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Safety Targets for Probabilistic Safety Analysis for Swiss Nuclear Power Plants

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Initial Condition

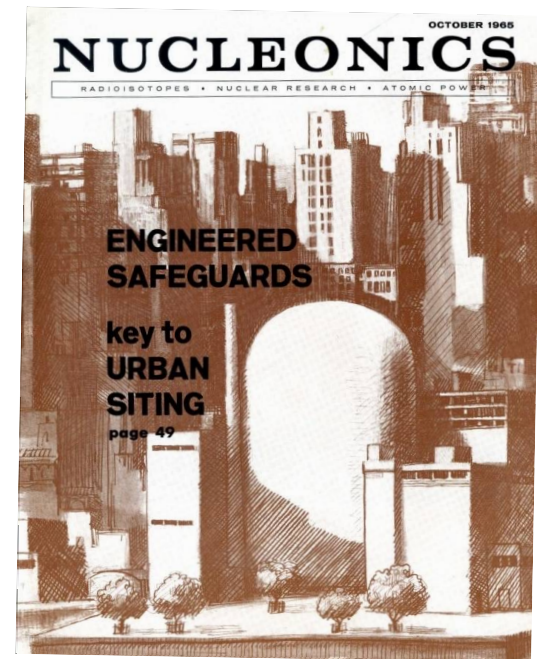
“The 1950s ... atom became a symbol of progress and benefit to humanity. ...” (Char & Csik 1987)



Hydrofoils glide across the oceans with nuclear power.

First safety consideration

- CP-1 (1942): Shutdown Systems (Safety Control Rod Axe Man - SCRAM)
- US Reactor Safeguards Committee required in 1950s: Placing for non-containment plants:
 $R = 0.016\sqrt{P_{th}}$ km
 P_{th} - thermal power in kilowatt



Early Accidents (mostly non-commercial Reactors)

- 12/12/52 Chalk river, Canada Test reactor NRX, Core Damage, Release
- 22/07/54 Steam Explosion of BORAX-Reactor NRTS
- 29/11/55 Idaho Falls, USA, EBR-1, Partial Core Melt
- 29/09/57 Kyshtym, USSR Waste storage, Chemical Explosion
- 24/05/58 Chalk river, Canada Test reactor NRU, Fuel rupture, Fire
- 25/10/58 Vinča, Yugoslavia Test, Reactor Criticality Excursion
- 26/07/59 Santa Susana Field Lab, Test Reactor SRE Excursion, Fuel Melt, Release
- 03/04/60 Waltz Mill, USA, Test reactor, Core Melt
- 03/01/61 Idaho Falls, USA, SL-1, Steam Explosion (**Rocket Mode**)
- 24/07/64 Rhode Island, USA, Fuel fabrication, Criticality Accident
- 05/10/66 Newport, USA Power reactor Unit 1 fast breeder, Fuel Assemblies Melted
- 01/05/67 Chapelcross, UK Power reactor Unit 2 Magnox, Fuel Element Melt, Fire
- 01/05/67 Chelyabinsk, USSR Fuel fabrication, Radionuclides Dispersal from Lake
- 21/01/69 Lucens, Switzerland Test reactor coolant loss, Excursion, Explosion
- 17/10/69 Saint Laurent, France reactor Unit A1 UNGG Partial (50kg U), Core Melt
- 26/05/71 Moscow, Russia Test facility SF-3 Kurchatov Institute, Fuel Rods fall out
- 26/09/73 Windscale, UK Reprocessing Shop B 204 Gas leakage, Contamination
- 06/02/74 Leningrad, USSR Power reactor Unit 1 RBMK-1000, Circuit Rupture
- 30/11/75 Leningrad, USSR Power reactor Unit 1 RBMK-1000, Core Melt, Release
- 01/01/77 Beloyarsk, USSR, Power reactor ABM-200 early RBMK Unit 2, Core Melt

Early PSAs

- WASH-740 (1957): Damage 10^{-2} - 10^{-4} , Release 10^{-5} - 10^{-6} per year
- WASH-1400 (1975) First Large Probabilistic Safety Assessment
- 1983 first full scope PSA Level 1 for Beznau NANO-Optimization
- Results showed high CDF
- Seismic improvement of cable Trays, electrical cabinets and masonry walls, additional DC train, emergency procedures
- 1987 PSA required by Regulator (Level 1 and 2): Gösgen, Leibstadt, Beznau (Mühleberg)

US-Studie zeigt: AKW Beznau 100mal unsicherer als Gösgen!

● Ältere Schweizer Atommeiler sollen jetzt durch Notbunker sicherer gemacht werden

ZÜRICH – Eine neue und noch geheime US-Risiko-Studie für das AKW Beznau zeigt, dass die älteren Werke Beznau und Mühleberg rund 100mal unsicherer sind als die moderneren von Gösgen und Leibstadt. Um die Sicherheitslücke etwas zu schliessen, sollen unter Mühleberg und Beznau Notbunker gebaut werden.

No: in Mühleberg wurde eine solche Risiko-Studie noch nicht einmal in Auftrag gegeben. Experten rechnen aber mit ähnlichen ungünstigen Werten wie für Beznau.

Die Sicherheitslücke zwischen Mühleberg und Beznau zuzunehmen sowie Gösgen und Leibstadt; andererseits soll jetzt teilweise geschlossen werden.

