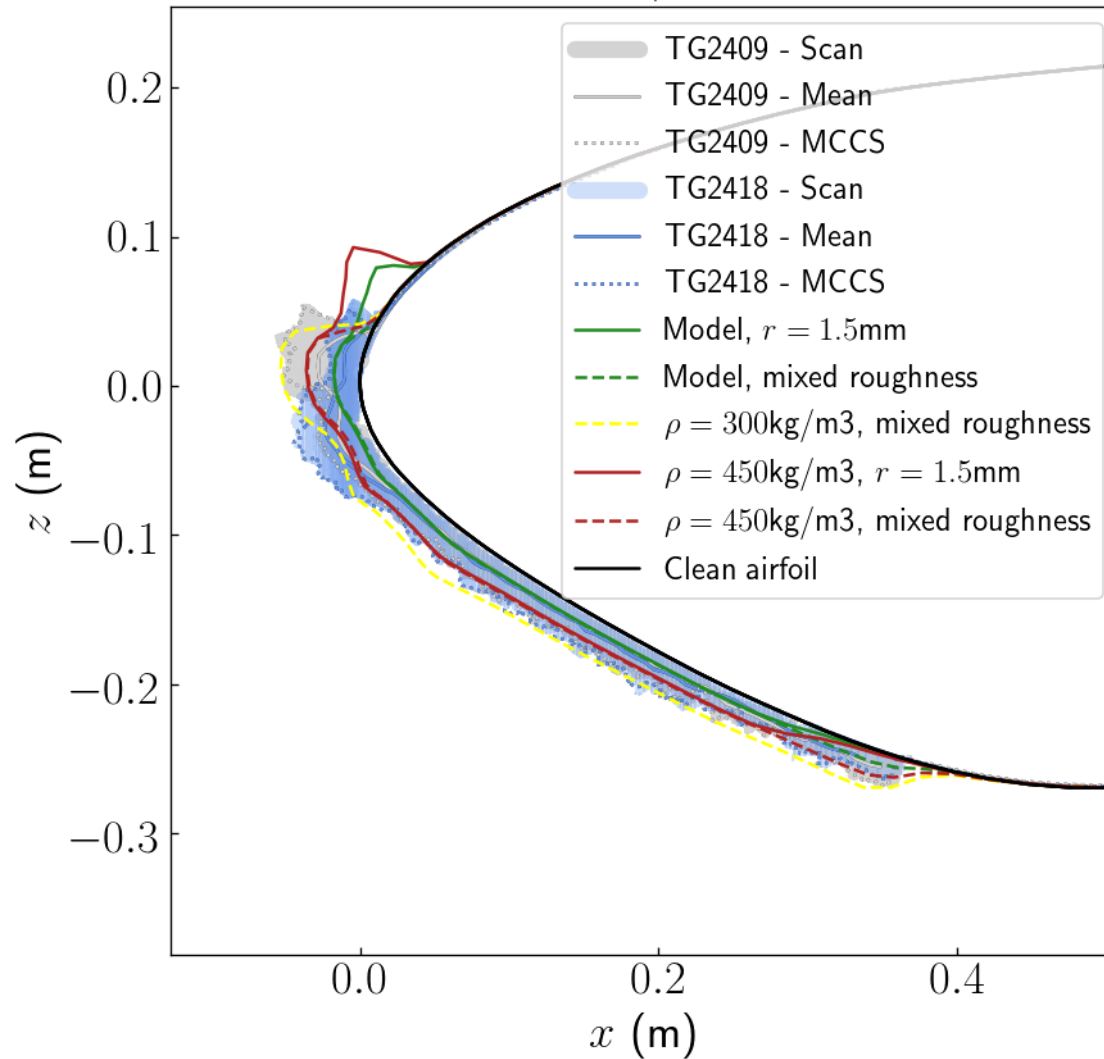
# MIDSPAN, CASE12



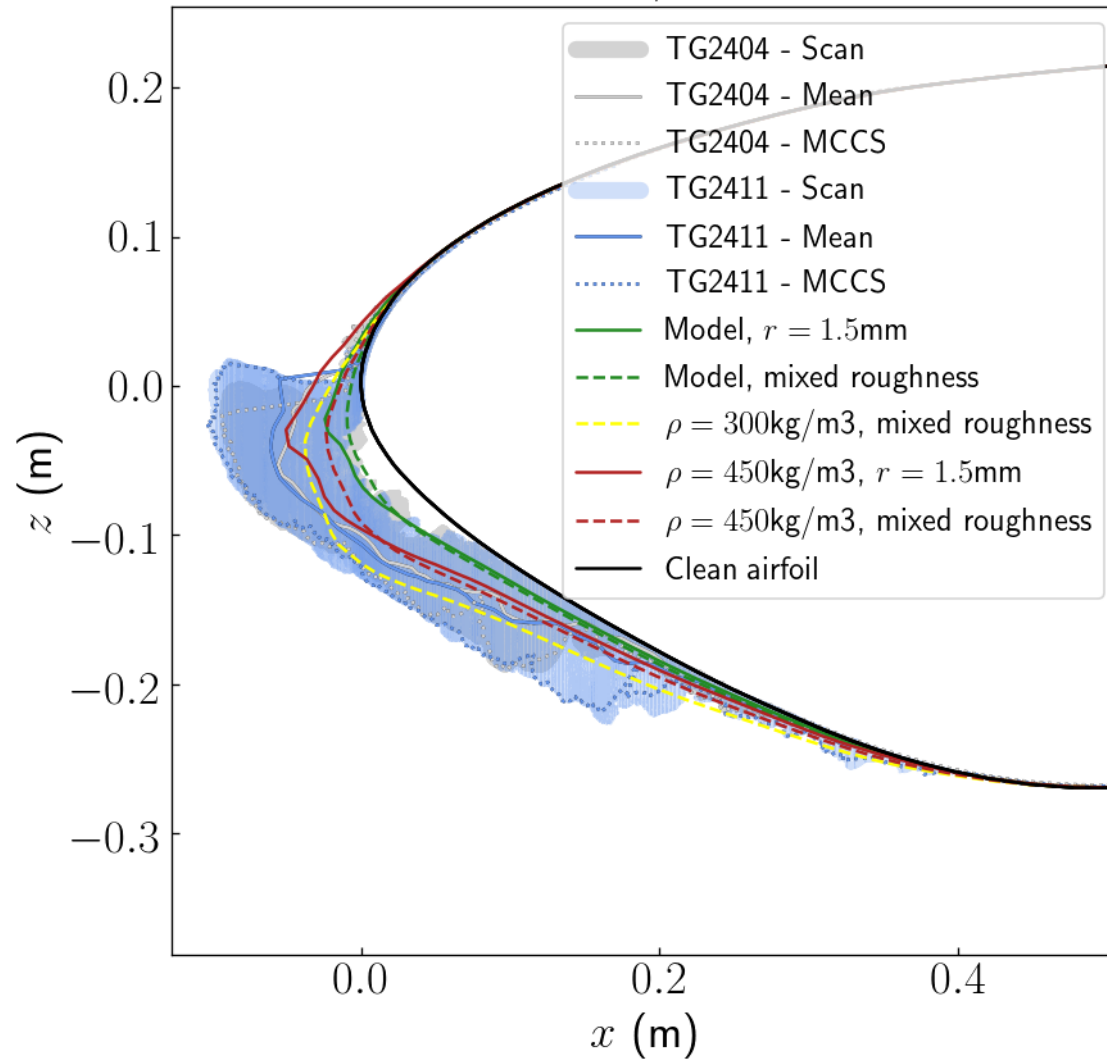
