Energy savings in data centers: A framework for modelling and control of servers' cooling

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From Wikipedia¹:

- [...] a facility used to house computer systems and associated components
- the main purpose [...] is **running the IT systems applications** [...] of the organization
- [...] large data centers are **industrial scale operations** using as much electricity as a small town

¹wikipedia.org/wiki/Data_center



Description of a limited line of a sec-

Structures within a data center and their logical connections



Footprint

EU-28: (year 2013)

- Industry market: 18.85 billion €
- Electrical power consumption: 103.4 GWh

(~ 3% of electrical power production)

• 38.6 metric tonnes of CO_2 emissions (347g/kWh)

- i) Electronics convert virtually all power into heat
- ii) Cooling accounts for up to 40% of power budget
- iii) Computing's power consumption dependent on thermodynamical state
- iv) DCs rarely operate at peak computing capacity²

Problem: Efficiency (static, nominal, cooling policies waste power)

²Often desired since it is paramount to maintain Quality of Service

Control-oriented solution

Measure & predict the thermodynamical state to reduce overprovision of the cooling resources

i) single server level (focus of this paper)

- ii) rack level
- iii) room level

Example of "atomic unit": air-cooled blade











Modeling air-cooled blades, in math

Notation

states:

•
$$\boldsymbol{x}^{c} = \begin{bmatrix} x_{1}^{c} & \dots & x_{n}^{c} \end{bmatrix}^{T} \Rightarrow$$
 temperatures of IT components
• $\boldsymbol{x}^{f} = \begin{bmatrix} x_{1}^{f} & \dots & x_{n}^{f} \end{bmatrix}^{T} \Rightarrow$ temperatures of air flows through IT components

exogenous inputs:

•
$$p = [p_1 \dots p_n]^T =:$$
 electrical power dissipated by IT components
• $x^i =:$ temperature of air inlet

manipulable inputs:

•
$$\boldsymbol{u} = \begin{bmatrix} u_1 & \dots & u_m \end{bmatrix}^T =:$$
 air mass flows produced by fans
(determining the air flows through the IT components $\boldsymbol{f} = \begin{bmatrix} f_1 & \dots & f_n \end{bmatrix}^T$)

Ingredients to be modeled



i) mass of the air flows fii) temperature of the air flows x^f iii) temperature of the IT components x^c

Model of the mass of the air flows



$$\boldsymbol{f} = \Lambda^{d} [\boldsymbol{u}] + \Lambda^{r} [\boldsymbol{f}]$$
(1)

$$\Lambda[\boldsymbol{u}] = \sum_{i=1}^{\binom{m+d}{d}} a_i \boldsymbol{u}^{\boldsymbol{\alpha}_i}$$
(2)

Model of the mass of the air flows



$$\boldsymbol{f} = \Lambda^d [\boldsymbol{u}] + \Lambda^r [\boldsymbol{f}]$$
 (1)

$$\Lambda[\boldsymbol{u}] = \sum_{i=1}^{\binom{m+a}{d}} a_i \boldsymbol{u}^{\boldsymbol{\alpha}_i}$$
(2)

Generalizes:

- i) models without *warm* recirculation flows ($\Lambda^r = 0$)
- ii) models preserving total mass-flows (Λ^d and Λ^r row-stochastic matrices)

Model of the temperature of the air flows

Assumptions:

- i) perfect flow mixing
- ii) heat energy conservation

$$x_j^f = \frac{\Lambda_{(j)}^d [\boldsymbol{u}] \cdot x^i + \sum_{h=1}^n \Lambda_{(j,h)}^r [\boldsymbol{f}] \cdot x_h^c}{f_j}$$

(3)

Model of the temperature of the air flows

Assumptions:

- i) perfect flow mixing
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$$x_j^f = \frac{\Lambda_{(j)}^d [\boldsymbol{u}] \cdot x^i + \sum_{h=1}^n \Lambda_{(j,h)}^r [\boldsymbol{f}] \cdot x_h^c}{f_j}$$

corresponds to averaging

(3)

Model of the temperature of the IT components

$$\dot{x}_{j}^{c} = -h_{j}f_{j}(\boldsymbol{u})\left(x_{j}^{c} - x_{j}^{f}(\boldsymbol{u}, \boldsymbol{x}^{c}, x^{i})\right)$$
convection
$$+ \left[R_{(j)} \quad \rho_{j}\right] \begin{bmatrix} \boldsymbol{x}_{j}^{c} \\ x^{i} \end{bmatrix}$$
conduction
$$+ \underbrace{b_{j}p_{j}}_{\text{electrical power}}$$

(4)

Model of the temperature of the IT components



Euler forward discretization:

$$x_j^c(k+1) = \Psi_j^{\Delta}(x_j^c(k), \boldsymbol{u}, \boldsymbol{p}, x^i)$$
(5)

(4)

Minimum cost fan control

$$\min_{\boldsymbol{u}(0),\dots,\boldsymbol{u}(H-1)} \sum_{t=0}^{H-1} \sum_{h=1}^{m} (u_h(t))^3$$
subject to (for $0 \le t \le H-1, 1 \le j \le n$):
$$\boldsymbol{x}^c(0) = \boldsymbol{x}_0^c$$

$$\boldsymbol{u}_{\min} \le \boldsymbol{u}(t) \le \boldsymbol{u}_{\max}$$

$$\boldsymbol{x}^c(t+1) \le \boldsymbol{x}_{\max}^c$$

$$\boldsymbol{x}_j^c(t+1) = \Psi_j^{\Delta} \left(\boldsymbol{x}_j^c(t), \boldsymbol{u}(t), \boldsymbol{p}(t), \boldsymbol{x}^i \right)$$
(6)

numerical simulations

- i) how accurate is the polynomial flows model?
- ii) how conservative is the control strategy?

Validation of the model using CFD



Algorithm:

- **(**) set boundary conditions (i.e., $\boldsymbol{p}, \boldsymbol{u}, x^i$)
- e use CFD model as a virtual plant
- estimate the parameters using RLS

Validation of the model using CFD

 $\deg(\Lambda^d) = 2, \ \deg(\Lambda^r) = 1$



Validation of the control strategy

Experiment 1: $p(t) = p_{max}$

Experiment 2: p(t) = stochastic process with seasonal trends (medium-high loads)

Validation of the control strategy - Experiment 1



Validation of the control strategy - Experiment 2



Conclusions

- i) promising ability at capturing complex convective cooling effects
- ii) functional structure open to other cooling applications
- iii) can be identified starting from CFD models

Conclusions and future works

- i) promising ability at capturing complex convective cooling effects
- ii) functional structure open to other cooling applications
- iii) can be identified starting from CFD models

i) validate on real plants

- ii) generalize to "datacenter room control"
- iii) generalize to generic thermal networks

RISE SICS North ICE

- 3000 4000 servers (2MW)
- 160 m² lab
- biogas back up generators
- connections with the urban district heating network
- Generality, Flexibility and Expandability

Experiment-as-a-Service



RISE SICS North ICE



photos by Per Bäckström

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