● Der unbemannte Notbunker

PSA-Model: Risks considered

Political Risks

Early Decommissioning

Economical Risks

Price drop

Counterfeit spare parts

Insolvent suppliers

Social Risks

Strike

Riots

Sabotage

Wave of resignations

Technical Risks

LOCA

Cooling system failure

pump failure

Human Risks

Incorrect Operation

Natural Risks

Seismic

Flood

Fire, Heat, Drought

Sturm, Hurricane

Cold, Ice, Snow, Hail

Solar Storms

IT-Risks

Health Risks

Pandemics

Epidemic



PSA-Model: Size

Full Power Model

212 Initiating Events

1,200 Random Variables

1,800 Components

7,000 Basic Events

310 Top Events

> 25 Event Trees

> 10^{40} Accident Sequences

> 600 Fault Trees

Computation Time: Hours/Day

10,000 pages

Low Power and Shut Down Model

212 Initiating Events

1,400 Random Variables

1,800 Components

3,500 Basic Events

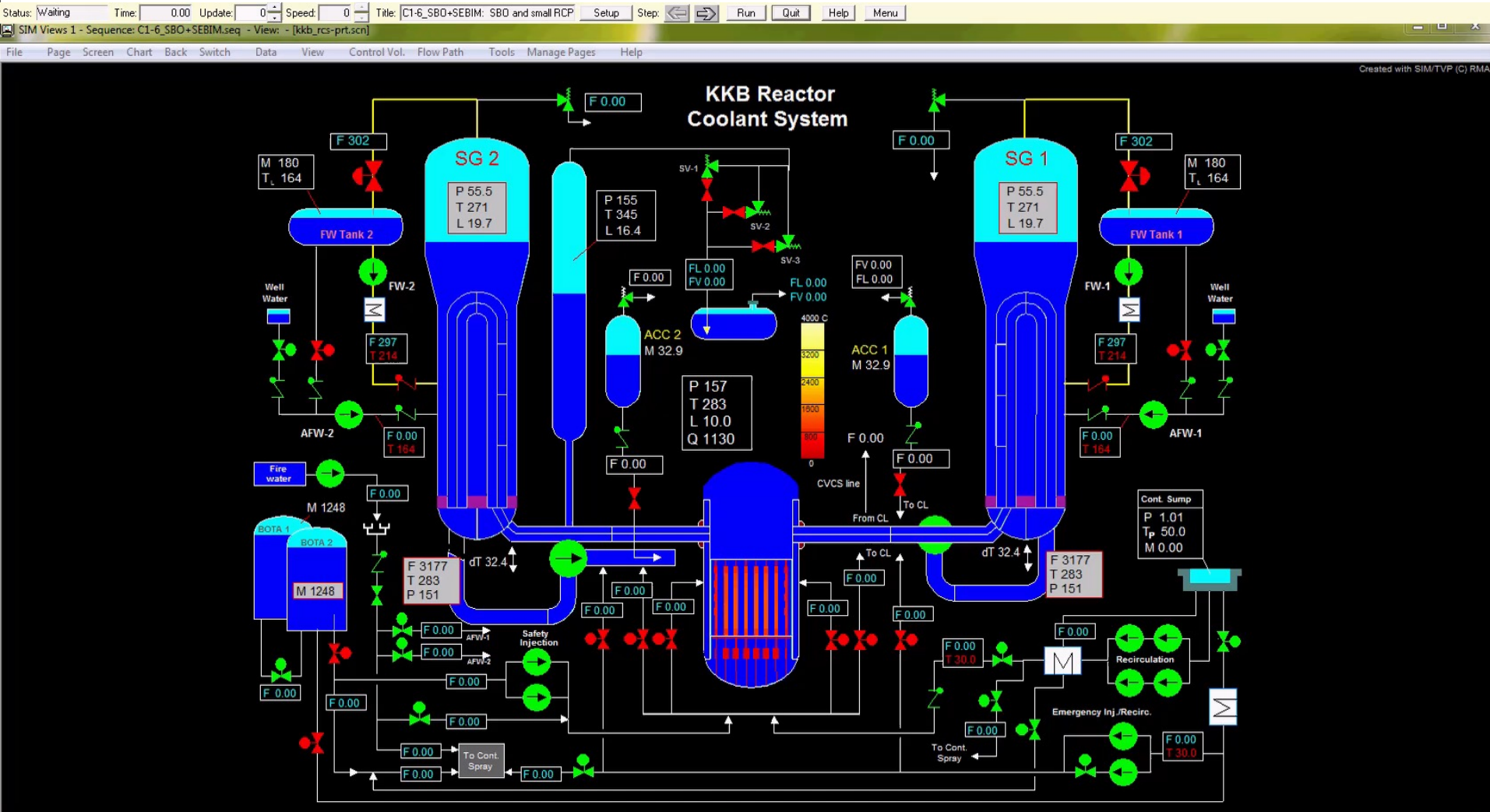
310 Top Events

20 Event Trees

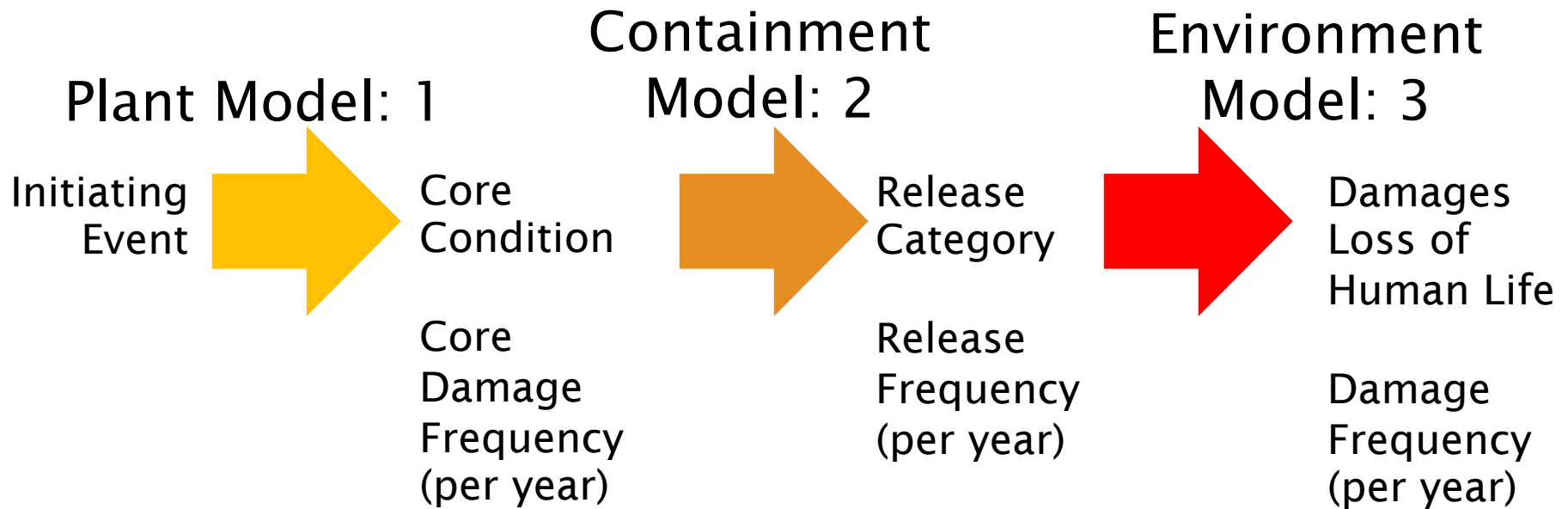
> 500 Fault Trees

Computation Time: Days/Weeks

PSA-Model: Deterministic Computations



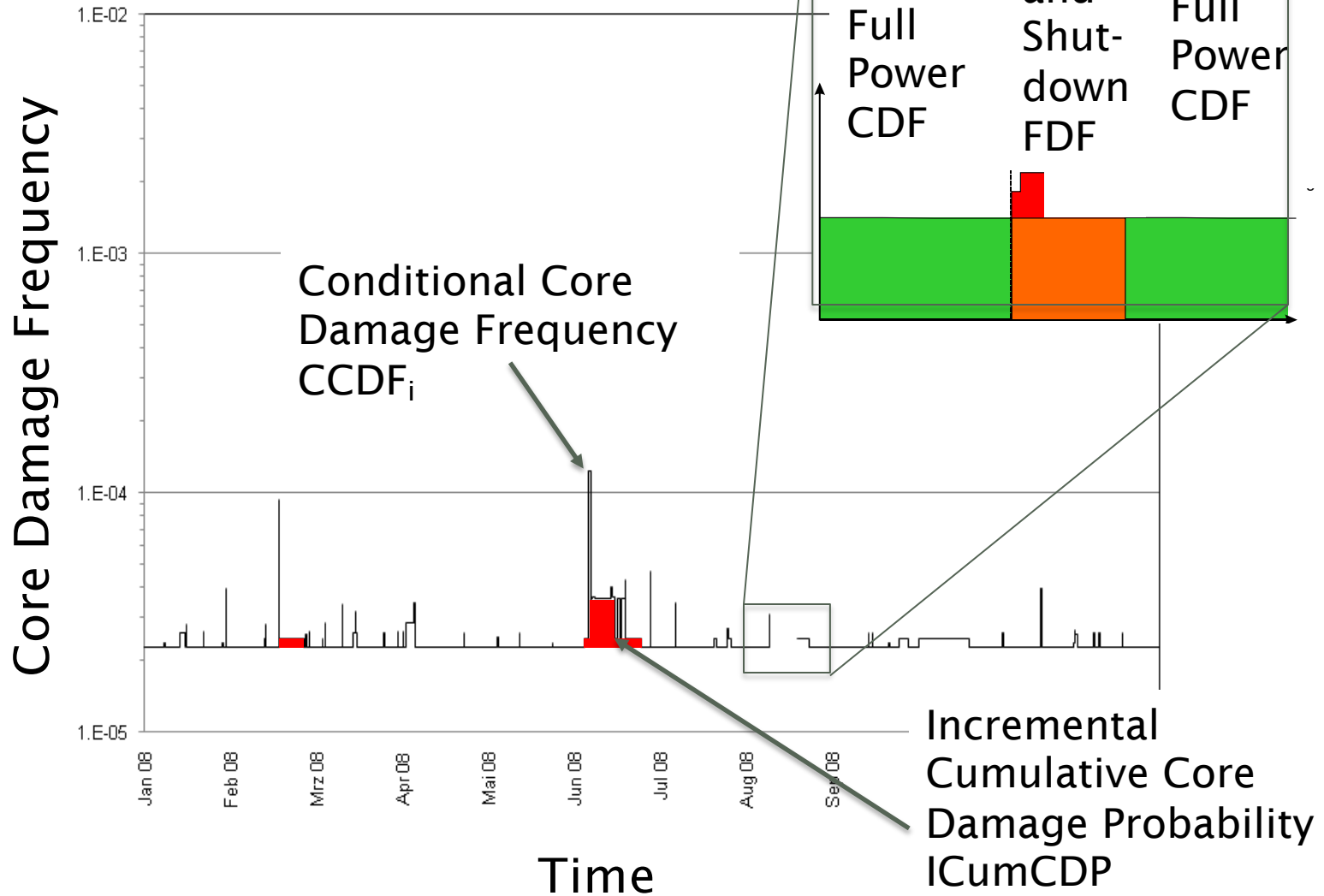
PSA-Model: Levels



Definition of Core Damage (Level 1)

- Maximum fuel rod temperature $>1,200^{\circ}$ C
- Overall oxidation of fuel rod >17 % of the fuel rod wall thickness
- Hydrogen production >1 % of the theoretically possible hydrogen
- Significant Change of Core
- Loss of Core Cooling

CDF over a Year



Int. Target Values

- USNRC (1982)
NUREG-0880:
CDF: 10^{-4} per year
