

Department of Chemical Engineering

Examination paper for TKP 4140 – Process Control

Academic contact during examination: Sigurd Skogestad Phone: 91371669

Examination date: 06 December 2017 Examination time (from-to): 09:00 – 13:00 Permitted examination support material: One (1) A4 double-sided piece of paper with your handwritten notes. Standard calculator.

Other information: State clearly all assumptions you make. You may answer in Norwegian or English

Language: English Number of pages (front page excluded): 4 (including Bode paper which may be handed in)

Informasjon om trykking av eksamensoppgave	
Originalen er:	
1-sidig	
sort/hvit □ farger □	
skal ha flervalgskjema 🗆	

Checked by:

Date

Signature

Problem 1 - Mixing process (30%)



Note that the three parts of this problem can be done independently.

Two mixing tanks are used to produce a diluted acid (q_2) from concentrated acid (q_A) and water $(q_{w1} \text{ and } q_{w2})$, (see figure). The main part of the dilution is done in tank 1, while tank 2 is used to fine tune the dilution to obtain the desired concentration $(q_{w1} \text{ is about } 10x q_{w2})$.

- (a) Write a dynamic model for the process (two balances for each tank). You may need to introduce symbols (variables) in addition to the ones given on the figure. No linearization or Laplace is required.
- (b) Formulate the 2x3 transfer matrix G₁ for the first tank with q_A, q_{w1} and q₁ as independent variables (inputs or disturbances) and V₁ and c₁ as dependent variables (outputs). No numbers are required, just the form (first-order, integrating, etc.) and sign of the gain.

(c) Now we consider control. The flow of dilute acid is set by the downstream process, so q_2 is a disturbance. Suggest a control structure on the flowsheet for each of the following two cases:

1) Measurements are c_1 , c_2 and the two levels. Suggest a control structure with four feedback loops.

2) Measurements are c_2 and the two levels. Suggest a control structure that makes q_{w2} return to its desired value at steady state.

Problem 2 – PID controller tuning (15%)

Consider a process given by the following process model

$$G_1(s) = \frac{3}{(100s+1)(10s+1)}e^{-2s}$$

In addition, the measurement has a time delay θ_m given by $G_m(s) = e^{-\theta_m s}$.

Design a PI- or PID-controller (say which one you suggest) using the SIMC rules with $\tau_c = \theta$ (effective delay) for the following two cases:

- a) $\theta_m = 1$.
- b) $\theta_m = 20$.

Problem 3 – Closed-loop transfer functions and tuning (10%)

Consider a process G(s) with no measurement dynamics.

- (a) We use a standard feedback controller, $u = C(s) (y_s-y)$. Draw the block diagram. Derive the closed-loop transfer function T₁ from the setpoint y_s to the output (measurement) y, and the closed-loop transfer function T₂ from the setpoint y_s to the input u.
- (b) Let $G(s) = \frac{k}{\tau_1 s + 1}$ and design a PI controller tuned with the SIMC rules and $\tau_c = \tau_1$ (this choice for τ_c is the basis for the so-called λ -tuning). Derive T₁ and T₂ for this case (make the result as simple as possible).

Problem 4 – Pairing and decoupling (15%)

The relative gain array (RGA) is a tool one can use to analyze interactions and decide on controller pairings in multivariable systems. Consider the following process and steady-state RGA:

 $G(s) = \begin{bmatrix} 10e^{-5s} & -3 & 6\\ 3 & 1.5 & -0.5\\ 5 & 2 & -1.5 \end{bmatrix}, RGA(0) = \begin{bmatrix} 0.45 & 0.22 & 0.33\\ -0.82 & 2.45 & -0.64\\ 1.36 & -1.67 & 1.31 \end{bmatrix}$

Note that input 1 corresponds to the first column in G, output 1 to the first row in G, etc.

- a) How would you pair the inputs with the outputs (controlled variables)?
- b) What are the implications if you pair on the following RGA values $\lambda_{i,i}$?

1.
$$\lambda_{i,j} < 0$$

2.
$$0 < \lambda_{i,j} < 1$$

- 3. $1 < \lambda_{i,j}$
- c) Explain what decoupling is and how it can be used to reduce the effect of interactions. Design a one-way decoupler for a 2x2 process G which may improve the control of y₁. Can the one-way decoupler always be realized?

Problem 5 – Closed-loop stability of inverse-response process (15%)

- (a) Consider PI-control of the process G(s) = (1-5s)/(8s+1) with integral time $\tau_1 = 8$. For what controller gain K_c is the closed-loop system stable?
- (b) Design a SIMC PI-controller for this process with $\tau_c = \theta$ (effective delay). What is the gain margin? What is the time delay margin?



Problem 6 – Controllability (15%)

We want to control the temperature (y=T) in a reactor. The MV is the cooling rate (u=Q) and the disturbance is the feed rate (d=F).

In the figure is shown the response in temperature to a large step disturbance (F + 30%) and to a change in the input (Q + 10%). Note that the largest possible input change is Q +50%.

We would like the temperature deviations to stay within +- 1K.

- (a) Suggest transfer functions for G(s) and G_d(s). For the scaling, let u=1 correspond to Q=50%, let d=1 correspond to F=30% and let y= 1 correspond to a temperature change of 1K.
- (b) Is the process controllable? Sketch the expected closed-loop response in temperature to a 30% increase in F.