# MIDSPAN, CASE13



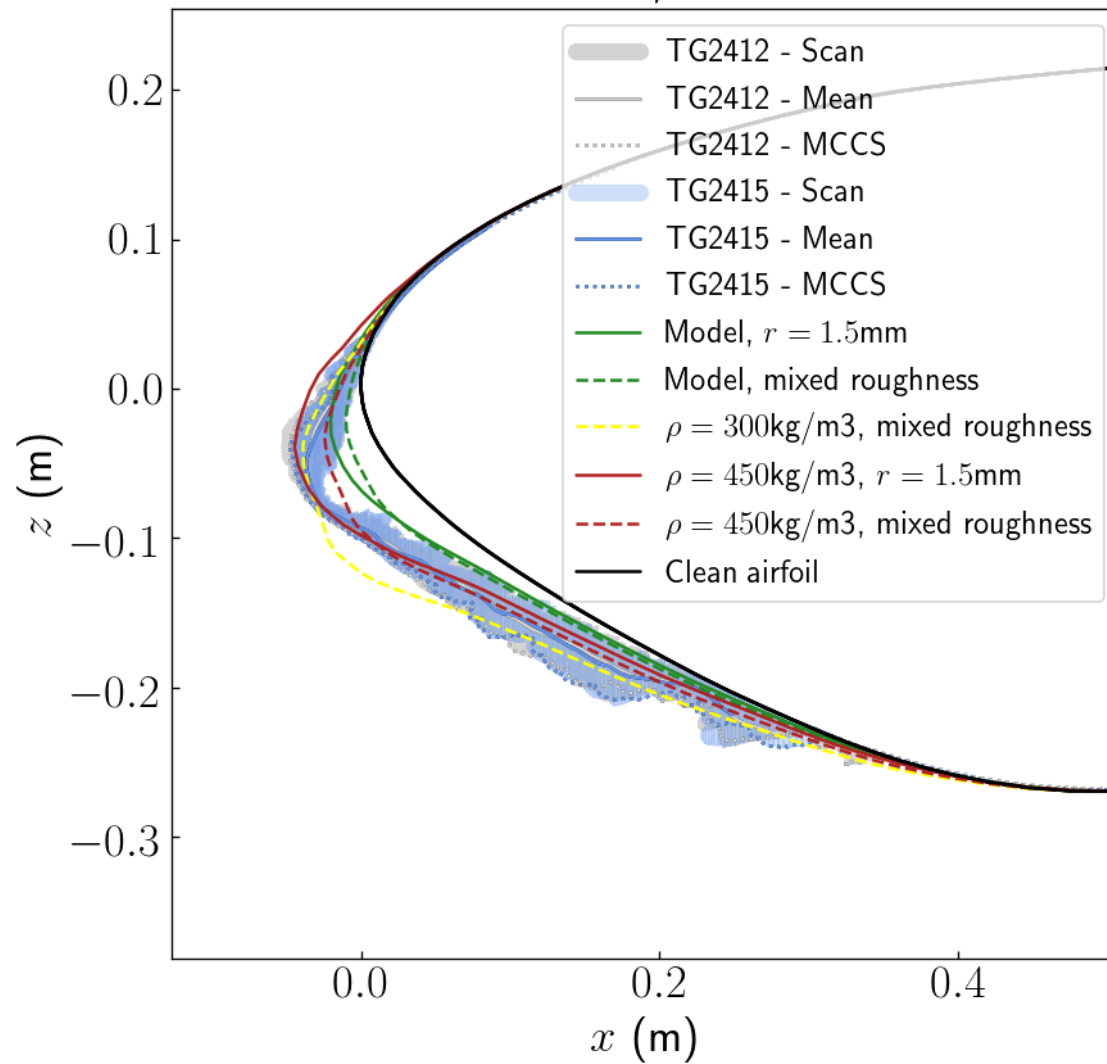
# INBOARD, CASE21



# INBOARD, CASE22

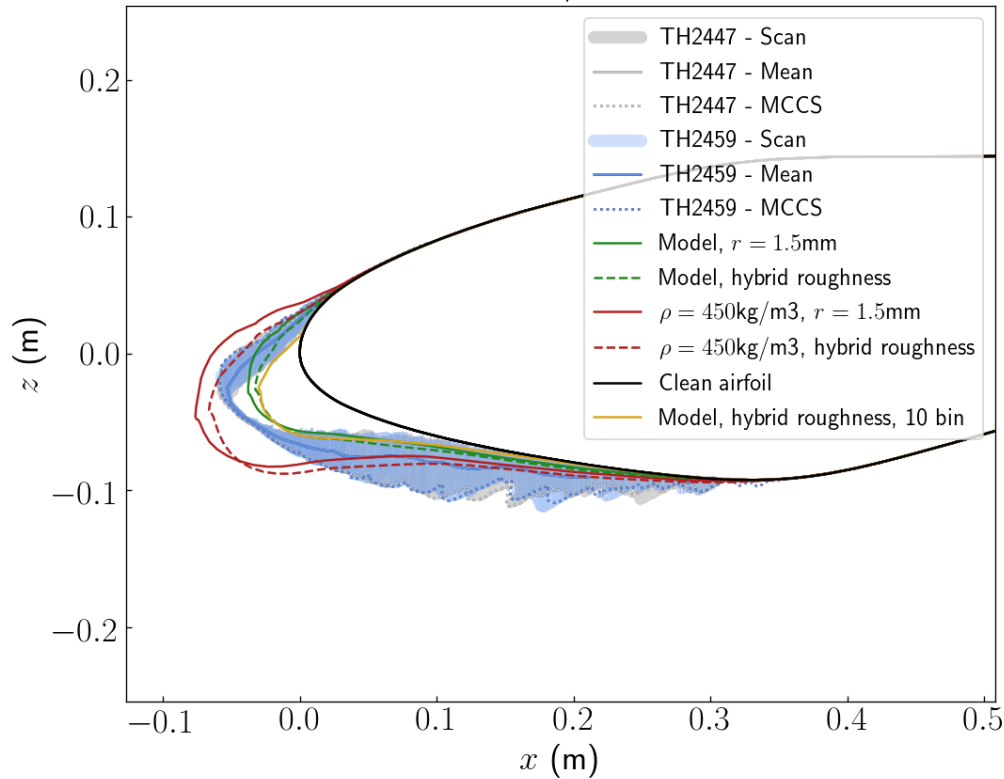


# INBOARD, CASE23



# Effect of the distribution

## MIDSPAN, CASE13



## INBOARD, CASE23