- IAEA (1988) 75 INSAG-3:
CDF: 10^{-4} ... 10^{-5}
LRF/LERF: 10^{-5} ... 10^{-6}
(order of magnitude)

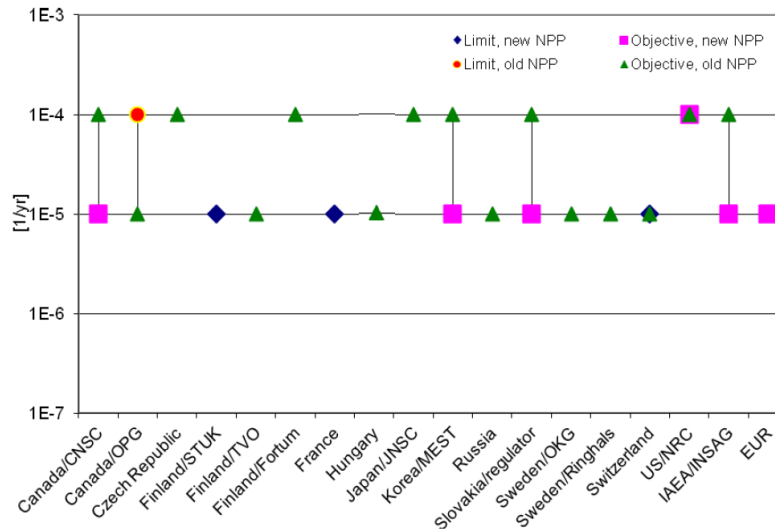


Figure 3 Numerical criteria defined for Core Damage.

Table 1: Core Damage Frequency from Various Country [5,6]

Country	Organization	Frequency	Notes
USA	Regulator	10^{-4} /yr	Objective
UK	Regulator	10^{-4} /yr	Limit
		10^{-5} /yr	Objective
Taiwan	Licensee	10^{-5} /yr	Limit
Switzerland	Regulator	10^{-4} /yr	Limit for existing plants
		10^{-5} /yr	Objective for new plants
Sweden	Licensee	10^{-5} /yr	Objective: This is a criteria or safety goal established by the licensees.
Slovak Rep	Regulator	10^{-4} /yr	Objective for existing plants
		10^{-5} /yr	Objective for new build
Netherlands	Regulator	10^{-4} /yr	Limit for existing plants
		10^{-6} /yr	Limit for new plants
Japan	Regulator	10^{-4} /yr	Objective
Italy	Regulator	10^{-6} to 10^{-5} /yr	Objective
Hungary	Regulator	10^{-4} /yr	Limit for existing plants
		10^{-5} /yr	Limit for new plants
France	Regulator	10^{-5} /yr	Objective for new plants
France/ Germany	Designers of EPR	10^{-6} /yr	Objective
Finland	Regulator	10^{-5} /yr	Objective
Czech Rep	Licensee	10^{-4} /yr	Objective for existing plants
		10^{-5} /yr	Objective for new plants
Canada	Regulator	10^{-5} /yr	Limit for new plants
	Licensee	10^{-4} /yr	Limit for existing plants
		10^{-5} /yr	Objective for existing plants
Korea	Regulator	10^{-5} /yr	plants
Slovenia	Regulator	10^{-5} /yr	Objective for new build