Bode paper:

									6 A. A. A.					!		¹ - 1				1.2.2	· · · ·									* * * *
	111	200	1.1	111			113		2112	12.1	1222		1.12	:::	11	1.12			200		115	: : :	100	22.2	:::	200	22	1:3	112	1111
	200			-1-1					(* * <u>*</u>		11222		1.17		:	· • [*]					:		111			(· · ·	1 - 1		111-
	1.1.1			·. · .										:	• • •													1.1.1		1111
														;								1.						1.1		1111
- · · · ·															:													111		1111
L	8						1		1 1.	. Å				!					·		•		1.1			ř	λ.,	1.1		1111
	:								11	0										:	: :	:					1	1		:::
	:	1 1		1.1			- 3						- 0	- 1					:	: :	: :	1.1					2	: :		:::
L									1					!					·	٤			1.1.1			· · · ·		1.1		111
E::::							110	::::					: :::	:::	:::	::::				:::		:::			:::			:::		:::-
	1111		:::	1111	:::	2222	111		1111	12.1			1.11	111	111	1.111				:::		111			:::		12.1	2:3	111	1111
																!														
	1.1.1	i		-1-1	- 7.7		· · ?		(+ + è	· .			1.10	• • •	· · ;	j					· · ·	· ? ·						1.1		
		-()		-1-1	- ; ;		$\sim -\frac{1}{2}$		(+ -)÷	· [(-		· · ;	;-				÷	(;	· ; .				(÷ - ;		
	1	: :							1.1	1						1					: :			1		÷	1	: :		:::
		· · · ·					;		(* *)				1.15	;	• • •	· - (-						- 7 -	111	(* * *		(· · ·	÷÷•	111		111
	1	: :		11	::				1 1	1				- 0		1			:	:	: :	1		1		1	1	: :	: :	:::
	:	1.1		1.1	11					1						1					: :			1		:	1	: :		:::
E	2.2.2	58 E I	222	555	e e e	2222	112		111	101			1.00	111								171					22	111	11	E
				22			110		111		1111		1.15			199					1.1						÷ -	111		1111
		111		111	111	2222	115		111	11			1.11		1.1	1.11						11					1.1	2.2.3	11	1111
	. i								i. i.	÷.,												. i .					. i	1.1		1114
L	. i								1t.						:	:			:		::	. i .				j	ί.	1.1	1.1	:::1
	1	: :		: :						1						1				:	: :			1			1	: :	: :	: : :
	1	: :		1.1	11				11	1				- 1		1			:		: :	1		1			1	1 1		:::
	:	: :		: :	11				11	1			1	- 1	:	1			:	:	: :	:		:		:	1	: :	: :	:::
H : : : : :	1111	20.03	C 1 C	2023	0.00	0000	:::	::::	2000	100	00000	0000	100	:::	1.0	101	100000	:::::	0.1.1	5 5 5	0.00	: : :	0.0	2000	:::	1111	100	200	111	1 2 7 2
þ:::::	111	2003	111	:00	:::	2000	:::	::::	St 12	:0:	10000		1.00	::::	10	:::::	100000	:::::	10.00	111	110	: : :	111	2000	:::	(c.c.)	20	515	111	1335
	2.1.1	(† 14) 1917 - Starter B	11	:::	111		$\left(\cdot \right)$		0.02	21	11111		: 12	111	11	101	100000		200		11	111	111	(* * *	• • •	(† 14) († 14)	21	(-	111	: : : i
E	111			2.1	111	<u>.</u>	11		111	11			1.11			1.1						11					11	111		1111
[1																													111
F · · · · ·	1.1.1		11	111	111		• • • ;		1117	17.1			1.11	• • •	• • • :	· · ; ·					: :	171			• • •			111		:::1
	(4.1		11	12				6.3	÷.,				:						;		. : .	11			(4.1	1.1	1.5	; ; ; . .
	1.1		1		11				11												: 1	1					1	1.1		:::1
	1	: :		11	11				1.1	1	: : : :					1	::::		:		: :	1	: : :	:		:	1	1	: :	:::
		÷			. ; ;				(š.	÷.,													1.1			(4.1	÷.,		::4
							::;			12.1			1 1 1 1	::;	::;	::;:		:::::		; : :		:;:			:::	::::	22	::;		:::=
	(22.20	:::	223		2111	110		111	100			1.11	111	11	122			22.2			101					12.2	2.1.3	11	1111
							• • •																							
- · · · ·	÷ • •	÷)	· · ;	-:-:	- ; ;		· · ;		(++)e	÷			j-	· - ;	· · ;	j					÷ -:	· ; ·				(· · ·	÷ -	÷	• •	
- · · · ·	÷	·()		-1-1	- ; ;		$\cdot \cdot ($		()-	- (· ·	· - ;	;	· -(-					()	- ÷ -						$\{\cdot, \cdot\}$	• •	
	:	:			• •				: :										•	•	: :			1				: :		: : :
		· · · ·							(* *)	÷;			1.15	•••;		(r.					11	· ; ·	111	· · · ·		(· · ·	÷.	111		1111
	:	: :		11	11				: :					- 1		1			:	:	: :			1		:	1	: :	: :	:::
	1	1 1	1	11	11	1	1		1.1	1		1	1				1111				: :	1	: : :	1		1	1	1.1		:::
	-																							-			_			
																														· · · · ·
				-																										
																			· · · · · · · · · · · · · · · · · · ·											
																			· · · · · · · · · · · · · · · · · · ·							1 - - - - - - - - - - - - -				
																			· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·										
																									••••					
																									••••					
													-																	
																									· · · ·					
																									· · · · ·					
																									· · · · ·					
																									· · · ·					
																									· · · · ·					