Isnaeni 2021,
Bengtsson et al. 2010,
Gu 2018

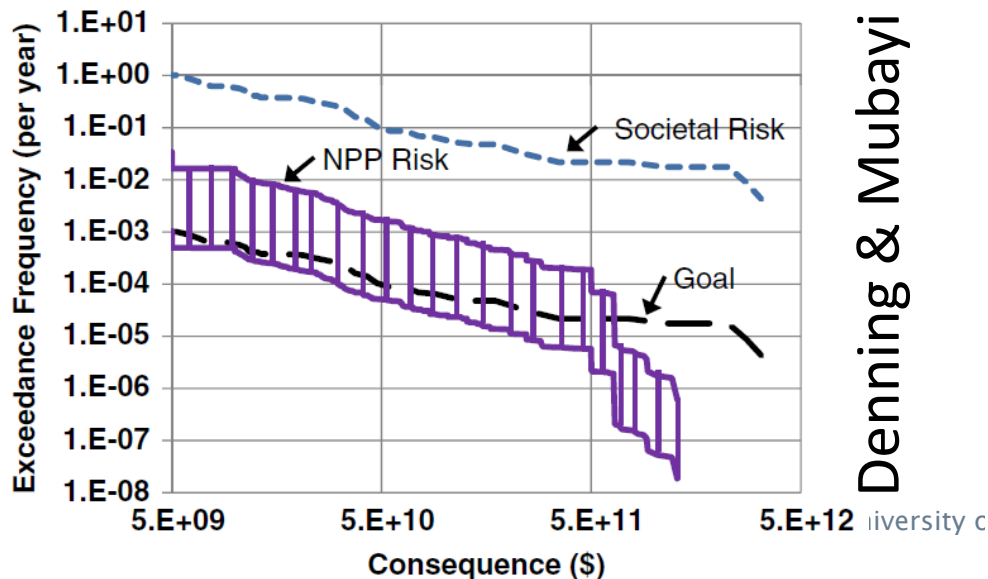
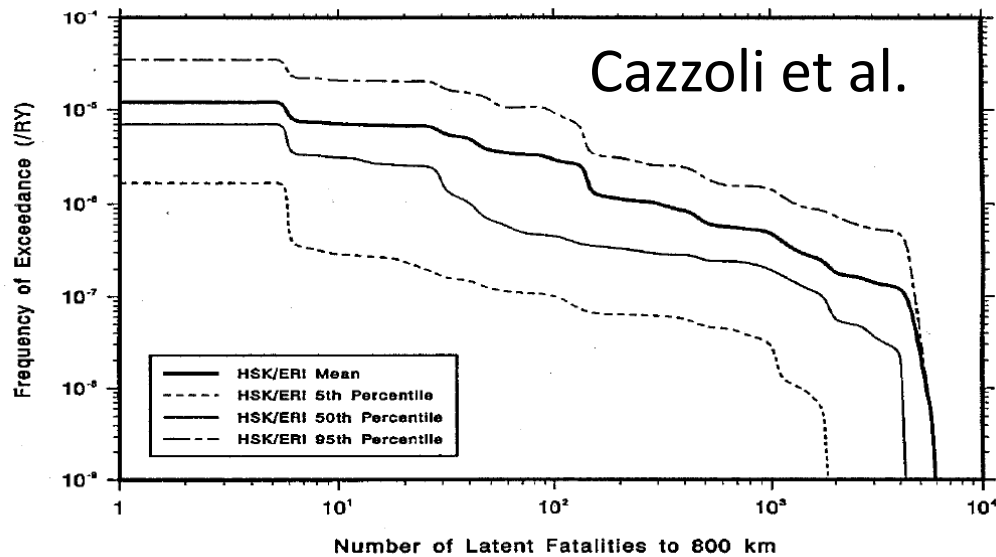
Swiss Target Values (Level 1 and 2)

- Regulated by Law and Ordinance (ENSI A06, UVEK-DETEC)
- CDF $> 10^{-5}$ per year, measures must be taken, if appropriate.
- LERF $> 10^{-6}$ per year, measures must be taken, if appropriate.
- CDF $> 10^{-4}$ per year, **immediate** measures must be taken
- Initiating event ... contributes $> 60\%$ to the mean CDF and contribution $> 6 \times 10^{-6}$ per year, measures must be taken, if appropriate.
- Design basis accident shall ... assess hazards with a frequency $\geq 10^{-4}$ per year for demonstration of adequate protection (HCLFP = 1 % fractile)...

Swiss Target Values (Risk based Maintenance)

- $CDF_{\text{Mean}}/CDF_{\text{Baseline}} > 1.2$, measures ... be taken, if appropriate
- No maintenance-related Conditional Core Damage Frequency per component unavailability configuration $> 10^{-4}$ per year
- Total component maintenance times per calendar year are limited: maintenance-related part of the Incremental Cumulative Core Damage Probability (ICumCDP) $< 5 \times 10^{-7}$.
- Safety-relevant components: $FV \geq 10^{-3}$ and $RAW \geq 2$
- INES classification of events using ICCDP

Target Values: Level 3



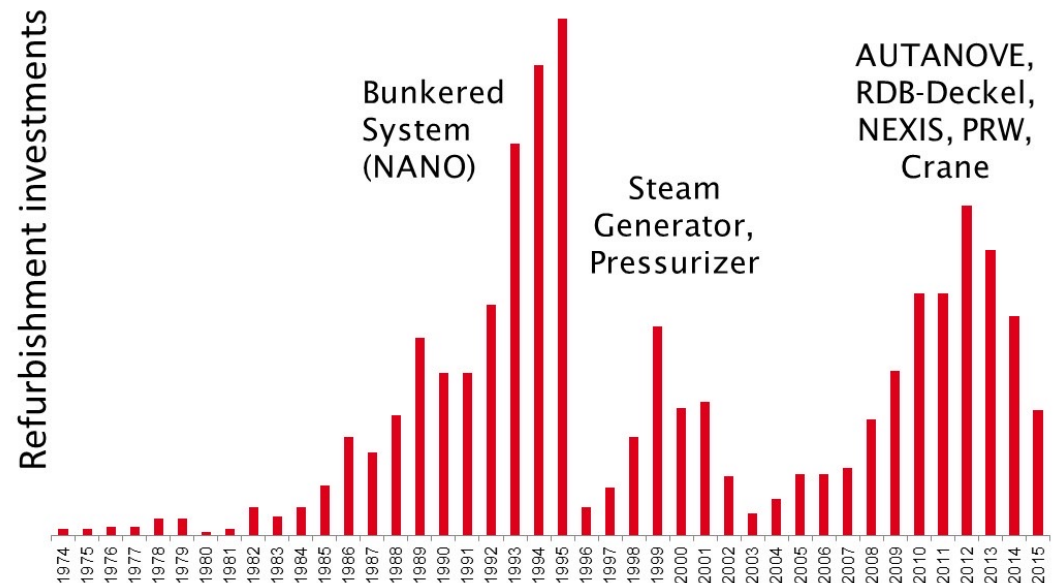
Origin of Target Values (1982)

- risk to individual should < 0.1 % of the sum of fatality risks from other accidents
- should < 0.1 % of the sum of cancer fatality risks resulting from other causes
- UVEK: Deterministic proofs related to safety levels based on Dose (**very important**)
 Event 10^{-3} : 1 mSv
 Event 10^{-4} : 100 mSv

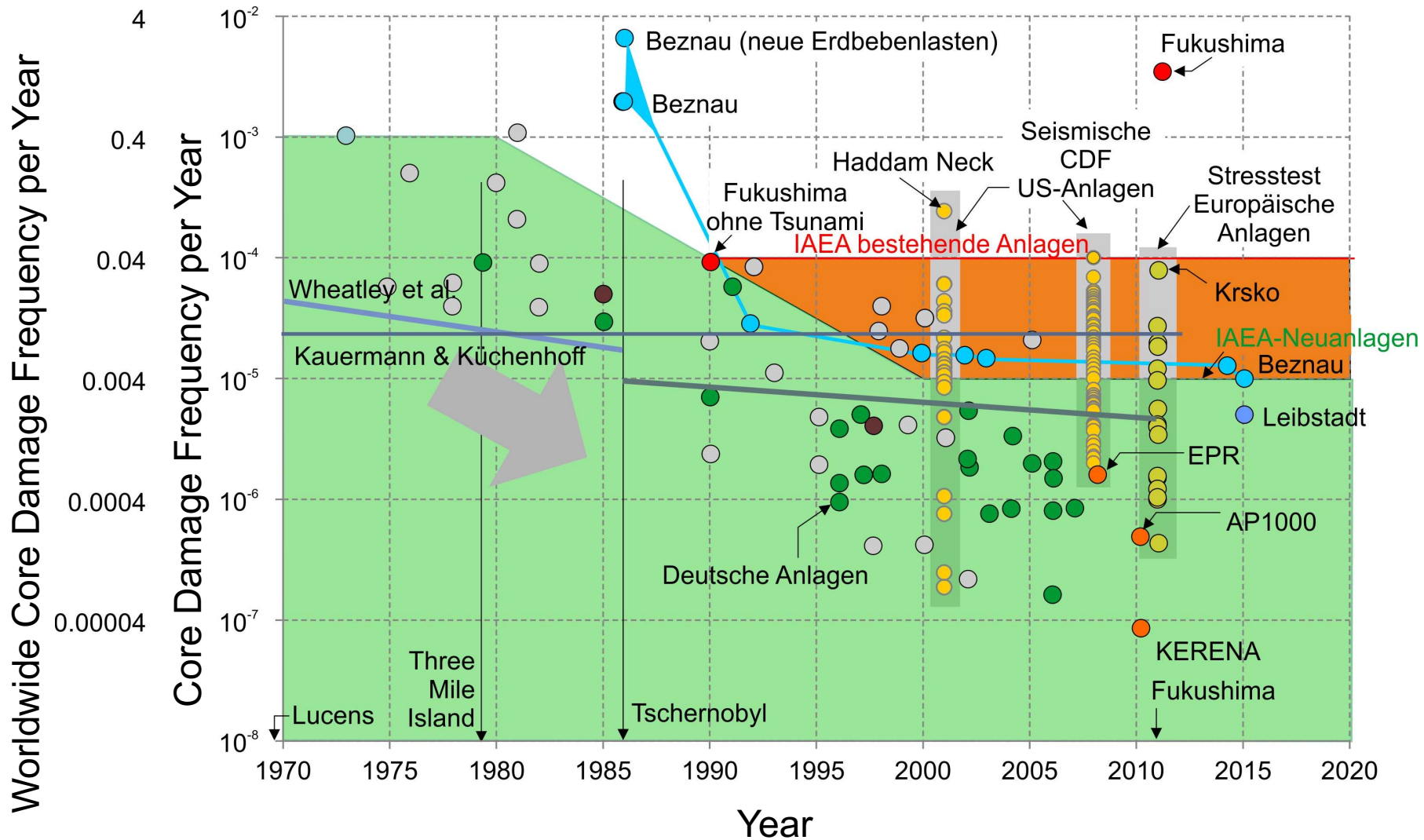
LQI Backwards Calculation and Refurbishment

- *LQI*: Backwards calculation of NANO: about 1 billion CHF
- *LQI*: Backwards calculation of AUTANOVE: < 100 Mill. CHF, but 700 Mill. CHF invested
- One can improve old plants only to a limited extend.
- No good solution keeping old plants running when official decommission dates

- Overall, 3,000 plant improvements



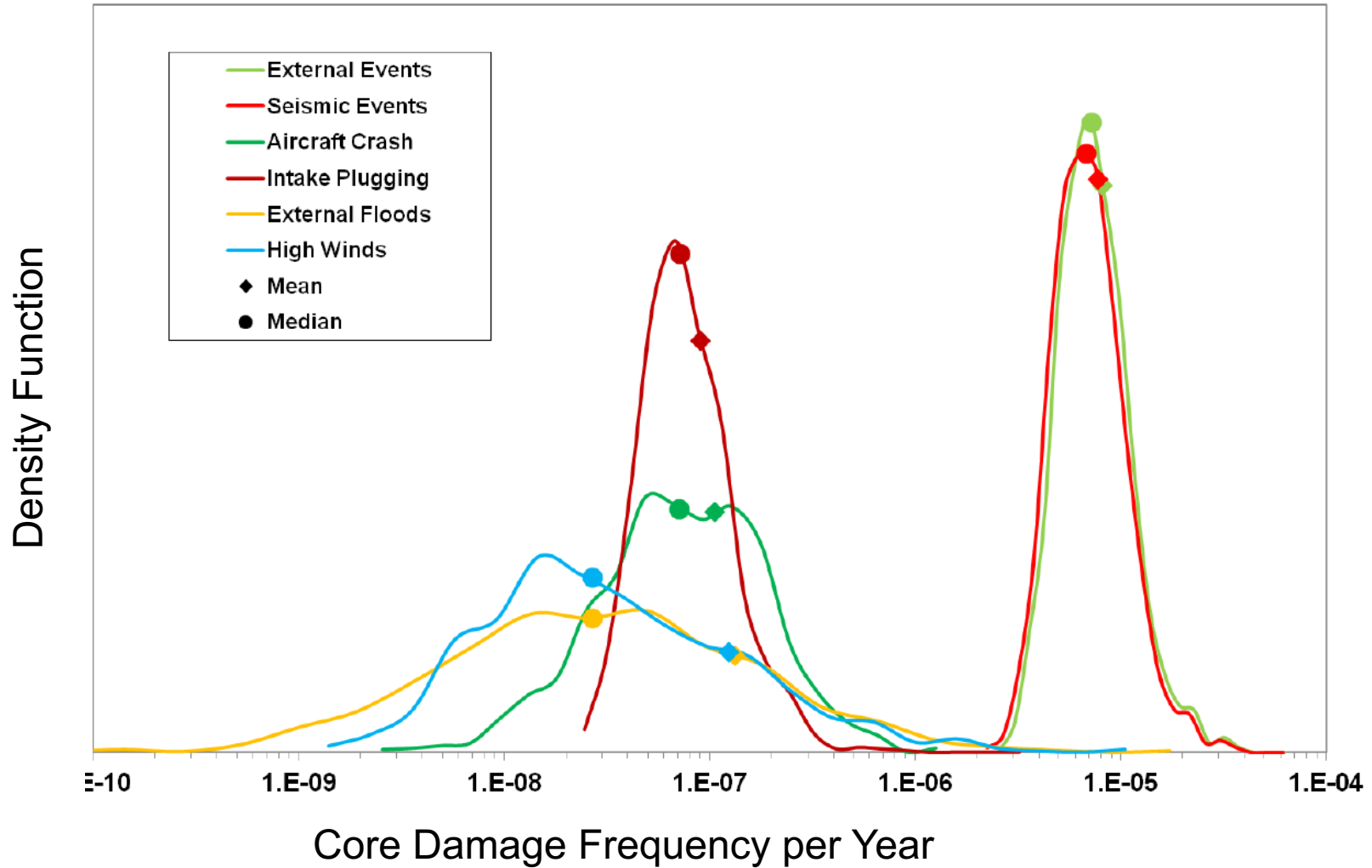
PSA-Models: Results and Backwards Calculation



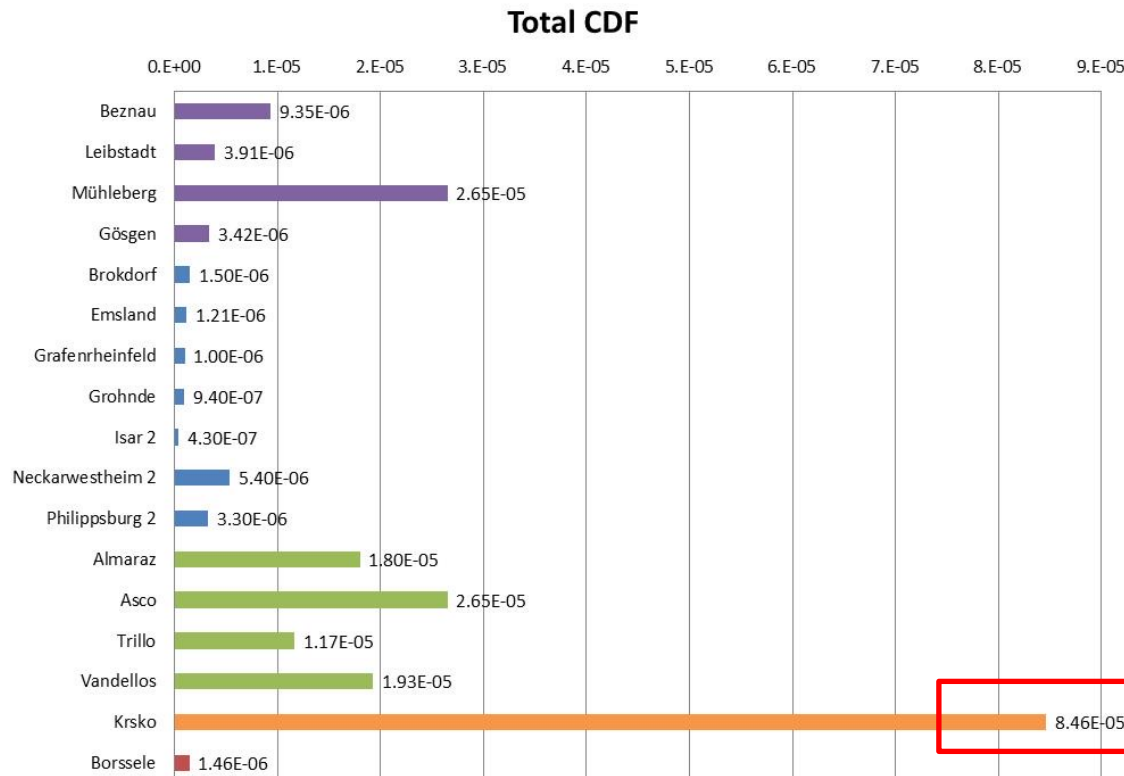
Conclusion

- Early design far too weak (much too optimistic, political will)
- Global annual CDF in 1970s close to 1 (backwards calc.)
- Improvement in PSA results (> two orders of mag. per century)
- Some strong critic against PSA (multi unit sites, correlation, cutoff, importance factors): “*Given the degree of uncertainty and complexity ... to ... nuclear risk assessment... risk-based probabilistic assessment has proven very limited.*” (Dorfman et al. 2013) – I do not agree!
- Large Uncertainty in some Initiating Events (seismic, floods)
- Deterministic Proofs and Safety Margins became more important (shutdown of plant)
- Defense in Depth, Barriers Concept, Continuous Improvement
- Just one Element in Decision Making

Uncertainty



Core Damage Frequency

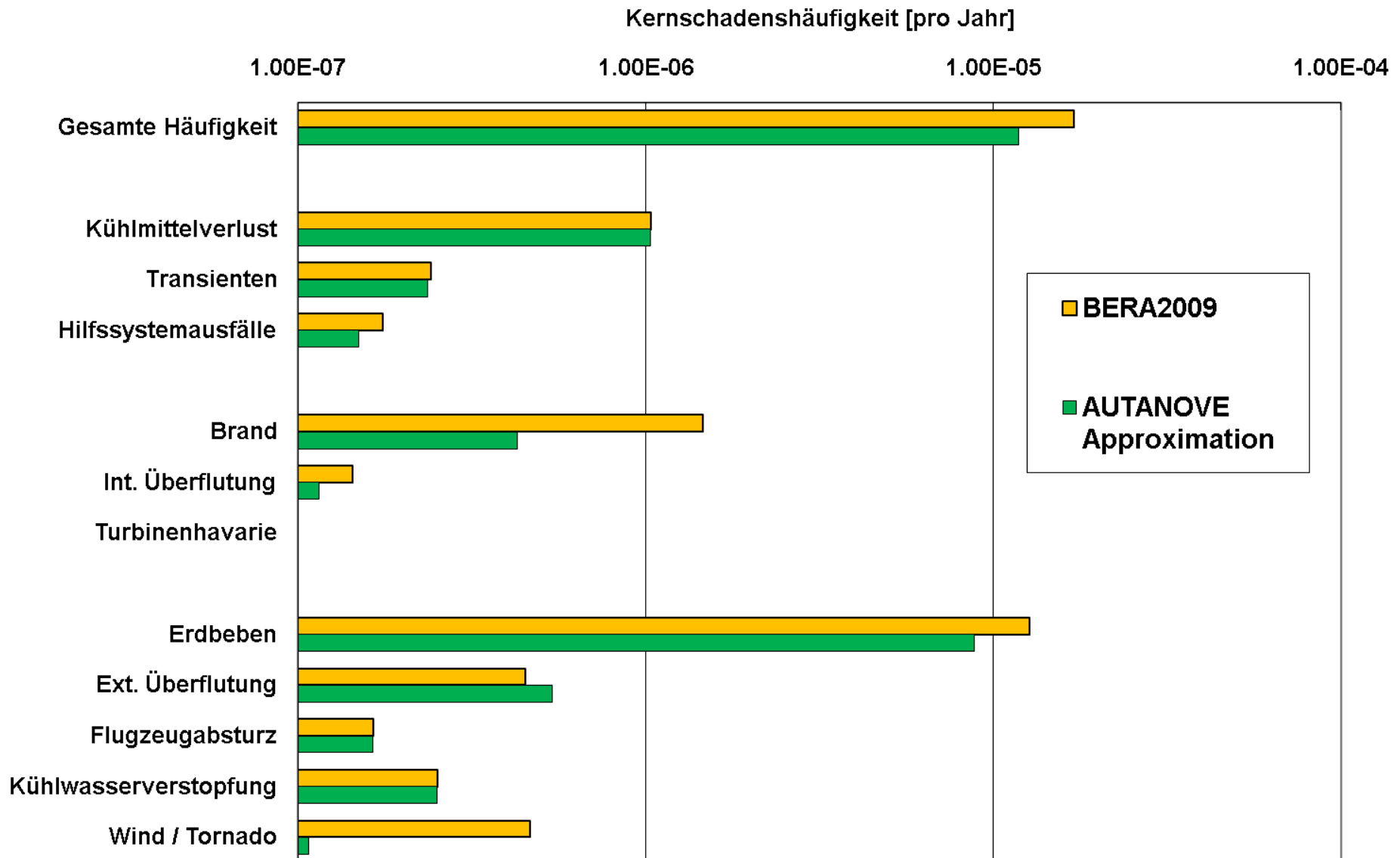


Plants Performing ≤ 2 from NUREG 1742

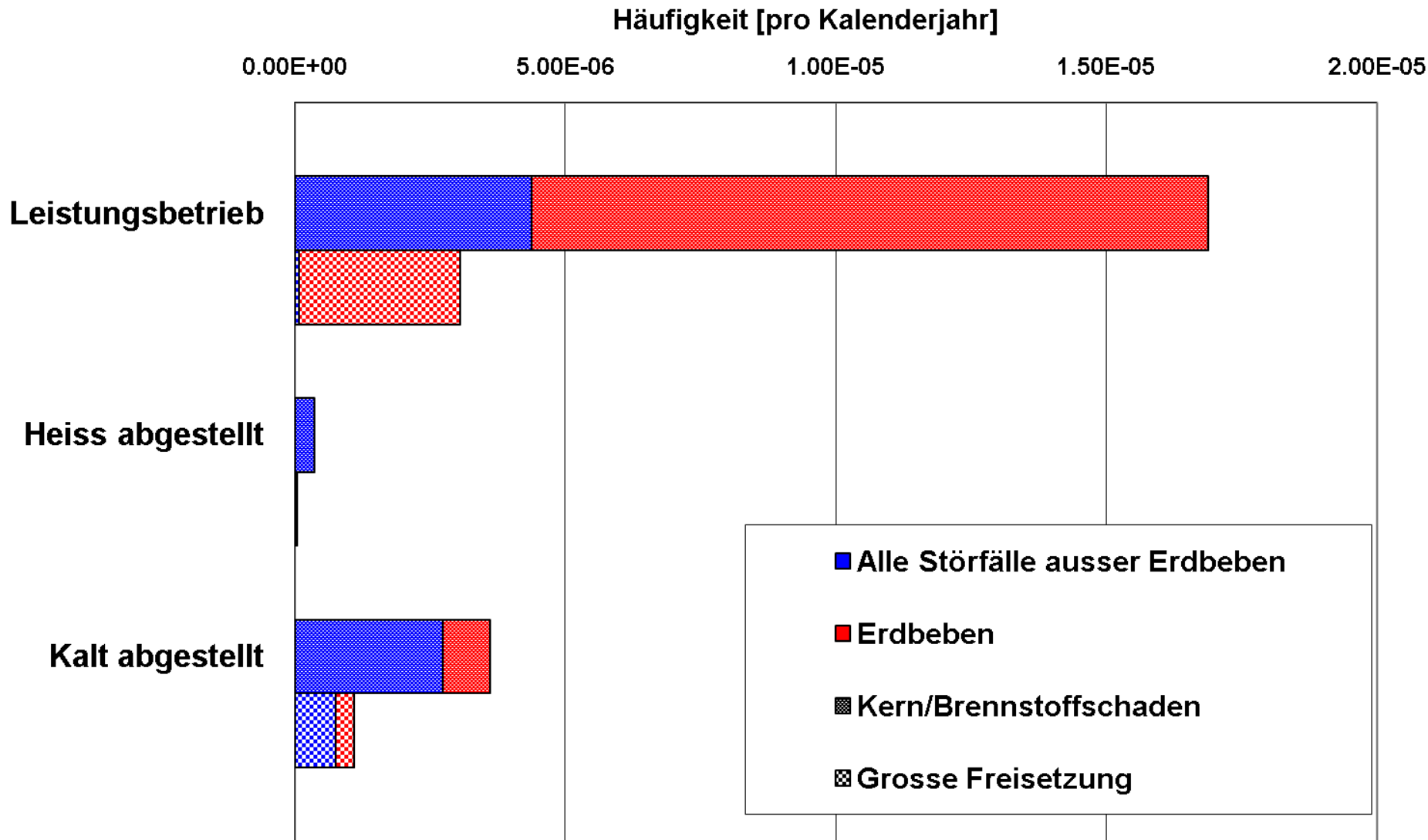
Beaver Valley 2	1.03E-05	Pilgrim 1	5.80E-05
Kewaunee	1.10E-05	Indian Point 3	5.90E-05
McGuire 1 & 2	1.10E-05	Haddam Neck	2.30E-04
Seabrook	1.20E-05		

Median of Mean Seismic CDF Value (EPRI Results)	1.20E-05
Mean of Mean Seismic CDF Value (EPRI Results)	2.50E-05

Core Damage Frequency



Core Damage Frequency



Core Damage Frequency

Importance Measure

Measure	Abbreviation	Principle
Risk reduction	RR	$R(\text{base}) - R(x_i = 0)$
Fussell–Vesely	FV	$\frac{R(\text{base}) - R(x_i = 0)}{R(\text{base})}$
Risk reduction worth	RRW	$\frac{R(\text{base})}{R(x_i = 0)}$
Criticality importance	CR	$\frac{R(x_i = 1) - R(x_i = 0)}{R(\text{base})} \times x_i(\text{base})$
Risk achievement	RA	$R(x_i = 1) - R(\text{base})$
Risk achievement worth	RAW	$\frac{R(x_i = 1)}{R(\text{base})}$
Partial derivative	PD	$\frac{R(x_i + \partial x_i) - R(x_i)}{\partial x_i}$
Birnbaum importance	BI	$R(x_i = 1) - R(x_i = 0)$

Level 3

Gauss'sches Fahnen-Modell

$$C(x, y, z) = \frac{Q'}{2\pi\sigma_y\sigma_z u} \cdot \exp\left(-\frac{y^2}{2\sigma_y^2}\right) \cdot \left(\exp\left(-\frac{(z-h)^2}{2\sigma_z^2}\right) + \exp\left(-\frac{(z+h)^2}{2\sigma_z^2}\right)\right)$$

$C(x, y, z)$ = Immissionskonzentration am betrachteten Ort

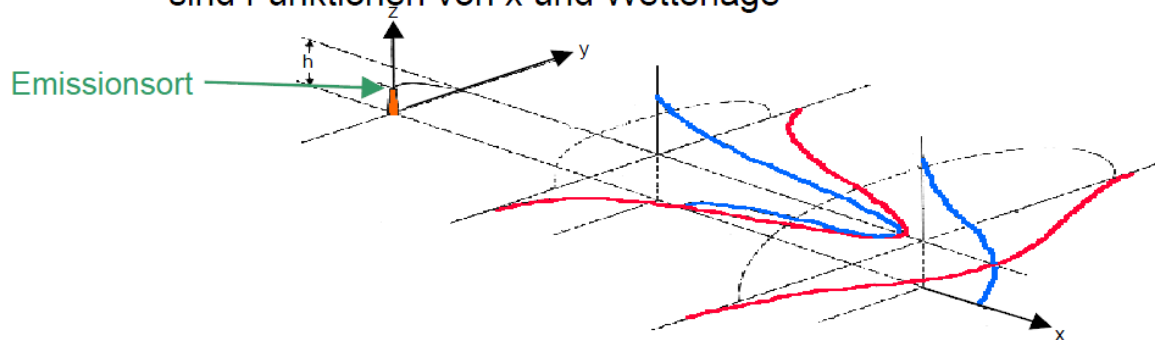
Q' = Emissionsrate, d.h. pro Zeiteinheit freigesetzte Schadstoffmenge

u = gemittelte Geschwindigkeit

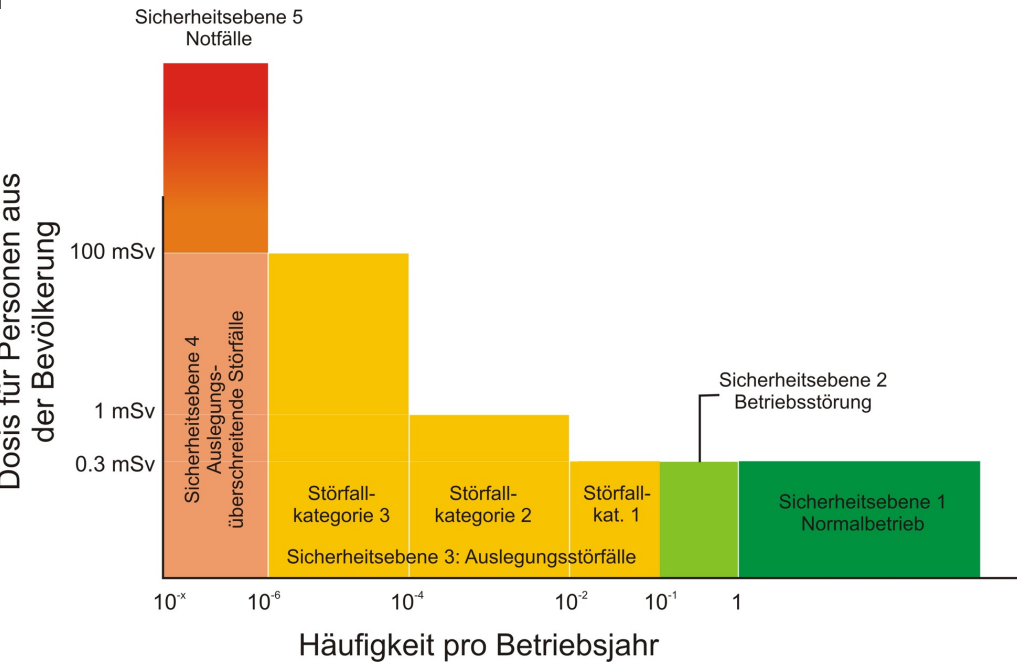
h = effektive Quellenhöhe

x, y, z = Abstände des Bezugspunktes vom Koordinatenursprung, wobei x der Windrichtung entspricht

σ_y, σ_z = Streuparameter der Konzentrationsverteilung in y - bzw. z -Richtung sind Funktionen von x und Wetterlage



Safety Level



Growth of NPPs

Nuclear power growth: 1951–86

Year	Construction starts		Connections to the grid	
	Units	GWe	Units	GWe
1951	1			
1952				
1953	2	0.1		
1954	6	0.5	1	
1955	3	0.1		
1956	9	0.8	1	0.1
1957	12	1.5	1	0.1
1958	7	0.6	3	0.2
1959	6	0.9	5	0.3
1960	10	1.0	6	0.6
1961	6	1.1	2	0.1
1962	8	1.3	10	1.0
1963	5	1.4	7	0.4
1964	10	3.0	8	1.1
1965	10	3.5	9	1.6
1966	16	7.4	8	1.2
1967	23	15.2	10	2.1
1968	38	26.1	6	1.1
1969	17	12.7	11	3.5
1970	37	24.9	6	3.3
1971	22	16.1	16	7.3
1972	22	19.3	16	8.8
1973	23	18.3	20	12.5
1974	35	29.8	26	16.9
1975	40	38.0	15	10.2
1976	29	27.2	19	14.1
1977	15	14.5	18	13.3
1978	21	18.2	20	15.8
1979	21	19.7	8	7.0
1980	23	21.4	21	15.3
1981	19	11.6	23	20.4